

# Reusable Rocket Engine Operability Modeling and Analysis

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#### **ACRONYMS**

CAPSS Computer-Aided Planning and Scheduling System

DAR deviation approval request **ELV** expendable launch vehicles **EMA** electromechanical actuator

gox gaseous oxygen

**GSE** ground support equipment **HPFTP** high-pressure fuel turbopump

**HPOTP** high-pressure oxidizer turbopump

specific impulse  $I_{SD}$ 

**KSC** Kennedy Space Center

 $LH_2$ liquid hydrogen liquid oxygen  $LO_2$ **MDT** mean downtime material review MR MS Microsoft®

**MSFC** Marshall Space Flight Center **MTBF** mean time between failure

**MTBM** mean time between maintenance

**MTTR** mean time to repair

National Aeronautics and Space Administration NASA

**OMEF** orbiter main engine facility

**OMI Operations and Maintenance Instructions** 

Operations and Maintenance Requirements and Specification Document **OMRSD** 

**OPF** orbiter processing facility

PR problem report

**PRACA** Problem Reporting and Corrective Action

thrust vector control assembly

R&R remove and replace **RLV** reusable launch vehicle **SSME** space shuttle main engine **STS** Space Transportation System **TVCA** 

**VAB** vehicle assembly building

#### TECHNICAL PUBLICATION

#### REUSABLE ROCKET ENGINE OPERABILITY MODELING AND ANALYSIS

#### 1. INTRODUCTION

The reusable launch vehicle (RLV) cooperative development program between NASA and the aerospace industry demands the design of cost-effective vehicles and associated propulsion systems. In turn, cost-effective propulsion systems demand minimal and low recurring costs for ground operations. Thus, the emphasis early on in this program should be effective operations modeling supported by the collection and use of applicable operations data from a comparable existing system. Such a model could support the necessary trades and design decisions toward a cost-effective propulsion system development program. These analyses would also augment the more traditional performance analyses in order to support a concurrent engineering design environment.<sup>1-4</sup>

In this view, functional area analyses are conducted in many areas including operations, reliability, manufacturing, cost, and performance, as presented in figure 1. The design engineer is responsible to incorporate the input from these areas into the design where appropriate. The designer also has the responsibility to conduct within and between discipline design trades with support from the discipline experts. Design decisions without adequate information from one or more of these areas results in an incomplete decision with potential serious consequences for the hardware. Design support activities in each functional area are the same. Models are developed and data are collected to support the model analysis. These models and data are at an appropriate level of detail to match the objectives of the analysis. Metrics are used in order to quantify the output. This is an iterative approach that supports the design schedule with results updated from increasingly more detailed design information.

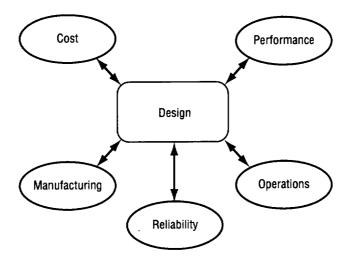


Figure 1. Disciplines in design.

Currently, in aerospace applications, there is a mismatch between the complexity of models (as supported by the data) within the various disciplines. For example, while good engine performance models with accurate metrics exist, the use of absolute metrics of reliability for rocket engine systems analysis is rarely supported. This is a result of the lack of good test data, lack of comparable aerospace systems, and a lack of comparative industrial systems relative to aerospace mechanical systems. Metrics also tend to be less credible for reliability. There is, as yet, not a comparable reliability metric that would allow one to measure and track reliability as the engine specific impulse (I<sub>sp</sub>) metric allows one to measure and track engine performance. Performance models such as an engine power balance model or a vehicle trajectory model tend to be of good detail, with a good pedigree, and the results well accepted by the aerospace community. The propulsion system designer has to be aware of these analysis fidelity disparities when it becomes necessary to base a design decision on an analysis.

There is a need to develop models to obtain different objectives. Early in a launch vehicle development program, a top-level analysis serves the purpose of defining the problem and securing top-level metrics as to the feasibility and goals of the program. This "quick-look" model effort serves a purpose—it often defines the goals of the program in terms of performance, cost, and operability. It also is explicit about the need to do things differently in terms of achieving more stringent goals. A detailed bottom-up analysis is more appropriate to respond to the allocation based on an indepth study of the concepts. The "quick-look" model is appropriate if the project manager is the customer; the detailed analysis is directed more at the design engineer. Both are of value. The "quick-look" model also may serve the purpose of the allocated requirements model, the model to which comparisons are made to determine maturity of the design. It is inappropriate to use the data that supported the allocation of requirements to also support the detailed analysis. Although often done, this is inappropriate and could lead to misleading results.

The acquisition of good data is a traditional problem for the definition of baseline systems for aerospace launch vehicle operations analyses. For all models developed here, the Space Transportation System (STS) and the space shuttle main engine (SSME) are used as the source of historical reusable vehicle and engine systems operations experience. For the detailed model, the approach demands the identification of the requirements for SSME ground operations and the root source of the requirements. From this, a reusable engine model is developed that is based on the SSME operations model. This is done through incremental modification of the baseline operations model based on the proposed changes from the SSME to the reusable engine. The modifications of these processing activities are based on changes in hardware configuration and technology, processing technology improvements, and operations philosophy. The reusable engine system model is then traceable to past requirements and historical experience. This modeling approach supports credible operations modeling and analysis. In this paper, the baseline SSME model and a demonstration of its utility are presented.

#### 2. BACKGROUND

The lack of historical data in support of aerospace launch vehicle operations analyses is acute. Data are either unavailable due to not being collected or not public, or are so highly aggregated as to mask needed detail at the process level. Top-level models generated by existing data were generally useful only for supporting programmatic goal discussions. Discrete event simulation models have often been models of choice.<sup>5-7</sup>

One approach to aerospace launch vehicle operations analyses is to compare with aircraft data. This information is generally more readily available and in the proper format with data collected from a maintainability point of view. Several papers have taken this approach.<sup>8,9</sup> While this data supports good model development, the question of applicability of results is more of an issue. This is especially true of rocket and aircraft propulsion systems with major differences in configurations, environment, and operating philosophy. Specifically, these differences include operating environment; operating temperatures, pressures, and thrust; ability to idle, taxi, and loiter aircraft engines and vehicles; use of cryogenic fuels on rockets; large performance margins on aircraft; nonintrusive health management of aircraft propulsion systems; and, perhaps the major difference, a philosophy of use with aircraft that tolerates test and operational failures (and even loss of life).

Ground operations analyses have also been conducted for aerospace launch vehicles based on available STS operations data. <sup>10,11</sup> Although the available data were found to be insufficient, <sup>12</sup> existing databases can be augmented by other sources, such as the experience of launch site personnel. This study builds on this approach. The SSME is regarded as the most directly applicable baseline for comparison with future and similar liquid oxygen (LO<sub>2</sub>)/liquid hydrogen (LH<sub>2</sub>) rocket systems. Thus, for this effort, extensive data collection was undertaken for STS propulsion systems to augment the existing databases. A baseline set of propulsion systems ground operations databases has been developed with the goal of supporting detailed engineering analyses of process and manpower requirements for future propulsion system concepts.

#### 3. OPERABILITY ASSESSMENT METHODOLOGY

# A. Approach

The operability assessment methodology described in this document reflects an end-to-end process flow model that models the uncertainties inherent in the attributes of the process flows. This approach attempts to substitute a rigorous and objective structure for more qualitative types of judgments and to focus design experiences to help determine areas of design confidence. It is to be used upfront in the design process and combines past flight vehicle experiences with design analysis to determine cost and schedule parameters of interest. It can be used in the analysis of any process flow where the goal is to optimize processing in order to minimize cost and schedule impacts.

The continuum of process flow activities includes development through manufacturing, assembly, and operations. For this modeling effort, the emphasis will be on the operational phase only. Figure 2 presents the flows of the operational phase of a launch vehicle, a subset of which will be the focus of this analysis.

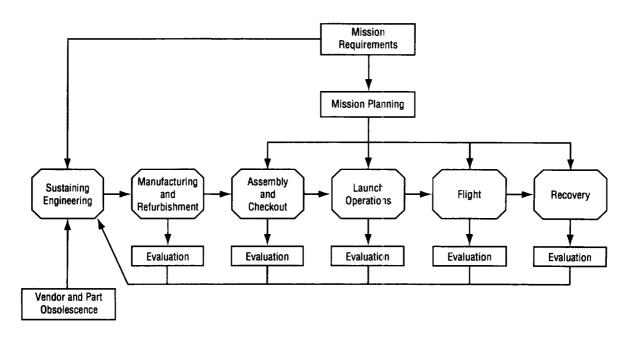


Figure 2. Launch vehicle process flow—operational phase.

The process flow model avoids estimates of cost and schedule parameters based upon nonspecific design characteristics such as weight and the use of integration "scale factors." In this modeling effort, cost and schedule indicators will be based upon realistic, high-fidelity process flows targeted against the current design configuration.

This approach incorporates past vehicle development experiences in terms of experience databases. These are critical parts of this methodology and are explicitly included in the approach. Since it is often difficult to obtain historical data to support these design decisions, a significant effort was undertaken to identify, incorporate, and appropriately structure this information for use with the process flow model.

Figure 3 presents the input flowing to the proposed process flows of a new launch vehicle. The new vehicle requirements and design configuration contribute in the definition of flows as does information gathered relative to historical launch vehicle flows. Data and requirements that are applicable from past launch and flight vehicles, including aircraft, expendable launch vehicles (ELV's), and the STS, may be used to generate or edit proposed flows and will be the main source of what is required (attributes) by these process flows in terms of manpower and schedule. The design and proposed flows will be continually updated, thus the approach is iterative. Also, historical data will be useful in providing insight into the traditional problems associated with the proposed process flow. Finally, new systems may require certain technology or special analyses to determine the operability of the system. This is also input to the process flow definition process. All of this information is, of course, subject to adaptation and interpretation by the design, manufacturing, and operations engineers. These groups and others must be involved at the outset in order for this to be a truly concurrent engineering effort.

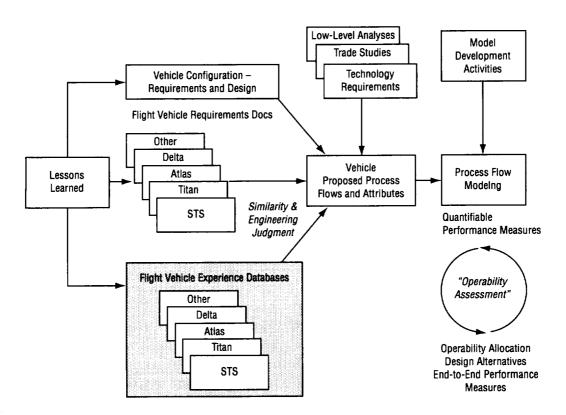


Figure 3. Operability assessment methodology.

The lessons learned on other vehicles implicitly affects current design engineering efforts and also serves to organize the search for applicable historical data. For example, the problems of past hydraulic systems on flight vehicles may cause the design engineer to attempt to include an electromechanical actuator (EMA) subsystem into the current design. Also, this "lesson learned" can serve to organize the identification of historical process flows, requirements, and experiences. Organized appropriately, historic processes associated with hydraulics can be easily pulled from the database, thus facilitating the analysis of this problem area by an appropriate design engineering team. This step of the methodology involves more of a qualitative assessment than a quantitative one. However, there is a structure surrounding the use of "lessons learned" that reflects the need to evolve and iterate this process with the "lesson learned" information.

Once the process flows and associated attributes have been defined, the modeling of the flows to generate quantifiable performance measures can be supported. The probabilistic nature of the system is clear due to the uncertain environment. Sensitivity studies, design change studies, and operability assessment studies are all supported.

A top-down approach is utilized in identifying and tracing process flows. At the outset, this hierarchical method is useful in identifying major cost and schedule drivers and assists in the allocation of scarce resources in the further analysis of the lower-level process flows. The danger of low-level analyses is the danger of misallocation of scarce resources to analyses that are not clearly important cost or schedule drivers. A top-down approach creates traceability of functional flows at each level in the hierarchy. It also serves to document and allocate the top-level program requirements. Its usefulness is limited to a "quick-look" analysis and for comparison purposes with the detailed analyses.

This methodology is designed to incorporate results from bottom-up analyses. Systematic evaluations of low-level process flows in terms of cost and schedule attributes will feed a detailed modeling activity. Once both models exist and comparisons are supported, both goals and actual timelines are subject to change: the top-down apportionment can be reallocated or changed; and the bottom-up reanalyzed and adapted to design changes resulting from changes incorporated into the design influenced by this modeling activity. Given this approach, the initial emphasis of this effort will be on supporting relative comparisons among design changes. Upon completion of an appropriate level of detail, accurate estimates can be generated.

Figure 4 provides an overview of this two-pronged approach. First, a goal timeline is created from a future launch vehicle operations concept. Making this goal reflect an actual design is desirable if such a design exists. However, these are goals, and as such, are meant as comparison points for a bottom-up engineering analysis of a historical baseline system. The second prong is this bottom-up effort, which provides an experience base and supports traceability to design, technology, and process improvements for the future launch vehicle propulsion system. This bottom-up effort is the focus of this paper. A previous paper presented the goal-oriented approach, with both scheduled and unscheduled processing included in the goal flows. By nature, this approach is iterative. Comparing the historical estimates against the goals provides an identification of key differences. Design decisions will seek to lessen these differences—larger differences seeking the most design effort in an appropriate design manpower allocation process. The design will change and so also will the goals. Unrealistic goals and requirements will be identified and adjusted. Trades between performance and operations or cost and operations will be key for the overall risk assessment. A previous paper also laid out an example of such a bottom-up analysis based upon experience

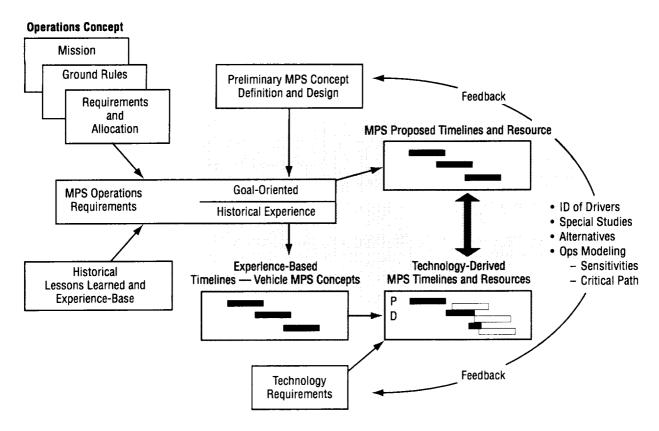


Figure 4. Design-to-operations analysis approach.

data.<sup>14</sup> Yet another paper points out the need to begin with experience-based requirements for this type of bottom-up analysis.<sup>15</sup>

Performance requirements as defined in requirements documents are allocated to a lower level and serve as goals for the system designer. One of the purposes of this effort is for the quantification of operability measures to support the comparison of the design against the requirement. Thus, this methodology serves to verify the relationship between design decisions and the fulfillment of design objectives. Furthermore, an appropriate quantification can serve to support the analysis of the current design suitability against a previous design. In this sense, both absolute and relative measures of merit are generated in this modeling approach. However, before a fully detailed model supporting the generation of absolute measures can be generated, a top-down flow can support the relative model comparison of critical use to the designer. A designer involved in a specific area of design can "stub" in the other parts along with their schedule and cost estimates and work in detail in their appropriate design area.

#### **B.** Key Concepts and Definitions

Establishing good measurable metrics is key to any functional area analysis methodology. Following is a discussion of key operability definitions and metrics.

Operability—the ability to support required flight rates and schedules and to meet a variety of operational characteristics while minimizing cost and risk. In this definition, operability is not directly

measurable. Common metrics for operability include availability, turnaround time, and dependability. The definition of operability touches upon several key ideas including those of minimizing cost and risk. Risk may be defined as an expression of the likelihood and consequence of an event of interest. Risk involves an attempt to understand the uncertainty in and between the functional areas of the design. This emphasizes the need to model an end-to-end system.

Dependability—probability of achieving a given launch without sliding the schedule on the next launch, given that the system is not in postfailure standdown; if hardware, the ability for the hardware to perform as needed when needed. Often defined in terms of probability of launching within x days of the originally scheduled launch date.

Availability—fraction of time the system is operational rather than in standdown or delay; the probability that a piece of equipment will be capable of performing its mission when needed rather than being unserviceable due to failure, delays, or intentionally or unintentionally removed from service for maintenance or testing; is useful as metric for both hardware and processes; inherent is mean time between failure (MTBF)/(MTBF + mean time to repair (MTTR)); operational is mean time between maintenance (MTBM)/(MTBM + mean down-time (MDT)); also, scheduled time/(scheduled + unscheduled time). This latter definition is more aerospace-oriented given its acknowledgment of few vehicles that require extensive processing due to leading-edge technologies and cryogenic fuel operations. The traditional definition of availability is directed more at the military and commercial aircraft operations where there are large fleets of vehicles and preflight operations are relatively minimal. The process definition of availability is more suitable for this discussion and will be referred to throughout this analysis. Also, in this definition, a system is penalized only for unscheduled maintenance activities that occur on the critical path.

Turnaround Time—a measure of maintenance having to do with time from last recovery to next launch.

Reliability—probability of successfully concluding a mission segment; probability that an item will perform a required function under stated conditions for a stated period of time. Though metrics for reliability are not often included in operations analyses, reliability of the components and systems plays a critical role in determining the operability of the system. The operability study in this paper will include engine reliability measures.

#### C. Modeling and Uncertainty

The goal of any modeling activity is to accomplish accurate quantification in as realistic an environment as possible. This involves the need for quantifying in the presence of uncertainty. Thus, the model should ultimately be reflective of a probabilistic approach. Uncertainty is not only reflected in the accuracy of the information that exists but also in the availability of information that may lead to an inability to effectively model the system. These are both important pieces of information—manpower can be allocated to obtain the data or to complete the analysis that is required to lessen the uncertainty. The analyses cannot entirely eliminate the uncertainty associated with a process flow but are intended more to understand the extent of the uncertainty. Indeed, if no uncertainty exists in a design, no decisions are necessary.

There are several sources of uncertainty inherent to a process flow, including variation of nominal processing; that is, a process scheduled for 5 hr may actually take 4 hr one time and 6 hr the next. This can be modeled through the selection of an appropriate process time distribution supported by empirical evidence. Other realistic scenarios that will affect the schedule and cost include process failures, equipment failures, and associated unscheduled maintenance activities. Also, delays due to repair times, queuing delays, and waiting for resources can affect the planned schedule. The weather is a major source of delay at time of launch.

#### **D. Process Flow Definition**

The types of documents and databases used to generate the process flow for this analysis may be identified. In the case of the world's only RLV, the space shuttle, the documents that describe the requirements and the implementation of the requirements are the Operations and Maintenance Requirements and Specification Documents (OMRSD) and the Operations and Maintenance Instructions (OMI), respectively. Applicable process requirements and flows have been obtained from these sources for the specification of new vehicle operations process flows.

Some attributes of the proposed flows can be obtained from the electronic database system in use by the STS program. The STS Computer-Aided Planning and Scheduling System (CAPSS)<sup>16</sup> contains the nominal schedule and manpower requirements while the Problem Reporting and Corrective Action (PRACA)<sup>17</sup> supplies the information on the problems and off-nominal flows that occur throughout STS processing. Other commercial launch vehicle data such as Titan, Atlas, and Delta operations requirements documents and operations experience databases, if available, can also support this type of analysis. Data requirements include both nominal and off-nominal process times and resource requirements. Mean time to repair along with incidence of repair are typical performance measures derived from such databases.

As stated earlier, the data that supports the allocation process and the data that supports the detailed design evaluation should come from separate sources. In aerospace analyses, this is often not the case, primarily due to the lack of good data. While rough parametrics from one detailed source may feed the allocation process that uses several sources, this kind of analysis should be discouraged. At best, this kind of analysis is redundant and provides little confidence that the conclusions reached are correct. It could lead to inaccurate and misleading conclusions, resulting in a misallocation of design resources.

## 4. MODELING TOOLS

Several good off-the-shelf software packages fit the need to support operations model development. A process flow model is the model of choice: it allows the analysis of timelines, schedule dependencies, resource requirements, and supports the generation of measures of operability including recurring costs, availability, and dependability. The models used here utilize Microsoft® (MS) Project¹8 for deterministic flow analysis and Imagine That!® Extend™ software¹9 for probabilistic support. The benefit of MS Project™ as a process modeling tool is its ability to graphically represent detailed tasks in Gantt charts, allocate and track resource levels, and filter project information. Inputs to the model include the task description, resource allocation, task duration, and establishment of task precedence. MS Project™ is generally all that is required to do the "quick-look" analysis—layout top-level requirements and allocations to subsystems and components. Charts, tables, or reports can be customized to output the level of detail desired by the user. Extend™ allows us to apply the model in a discrete-event simulation format. It supports ease-of-input (icon-based), provides good report-generation capabilities, is well supported and tailorable with source code available, and provides animation capabilities useful for display and debugging purposes.

#### 5. BASELINE ENGINE OPERATIONS DATA

#### A. Data Collection

The data collection process was a considerable part of this activity. This section will discuss this process and the data in some detail. Data were collected from a task-by-task point of view: what is required to complete only this task. Often times data are collected from a time-reporting point of view, making it difficult to determine actual task time. Appendices are provided to this document that will contain the data collected. An overview of the SSME data collection in support of the operations modeling approach is shown in figure 5. The analysis consisted of three parts: deterministic model of allocated processing, deterministic model of unscheduled processing, and the probabilistic model. This section discusses the baseline SSME model in the context of the deterministic modeling approach (both scheduled and unscheduled) and the baseline requirements database that is the foundation for all SSME processing activities. A complete presentation of the SSME operations database resides in appendices A (requirements), B (scheduled), C (unscheduled), and D (results).

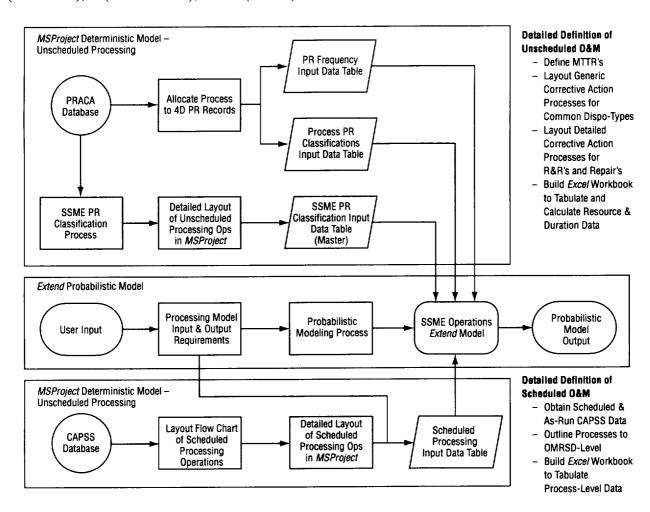


Figure 5. Operations modeling and data collection process.

# **B.** Scheduled Processing

The first step was to define the nominal SSME processing flow. This was accomplished with flowcharts that identified the OMI-level processes and the location/facility in which the process was performed. SSME component life limit issues dictate that engine removal be scheduled each processing flow to allow the SSME's to be processed offline in the orbiter main engine facility (OMEF). Thus, in addition to the every flight requirements defined by OMRSD, nominal processing, for the purposes of the model, included SSME removal in the orbiter processing facility (OPF); SSME processing off-line in the OMEF; high-pressure turbopump removal and installation in the OMEF; and SSME installation in the OPF.

Data collected relative to SSME processing is presented in figures 6–9. Figure 6 identifies the OMI's and the serial and parallel nature of the process flow for the events that occur immediately after flight in the OPF. The engines are then moved to the OMEF. Figure 7 presents the processes and flow for this facility. After processing in the OMEF, the engines are returned to the OPF to be reinstalled on the vehicle. This process is shown in figure 8. After installation, the engine processing steps that occur during the vehicle assembly building (VAB) and pad operations are defined (see fig. 9). The detailed SSME scheduled data that matches the OMI's in figures 6–9 appears in appendix B. These data are quite extensive, breaking out process flow dependencies, clock hour, and manpower requirements by type for each engine process. It should be noted that not all engine processing is fully represented here. Some routine and periodic actions associated with minor OMI's, job cards, or deviation approval requests (DAR's) were excluded in order to present a system that can be represented in a model as an operational system. It is arguable as to whether or not the Shuttle system is a fully operational system. There are too many things that are done that are not necessarily repeatable from a modeling point of view. For example, the exact order of engine processing in the OMEF is subject to visibility, manpower available, and priorities in place at the time of repair, making this aspect difficult to model.

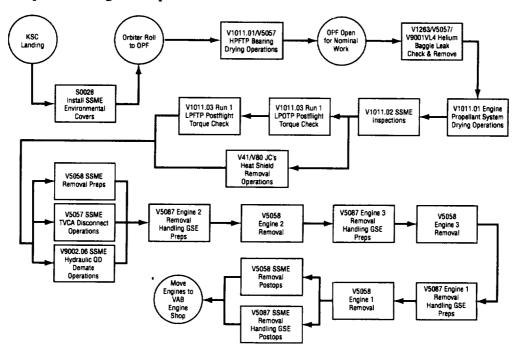


Figure 6. OPF SSME postflight operations.

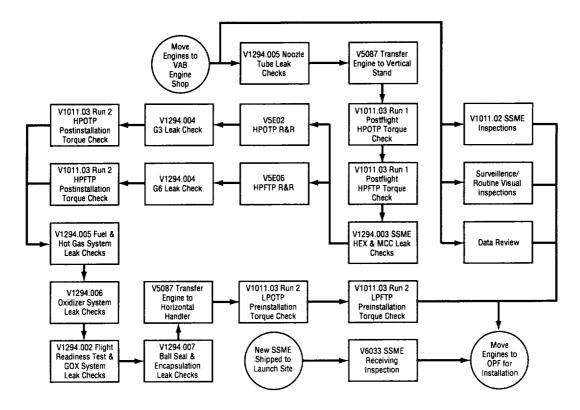


Figure 7. OMEF SSME operations.

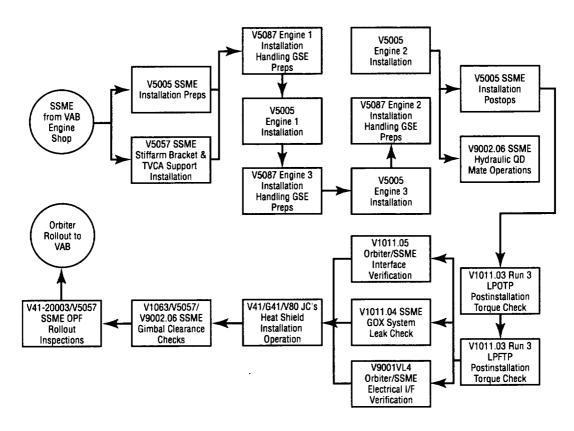


Figure 8. OPF post-SSME installation operations.

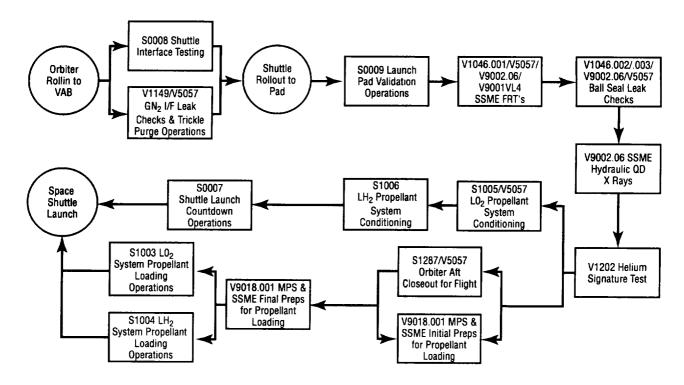


Figure 9. SSME VAB/pad processing operations.

The data that were collected were laid out into Gantt charts and task sheets to a lowest level of detail. Technician, quality control, and engineering resources were identified for each detailed task and the task duration was quantified based upon National Aeronautics and Space Administration's (NASA's) SSME engineering experience at Kennedy Space Center (KSC). Figure 10 exemplifies the level of detail outlined in each deterministic process; in this case, the high-pressure fuel turbopump (HPFTP) removal and replacement. In figure 10, many tasks have been rolled up to subtasks for brevity of presentation.

ID	Man-hr	Jul 23, '95 Jul 30, '95 Aug 6, '95 Aug 13, '95 Aug 20, '95 Aug 27, '95
טו	mall-III	TWITESSMITWIFESSMITWIFESSMITWIFESSMITWIFESSMITWIFESS
1	375.75	HPFTP Removal and Replacement
2	4	₩ HPFTP Removal GSE Preps
4	0.25	QC Call to Station
5	36	₩HPFTP Removal Preps
17	31.25	₩ HPFTP Removal Operations
32	29	Pump-Out Powerhead Inspections
37	42	HPFTP Internal Inspections
38	6	Tech [2], QC  ■ Remove HPFTP Bellows Shield
39	8	QC, Engr  Perform HPFTP Inspections w/Bellows Shield Removed per V41BU0.08
40	12	Tech [2],QCI Install HPFTP Bellows Shie d
41	16	QC, Engr∎ Perform HPFTP Internal Inspections per V41BU0.075
42	64.25	HPFTP Make to Powerhead
56	24	₩High Presure Fuel Duct Alignment
58	23	₩HPFTP Securing
59	4	Tech, QC I Secure Low Pressure Fuel Duct ● Joint F3
60	2	Tech, QC Install Elliptical Plug o Joint 64.3
61	12	Tech [2],QC Install Sensors, Sensor Mounts and Sensor Lines
62	1	Tech, QC Secure HPFTP Liftoff Seal Drain Line
63	4	Tech, QC Install Heat Shield Brackets to Nozzle
64	24	→ HPFTP Sensor Electrical Mate

Figure 10. Example of detailed model—HPFTP removal and replace.

Although serial and parallel relationships were established between the detailed tasks and OMI processes within the Gantt charts, it is difficult to accurately predict overall OMI durations or end-to-end vehicle or SSME subsystem processing times. Reasons for this include:

- 1. Lack of all downtime data including logistic delay time, administrative delay time, and maintenance delays downtime.
- 2. Interdependence between SSME and other subsystems was not modeled.
- 3. Other vehicle subsystems not modeled.

While accurate predictions of SSME processing are not always possible with this data, it is appropriate for future launch vehicle engine analysis since these kinds of attributes need not be modeled. Of interest for a future system analysis is the definition of an operational system. It is not desirable to model all the artifacts of the STS processing system as appropriate to the new system. While downtimes will occur for a future system as well, it is premature, without detail, to model those. Of course, a complete vehicle model should represent the engine-vehicle interface and other subsystem operations fully.

The baseline SSME model will provide insight into the actual workload, required subtasks, and the overall processing flow. This actual manhour prediction method differs from top-down manhour estimates in that manhours of downtime are not accounted for. The utility of determining manhours in this fashion is that labor-intensive processing activities are readily identified whereas the actual impact of each processing activity can be masked by downtimes in the top-down approach.

## C. Unscheduled Processing

An analysis of SSME unscheduled maintenance operations was performed using the PRACA database. Unscheduled maintenance information from the PRACA database was obtained for 30 STS flights between 1989 and 1994. During this period there were 3,785 problem reports (PR's) that were processed. This is engine PR's only, thus, ground support equipment (GSE), facility, and spares PR's relative to the engine were not included. The PR's were sorted and grouped by component, malfunction, and disposition code. This allowed the filtering of this database into 123 PR classes representing 84 SSME processing flows. PR's were further classified into six types based upon processing action taken. The six types, the 123 classes, and the number of applicable PR's are presented in table 1.

Table 1. SSME PR classification summary.

Number of Classes	Number of PR's
70	795
13	79
19	1,121
6	156
7	137
8	82
	70 13

This filtering processed 2,370 PR's. PR's that were eliminated from the database during this classification and filtering process included PR's from incomplete processing flows and PR records with insufficient data to allow it to be classified.

Each PR will fall into one of the six classification types. These types were categorized based upon the disposition code in the PRACA database and limited to the detail provided therein. These represent the most common actions required for each PR at the lowest level of detail possible. Each classification type was outlined to identify the basic tasks and resources associated with setup, performance, diagnostics, administration, review, and delay times. Figure 11 presents an MS Project<sup>TM</sup> view of the base remove and replace (R&R) classification type. In addition, an initial attempt at quantifying the resources required was conducted. Note that these are initial estimates until more accurate data can be made available and collected. The actual "hands-on" R&R time is represented by a milestone on line 4. This would be replaced in the model by the actual component R&R timeline.

The classes identify the number of different PR's that fall into each PR type. These are usually associated with components or hardware. In the case of an R&R PR type, the 70 different classes are mostly associated with different hardware or components that require R&R. However, this is not necessarily the case for the other PR types. For example, a large number of PR's were generated due to contamination and corrosion on unidentified hardware. Because the detail in the database did not allow us to associate the corrosion problems with the hardware or component, the contamination and corrosion PR's were separated into five different PR classification types based upon the nature of the disposition (repair, material review (MR) repair, accept, MR accept, or waiver/exception). The five other PR classifications as well as the standard R&R operations by component appear in detail in appendix C.

	Duration		y	Wed	ines	day	Th	ursd	ay		Frid	ay	S	atur	day	S	und	ay		7
ID	hr	Man-hr	4	12	8	4	12	8	4	1	2 8	4	12	8	4	12	8	4	1	2
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Figure 11. SSME base R&R.

This PRACA database is limited in that it does not provide resource or task duration information for unscheduled corrective actions. However, PRACA does provide data to determine the frequencies of PR's as well as information to determine what malfunctioned and how the PR was dispositioned. Corrective action processes, including task descriptions, durations, and resource assignments, were defined and quantified by SSME engineering in the same manner as the scheduled processes for each PR classification.

A few low-level processes were set to a standard time for simplicity sake. For example, QC response time was set to one standard value, when in actuality, this value is more dynamic. The unscheduled data as it applies to the six PR classifications appears in appendix C and a summary of the results from the data (relative to SSME) in appendix D.

# D. Baseline Requirements Database

Figure 12 describes how the data collected are being applied to the reusable engine analysis. The applicable requirements identified by the STS OMRSD's are mapped to major corresponding STS OMI's (see appendix A). An iterative review process identifies, task by task, the appropriate processing for the future engine operations. Future reusable engine-specific operations are added; SSME operations artifacts are removed; changes to processing facilities and support equipment is identified; and any dependency, timeline, or resource requirements are also specified. This leads to a traceable proposed operations flow prediction and resource estimate. Table 2 displays a sample of the OMRSD/OMI database with comments as to the applicability of the requirements to the reusable vehicle engine.

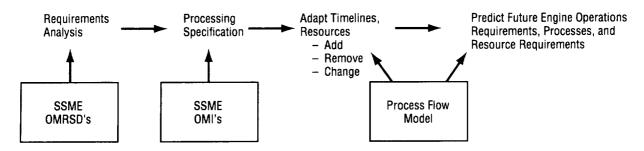


Figure 12. Requirements to process definition.

Table 2. OMRSD/OMI (	database with	requirements	rationale.
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OMRSD Number	New Engine Use	OMRSD Description (V41 File III Dated 9/15/95)	OPF OMI's	Engine Shop OMI's	VAB/PAD OMI's	DMRSD Rationale/Root Causes
V41BL0.050	. c	SSME Weld 22 & 24 Lk Ck	V1011.05 Seq 07	V1294.007 Seq 04	V1046.003 Seq 07	Due to poor processing, HPOTP balance cavity standoff welds are leak checked – No leaks ever verified, but lack of weld penetration up to 90% has been found on these welds. Standoffs have been suspected of leaking and caused return to Canoga.
V41BL0.060-A	n	E1 HPOTP Plug Weld Lk Ck	V1011.05 Seq 09	V1294.004 Seq 04	V1048.004 Seq 04	Plug weld leak occurred on a unit – Concern over these welds leaking either Gox/Hellum/Hot gas into boat tail – therefore all external plug welds or the housing are checked
V41AX0.020-A	у	E1 LO <sub>2</sub> Feed (Joint 01) I/F Lk Ck	V1011.05 Seq 07		V1046.003 Seq 05	Ensure joint integrity of LPOTP to pump inlet ducting after engine is installed
V41AX0.020-B	у	E1 LH <sub>2</sub> Feed (Joint F1) I/F Lk Ck	V1011.05 Seq 05		V1048.002 Seq 04	Verify pump inlet joint integrity after installing the LPFTP
V41AX0.020-C	у	E1 GH <sub>2</sub> Press (Joint F9.3) I/F LK CK	V1011.05 Seq 09		V1048.004 Seq 04	Joint integrity Post Engine Installation
V41BL0.033	у	SSME Encapsulation Oxid Sys ISO Test		V1294.007 Seq 04		System leak integrity check for launch ~ Mat. 1 or Weld Thru-Crack: Seal not Sealed - > Crit. 1
V41BL0.034	у	SSME Encapsulation Hot Gas Sys ISO Test		V1294.007 Seq 04		System leak integrity check for launch - Mat. 1 of Weld Thru-Crack: Seal not Sealed - > Crit. 1
V41BP0.010-A	n	E1 GO <sub>2</sub> /GCV Ext Lk Ck & Orifice Verif	V1011.04 Seq 07	V1294.002 Seq 17	V1046.005 Seq 05	Establishes leak test of all gaseous oxygen syster joints from the AFV to the orbiter interface on an each flight basis
V41AQ0.010-A	y	E1 Sensor Checkout	V1011.06 Seq 02	V1294.002 Seq 06	V1046.001 Seq 04	Planned Preflight Checkout

From table 2, development or definition of an reusable engine operations concept is traced to the SSME experience. This database was developed to link propulsion system concepts and technology candidates to the SSME operations experience. The backbone of the SSME experience is the OMRSD database. Deterministic model data are linked to the OMRSD database for each requirement. Additionally, root causes and/or OMRSD rationales are provided that allow for rapid determination of those OMRSD's affected by technology improvements or hardware configuration changes. From table 2, first row, a requirement was established for SSME weld and leak checks on the high-pressure oxidizer turbopump (HPOTP). The root cause of this requirement is a concern for weld integrity. The OMRSD number, three applicable OMI's, and an applicability column for the new launch vehicle engine are provided. It is interesting to note that this requirement was generated well after the design of the SSME and its processing when potential problems with welds were identified. This specification of postdesign requirements is likely to occur in a new launch vehicle engine as well.

#### 6. MODEL DEVELOPMENT AND RESULTS

The scope of the analysis for this document is a future launch vehicle ground operations analysis that includes shuttle-based uncertainties associated with scheduled and unscheduled maintenance. The emphasis is on propulsion systems and the specific topic is the engine which will be modeled in order to be responsive to the vehicle requirements. Of course, the engine processing is only one part of the overall vehicle processing. Interactions of the engine processing and other subsystems must be taken into account to get a proper estimate of vehicle and even engine flows. The results of this analysis reflect the impact of unscheduled processing on turnaround time in a deterministic model and on launch availability and dependability in a probabilistic model. The attributes of the maintenance activities will be limited to those supported by analysis of the STS PRACA, CAPSS, and Marshall Space Flight Center (MSFC) Propulsion Laboratory operations databases.

Given ground rules and assumptions, key processes were laid out for a fully reusable future launch vehicle engine concept. To avoid proprietary data considerations and to simplify the presentation, a roughcut engine design is assumed for this analysis. It is essentially SSME-like;<sup>20</sup> a pump-fed LO<sub>2</sub>/LH<sub>2</sub> highthrust engine with pneumatic and EMA valve control (no hydraulics) and health monitoring capabilities. The proposed launch vehicle uses three such engines with engine processing conducted in parallel. From this, a logic model associated with the flow of ground processing is developed. A 40-hr, goal-oriented engine ground flow serves as a baseline to the defined flows. Effectively, this 40-hr timeline was provided as a requirement (baseline allocation) for this model activity. Figure 13 shows the engine flows and the success-oriented timelines by processing facility. Three facilities were assumed after landing—a single processing facility with five bays and two launch pads. From figure 13, engine ground operations processes include drying; access; visual inspections; leak checks; and closeout on each engine in the processing facility and purge; flight readiness test; and launch preparation on the engine set on the pad. An unscheduled maintenance timeline is supported in parallel with the scheduled timeline. Key assumptions and ground rules to this development were 30 flights per year, a five-vehicle fleet, and 7-day missions. Others included minimal and automated operations, separate payload processing, depot maintenance every 20 missions, and automated health monitoring. Manpower assumptions included two shifts per day, 5 days per week for processing facility operations and three shifts per day, 7 days per week for all other processing.

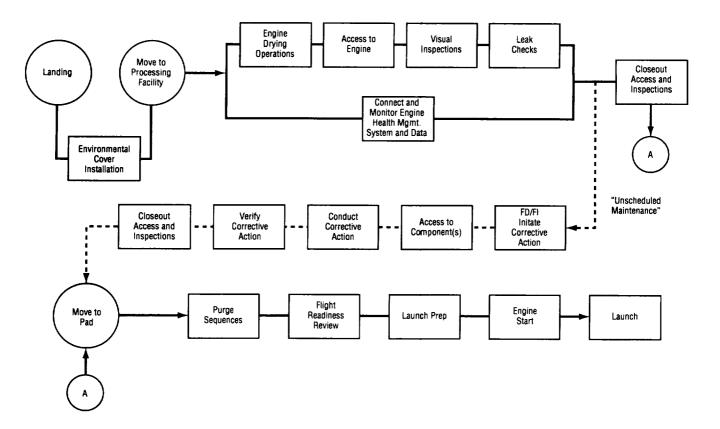


Figure 13. Engine operations processing.

#### A. Deterministic Model

An MS Project<sup>TM</sup> model was developed to reflect the processing requirements (top-level and allocated) of the engine system. From the flows defined in figure 13, processing timelines and resources required were input into the MS Project<sup>TM</sup> scheduler. The tasks were defined to three levels as subprojects. Figure 14 presents the top level to the level of detail at one of the lowest level processes defined here—that of the engine drying operation. Total duration and manpower requirements in the subprocesses of figure 14 can be rolled up to the top level in a very direct fashion. This is the allocated appropriate times and requirements for those systems within the constraint of the overall requirement, which was provided as a top-level requirement; in this case, 40-hr total for the engine. Thus, the times and resources reflect a relative allocation to the subsystems: it remains to be seen, for example, whether or not a gaseous oxygen (gox) system leak check will take the 1 hr allocated, but the 1 hr allocated to this system is consistent with the time allocated for the fuel system leak checks (1 hr). Again, this model serves as the goal-oriented model useful for allocation and comparison with the detailed engineering estimates. In the approach identified in figure 4, this is the top half—the goal-oriented model.

ID	<u> </u>	Task Na	ame	Duration (hr)	Work (Man-hr	Dec. 1			Dec. 8, 1997			5, 1997		. 22, 19	
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	9 Install Plugs/Gages/Drain 10 Activate Pneumatics/Valv				1		1		Tec						
	11 Conduct Ox. Sys. Drying F					1		4		•	Tech[4	41			
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Figure 14. Hierarchical engine model.

This type of modeling often predominates, especially early in design. With an emphasis on new ways of doing business, this goal-oriented modeling is often the only type of modeling undertaken on a program. There are several reasons for this. It can be time consuming and resource intensive to conduct a bottom-up analysis and difficult to present an unpopular result. The weakness of the goal-oriented modeling should be apparent. It often has no basis in reality. One example of how misleading goal-oriented modeling can be was that for the STS program. Early modeling predicted up to 60 flights per year with a 2-wk turnaround time,<sup>21</sup> very different from current shuttle capabilities.

Sensitivity studies of the MS Project<sup>TM</sup> model and even simple "back of the envelope" analysis can shed some light on the sensitivity of this system. For example, increasing scheduled uncertainty to 50 percent increases total duration, for what is essentially a serial flow, a proportional percentage—from 40- to 60-hr duration with personnel manhours increasing from 319 to 478.5. Concerns with meeting availability and dependability requirements increase also. However, even a 50-percent increase in scheduled processing may not be a serious impact. Adjustments in scheduled timelines or built-in holds can be included

to deal with this. Even if dependability is defined as launch within 2 days of scheduled launch, such variation is manageable—an extra 20-hr duration is still within 2 days, if there are multiple shifts per day.

Much more significant is the variation in unscheduled processing. In the baseline case, the unscheduled processing is designed to be in parallel to scheduled processing. Even this can tolerate some additional unscheduled processing before impacting overall flow. However, this assumes sufficient manpower to handle problems in parallel and that problems will occur in parallel. Such an assumption is not credible. For example, if four to six engineers are allocated to handle processing, the extra unscheduled activities cannot be conducted entirely in parallel without a schedule slip—there simply is not enough manpower. Also, if problems occur late in launch to critical path operations, there is a serial effect—problems must be resolved before any more normal launch processing can be supported. Built-in holds can also mitigate the problem of unscheduled processes, especially early in the flow. Late processes, such as pad processes, must attempt to minimize all unscheduled activity.

In this deterministic model, the unscheduled maintenance activities were added to reflect these issues. A notion of unscheduled maintenance considerations should be incorporated into the requirements allocation for accuracy sake. Table 3 lays out the SSME-based experience and the impact per OMI for this analysis. For example, from the historical SSME record, twice as much time is spent on unscheduled maintenance during the visual inspection OMI (V1011.02) than for scheduled maintenance. Table 4 presents the results of this analysis including a run with the unscheduled maintenance data. The first column of the table presents the baseline results—both clock hours and personnel manhour requirements. The second column adds in unscheduled timelines based on STS SSME experience. If the unscheduled activities are assumed to be done in parallel, the overall impact to the timeline is small. That which is not on the critical path has little impact, while adding unscheduled maintenance activities to critical path operations is realistic and has a significant impact. The impact to the overall dependability and availability metrics can also be considerable as will be seen in the next section. Keep in mind that many of the SSME OMI's have already been excluded and that the baseline processing time is allocated. The result in table 4 is more of interest in a relative sense—the duration and manhour requirements practically doubled with experience-based unscheduled maintenance included in the analysis (from 40- to 70-hr duration, 348 to 615.6 man-hour total). Further and more detailed analysis is clearly necessary.

Table 3. SSME unscheduled maintenance experience.

Task Description	OMI Number	% Additional Unscheduled Processing*
Envir. Cover Install	S0028	10
Engine Drying	V1011.01	10
Assess to Engine	V5058/V5057/V5087	10
Visual Inspections	V1011.02	200
Leak Checks	V1294.xx	100
Closeout	S1287/V5057	50
Purge Sequences	V9018.001	10
Flight Readiness Test	V1046/V5057/V9002	75
Launch Prep & Start	S0007	10

<sup>\*</sup> Per SSME Experience,1989-1994

Table 4. Goal-oriented engine operations timelines.

Task Name	40-Hr Goal-Oriented Baseline		40-Hr Baseline With Unscheduled Maint. Included (SSME-Based)*	
	Duration, hr	Man-hr	Duration, hr	Man-hr
Processing Assessment	40	348	70	615.6
<ul> <li>Landing Operations</li> </ul>	2	6	2.2	6.6
Processing Facility Operations	30	310	59	573.8
<ul><li>Engine Drying</li></ul>	3	20	3.3	22
- Engine Access	2	8	2.2	8.8
- Inspections	8	32	24	96
– Leak Checks	8	32	16	64
– HM Monitor	[20]	40	[22]	44
<ul> <li>Unscheduled Allocation</li> </ul>	[24]	144	[48]	288
- Closeout	9	34	13.5	51
Pad Operations	8	32	8.8	35.2

<sup>\* 1989-1994</sup> 

This concludes the discussion of the goal-oriented model and analysis results. Turnaround time and resource requirements have served as primary metrics to this point. Operability metrics such as availability and dependability are more appropriate to a detailed probabilistic model. The probabilistic model and its results are the topics of the next section.

#### B. Probabilistic Model

#### 1. Overview

The following analysis serves to illustrate the probabilistic approach—modeling to include uncertainty in the analysis. As in the earlier deterministic analysis, the scope of this analysis is a future engine operations analysis that includes uncertainties associated with unscheduled and scheduled maintenance. Consistent with the overall process, requirements were generated from the STS requirements list applicable to this new engine system. Engine design data were assumed for this application and use no proprietary information. Identical to the engine used for the deterministic model analysis, the future engine system is a pump-fed LH<sub>2</sub>/LO<sub>2</sub> system with EMA and pneumatic valve actuation (no hydraulics), and active health monitoring. A three-engine vehicle is also assumed for this analysis. The emphasis is on the engine processing, with the vehicle operations requirements allocated out to the engine level. The interest here is on the impact of engine scheduled and unscheduled processing on engine dependability and availability. The data used as baseline for this analysis are those of the shuttle engine system.

<sup>[]</sup> Not on critical path

# 2. Operations Concept

Given ground rules and assumptions, key processes were laid out for a fully reusable future launch vehicle concept. These are the same as those laid out for the deterministic model of the previous section with detail of depot maintenance now included. A logic model associated with the flow of ground processing was developed and figure 13 shows these engine flows by processing facility. The assumptions and ground rules are the same as in the deterministic case except for the following. Depot maintenance consists of engine removal and replacement, more detailed tests and checkout, and generally takes 30 days. Automated health monitoring is assumed, although this would only affect diagnostic and isolation time for unscheduled activities. Three vehicles may be on orbit at one time and two vehicles can be in depot maintenance at one time. The resources have been designed for minimal bottlenecks. This includes manpower, which is assumed available when and where needed, given shifting constraints. The block flows reflect periodic and depot maintenance operations that utilize parallelism and adequate manpower. For example, the engine processing for the three-engine vehicle is done in parallel. This provides a much shorter process clock time; however, manpower must be calculated accordingly. Typical engine operations include engine drying, inspection, and leak checks for the routine turnaround operations and engine removal and replacement for the depot maintenance operations. This discrete-event logic flow will be represented in a simulation model to be developed as part of this analysis. This flow will be modeled over a 20-yr lifetime. Results will be presented from a set of Monte Carlo runs.

## 3. Model Development

A computer program that supports discrete-event simulation on a personal computer was used for this analysis. This package, Extend<sup>TM</sup>, allows icon-based time and event modeling. The package is available commercially and provides ease of use in building models and in specifying output parameters. It supports probabilistic modeling and hierarchical levels of detail for complex systems.

The logic of the operations processes timelines was incorporated into the Extend™ modeling language and runs were made to analyze the parameters of interest. All simulations for this analysis were performed on a PowerMac 7600. This operations model was developed fully from Extend™ library building blocks. Figure 15 presents the top level of the ground operations modeled. The model is reflected in a hierarchy, the lowest level of detail for the processing facility, as presented earlier in figure 13. From figure 15, the processing facility with five bays (three for nominal, two for depot); the two pads; the runway; and vehicle tows are evident. The five vehicles come in as scheduled in the new vehicle block to the appropriate routine processing in the upper three bays or the depot processing in the lower two bays.

This probabilistic detailed model serves as an experience-based model outlined in the approach of figure 4 (lower half of schematic). Results from it are intended to be compared against the goal-oriented model results.

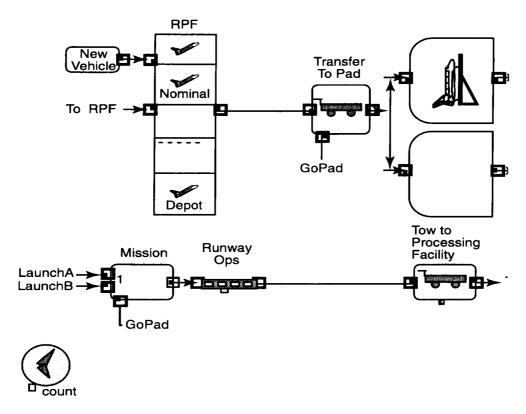


Figure 15. Extend reusable engine operations model.

#### 4. Data and Metrics for Analysis

For this analysis, the data as described in section 5 were used for model data support. As stated earlier, this database keeps track of the ground operations unscheduled and scheduled maintenance activities for SSME processing. Distributions around the scheduled and unscheduled maintenance processing are modeled with a triangular distribution, 22 selected due to its "conservative" nature. Evidence exists that for process simulation the lognormal distribution may be the most appropriate. 23,24 Such evidence also exists relative to some aerospace applications; 25,26 but without actual operational data to support this, the triangular distribution has been chosen. The triangular distribution requires a minimum, a maximum, and a mode. For this application the mode is the selected STS value, the minimum is 5 percent less than the mode, and the maximum 10 percent greater than the mode. These values were accepted during the data collection process by the system engineers as generally representative of actual shuttle engine task processing uncertainty. Extend<sup>TM</sup> supports many distribution types including the definition of a user input type. If desired, distribution types and parameters can be easily varied as part of a sensitivity study.

Metrics for this analysis include measures of merit for availability and dependability. The measure of availability deemed most suitable for this analysis is the one described earlier in the metrics discussion for process availability—nominal processing divided by total processing which includes nominal and off-nominal processing times. Off-nominal processing time includes unscheduled maintenance, queuing delays, and standdown times due to failures. This is a measure deemed more suitable to spacecraft processing systems due to the processing-intensive nature of cryogenic-fueled rocket systems and small fleet sizes.

The dependability measure is a characterization of the on-time launches. This is reflected in a probability that all vehicles are launched on time (from an engine processing point of view), measured as within 2 days of original launch date.

Requirements for engine processing were collected via the STS requirements list. There are three engines per vehicle with an engine out at liftoff capability. The only unique engine operation process proposed and not covered by STS operations is an engine-to-engine mate process which slightly expands the timelines for inspection and engine R&R.

The reliability of the engine will be modeled as will any associated standdown time due to failures to illustrate the impact of reliability on operability. Standdown time in this case is 4 mo and is a required result of any vehicle failure. A range of reliability values and their impact to the overall processing system will be presented. Appendix E presents the engine out reliability analysis and its impact on engine set reliability that is used in this analysis.

#### 5. Results

The simulation time for the model was set to 20 yr and run in a Monte Carlo environment. A relatively evenly spaced flight manifest spanning this duration served as input for the model. Vehicle flights were staggered so that, at most, three flights were on orbit and, at most, two vehicles (engine sets) would require depot maintenance at any given time.

It was apparent from back of the envelope analysis that the use of the complete shuttle engine database would present a processing timeline that was a factor of 10 over the allocated requirement. Availability for such a system is approximately 70 percent and dependability is very low unless processing start dates were backed up to allow for this extra processing. If enough time is allowed up front, any system can be made technically dependable. Implicit in the measure of dependability is an acceptable and minimal turnaround time. This is a problem in using the STS system. The inherent philosophy and conservatism associated with this manned system leads to intense processing requirements due to extensive checking and double-checking. Using shuttle experience data results in a vehicle that is only capable of five flights per year at the outset. The required processing times preclude any more. This also assumes processing manpower available to process all vehicles in parallel to support a maximum of 25 flights per year. This would result in a prohibitively expensive system. Thus, for this analysis, a decision was made to just use the "active" process conducted on the shuttle engines for this model. This excludes all vehicle setup and access time (except that explicitly allowed); all GSE setup; test setup; and of course, shuttle-specific operations. Clearly as important to the processing requirements for the future engine system is the philosophy of operation. Philosophy changes create the most significant process changes; of course, it remains to be seen whether these changes can be maintained when the actual system is in operation.

Given the above ground rule, a baseline case with no off-nominal (unscheduled maintenance) time was first established. The results for the probabilistic analysis for the operability parameters are presented in table 5. This turnaround baseline required, on average, 109.6 hr per flight. When adjusting for manpower shifting, this translates into just over a 6-day turnaround. The dependability measure assumes launch on time if launch occurs within 2 days of the original scheduled data. This system is appropriately rated at 100 percent for both availability and dependability. Without unscheduled processing time, the only

uncertainty in this system is in normal processing and this is not enough to affect on-time launch. It is interesting to note that the original goal for the turnaround of the engine system as presented in the deterministic model was 40 hr. Even with extensive and optimistic ground rules, the projected turnaround is over twice that without considering any unscheduled processing. Extra manpower may make up some of the difference but this also raises the cost to the processing system. Clearly, the original goal must be adjusted to be more realistic.

Case	Availability (%)	Dependability (%)
Full-up STS	70	Low (Assumption Dependent)
Active Processes Only (No Unscheduled)	100	100
Active With STS Unscheduled	82	0
Active With 25% of STS Unscheduled	94	78

Table 5. Results of probabilistic analysis.

When the shuttle-based, off-nominal times were incorporated into the model as reflected in table 5, the turnaround increased to an average of 171.5 hr which translates into a 12-day turnaround (a weekend added since processing facility time goes past 1 wk). With only 6 days allowed for turnaround time with a 2-day buffer, the dependability of this system is zero. Availability of this system is at 82 percent.

It is reasonable to assume that improvements in unscheduled processing and hardware will result in something significantly better than for the shuttle. From table 5, the case where 25 percent of the shuttle unscheduled processing is assumed, the dependability is at 78 percent and the availability at 94 percent. Improvement to 10 percent of shuttle unscheduled processing improves the measures to 100 percent and 96 percent, respectively. The general relationships of process time, dependability, and availability for this system are presented in figure 16. A typical requirement (95 percent) for availability and dependability is also included in this figure. Availability varies from 100 to 82 percent, based upon the amount of unscheduled processing time. Dependability displays a unique shape—almost a step function. Only between 23 and 27 percent of STS unscheduled process time is any variation evident. This range is reflective of the variation in nominal and off-nominal processing. As such, dependability is a very sensitive measure. First, it is sensitive to the time allowed for processing—in this case, 6 days. Also, it is sensitive to the buffer amount; amount of uncertainty; and staffing schedules. Dependability can be improved by an early processing start or by the use of timing control mechanisms such as built-in holds. It is interesting to note that, traditionally, engine processing delays are not key to the vehicle launch delays and dependability. Weather is the predominant cause of vehicle launch delays.

Other typical results from a discrete event simulation model include resource estimates of interest such as facility utilization rates, manpower usage, and queuing delays. In order to identify areas of improvement for operations, a Monte Carlo analysis of each process was performed by reducing the unscheduled maintenance from the shuttle-based percentage to a 10-percent target. Total manhours, cost per flow, and launch delay time per flight were used to provide a quantifiable measure of improvement. The results from these analyses are shown in table 7 for each engine task in the current processing flow.

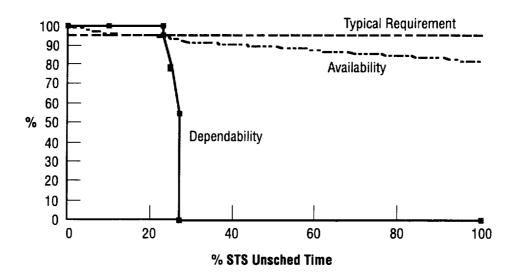


Figure 16. Operability measures by process time.

# 6. Effect of Uncertainty

Table 6 presents the impact of the incorporation of uncertainty in the model. As discussed earlier, the purpose of modeling this uncertainty is to provide for a more realistic model. The hours presented are the total for the system over the 20-yr period (600 flights). The uncertainty in this case has little impact on the availability measure, given that availability is a ratio of values, both changing in similar fashion. In this case, the impact is small since the processes modeled have relatively low uncertainty in both scheduled and unscheduled activities. Also, consistent with earlier conclusions, the dependability measure shows a high sensitivity to the amount of uncertainty. Indeed the use of the maximum amount of uncertainty for the case here drops this value to zero. Upon further analysis, this was determined to be an effect of processing facility operation being extended past 5 days, resulting in the addition of a weekend to the processing time. These two events were enough to push the launch time past the 2-day buffer allowed. The dependability value is controllable to a large extent through the use of different ground rules, built-in holds, earlier start dates, or additional manpower.

	• •				
Case	Sched Hr	Unsched Hr	Avail (%)	Dep (%)	
25% of STS Unscheduled Mode	166,460	11,482	93.5	78	
25% — Min	162,348	10,764	93.8	95	
25% — Max	171.552	12,402	93.2	٥	

Table 6. Probabilistic model uncertainty impact.

## 7. Reliability Impacts

When a measure of reliability is added to the model, impacts to operability are apparent. In this case, reliability is measured relative to catastrophic failure of the engine, and catastrophic failure of any engine leads to failure of the vehicle. The ground rule at the outset was that the system went into standdown of 4 mo after a failure in order to diagnose, isolate, redesign, or mitigate the problem causing the failure. The reliability impact of lost launches is presented in figure 17. Besides the failures, launches for the next

4 mo are delayed. Out of the 600 launches (rescheduled now over a longer period of time), 126 were canceled given an engine reliability of 0.95. For a reliability of 0.999, the number of lost launches is 1.8. Clearly, a reliability value much lower that 0.999 would be unacceptable to a launch system such as this one. Certain vehicle characteristics mitigate these failures (holddown, engine out), but the engines must be very robust for consistent acceptable operability scores. The relationship of reliability, dependability, and availability of this system as generated from the Extend<sup>TM</sup> model runs is presented in figure 18. The reliability estimates used for this analysis were as derived in the analysis of table 21 for the engine out at liftoff and catastrophic failure probability of 0.1 case. Clearly, reliability is the single biggest determinant of the operability of the system.

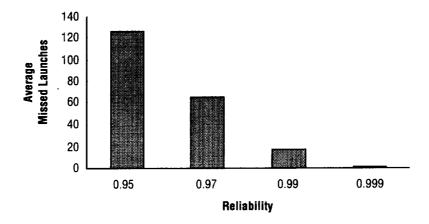


Figure 17. Impact of reliability on operability.

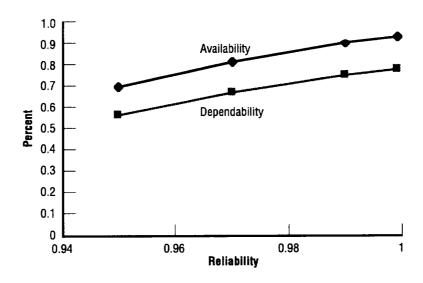


Figure 18. Operability metrics by reliability.

These results indicate the impact of scheduled and unscheduled processing and reliability on the launch system. Values of acceptable availability and dependability requirements would likely be around 95 percent. Considerable improvements in traditional spacecraft engine processing and design are necessary to meet this requirement.

These results indicate a potential manhour cost savings of approximately \$115.3K per flight along with a 7.4-hr reduction in the launch delay for the engine set modeled in this flow. The shuttle manpower data were used for this analysis. Figure 19 provides a graphical view of the manhour cost reductions and launch delay reductions for engine processing. While potential reductions are greatest in earlier processes (e.g., visual inspections), it is important to note that later processes may be more critical (e.g., pad activities). Timing controls such as built-in holds will be more effective earlier in the process flow. There is less opportunity for controlling delays late in launch.

Table 7. Engine processing manhours and launch delay reduction.

Process Description	Process MHRS (Sched)	Process MHRS (Total)	Process MHRS Cost- 3-Engine Set (\$K)	Target Cost Reduction (\$K)	Launch Delay Reduction (Hr)
Engine Drying	154	169	20.2	1.7	0.03
Engine Access	20	22	2.6	0.2	0.05
Visual Inspections	374	1,120	134.4	80.7	1.6
Leak Checks	216	432	51.8	23.4	2.4
Closeout Access	140	210	25.2	7.6	1.2
Engine Purge	52	57	6.8	0.2	0.8
Flight Readiness Test	52	90	10.8	1.4	0.5
Launch Preparation	40	44	5.3	0.1	0.8

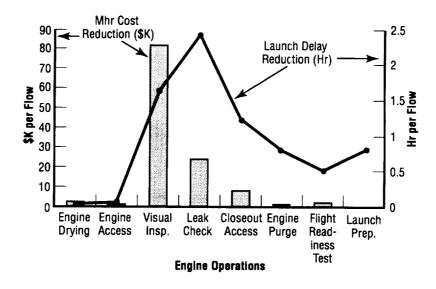


Figure 19. Engine operations manhours/cost analysis.

By using the shuttle-based results and the process target results, a relationship between percent nominal processing and clock hours or manhour cost can be determined for each process analyzed. This type of relationship provides a means to estimate how much improvement is needed to reduce the manhour cost of a given process to a specified target value, and where the improvements are most needed.

## 7. CONCLUSIONS

Deterministic and probabilistic operations models of engine processing flows have been constructed to illustrate the methodology defined in this document. The goal was to select appropriate metrics, develop a model, and conduct an appropriate design operations analysis. This supports design trade studies where operations will be considered equally with performance analyses. Traditionally, this has been a serious shortcoming of disciplines such as design operations. It has not been understood how to conduct such an analysis and what measures of merit to use. This analysis presents such an approach and applies it to a future engine concept. These models support trade and sensitivity studies allowing users to investigate "what if" scenarios to support design decisions. With the availability and dependability measures, it provides a means to quantitatively analyze scheduled and unscheduled maintenance activities for operations analysis.

The applications of this approach illustrate the traditional outcome in aerospace launch vehicle operations modeling. The difference between processing goals and initial historical-based operations estimates is large. This is at least in part due to the lack of good and accepted operations modeling techniques which use well-understood and interpretable metrics. The approach described here attempts to correct this problem by offering a rigorous process and good baseline data to identify operations concerns.

The results presented here represent a first iteration in an operations analysis process outlined in figure 4 for a hypothetical engine concept. Deterministic, goal-oriented modeling provides a top view of the requirements and allocations. The bottom-up, probabilistic analysis provides the operations processing estimates to compare against the goals and requirements. The first iteration involved the use of the STS engine (SSME) experience base. Further iterations will adjust this baseline to better estimates based upon actual design decisions. All specifications of processing are subject to requirements traceability via the STS requirements database.

Engine system scheduled and unscheduled maintenance impacts in the proposed launch vehicle flows have been identified. Critical path processes will have the greatest impact on launch delay. It is interesting to note that noncritical path processes defined in the initial operations concept may end up as critical path processes once an incidence of historical unscheduled maintenance activities is considered. From the results it is clear that the single biggest determinant of operability measures is reliability. While hardware reliability improvements are critical to improving operability, these results also point to improvements in corrective maintenance processing activities as critical to improved turnaround times and operability measures for future launch systems.

## **APPENDIX A—Engine Operations Requirements Database**

Table 8 presents SSME operations requirements (OMRSD's) and other pertinent information to support definition and traceability for future engine requirements.

Table 8. Engine requirements database.

OMRS B MUMBER	OMPSO DESCRIPTION (V41 FILE III DATED 9/15/96)	OMRSD EFFECTIVITY	Companent	OPF ORM's	ENGINE SHOP	VAR/PAD OMES	OTHER ONI'S	AT ONI'S	SUBSYSTEM CODE	OMRED RATIONALE/ROOT CAUSES	Real Cause Categories
V418L0.050	BBME WELD 22 & 24 LEAK CHECK	PKSC, NRAT	'нРотР	V1011.06 Seq 07	V1294 007 Seq 04	V1046 003 Seq 07		•	CODE	Due to poor processing, HPCTP balance cavity standoff welds are leak checked No teaks ever verified, but lack of weld penetration up to 90% has been found on these welds	Aft Compartment overpressurization
41 BLO 080-A	E1 HPOTP PLUG WELD LEAK CHECK	PKSC NRAT	неоте	V1011 05 6eq 09	V1294 004 Seq 04	V1046.004 Seq 04	V1294 005 6eq 07			Standorfs have been suspected of tending and caused neturn to Plug weld leak occurred on a unit Concern own these wolds lesions either Good-leikum/Hot gas into boattad therefore all	Aft Compartment overpressurreation
41AXD 020-A	E1 LO2 FEED (JOHNT Q1) UF LK CK	ER PR DMDP	Lines/Ducts	V1011.05 Seq 07		V1046 003 Seg 05			DUCTS	external plug weds on the housing are checked  Ensure joint integrity of LPOTP to pump met ducting after	Table 2
1 AXIO 0210-8	E1 LH2 FEED (JOINT F1) UF LIK CK	ER, PR, OMDP	Lines/Ducts	V1011 05 Seq 06		V1046 002 Seq 04			DUCTS	engine is installed  Verify pump intel joint integrity after installing the LPETP	Aft Compartment overpressurization
1AX0 020-C	E1 GH2 PREBS (JOINT P9.3) UF LK CK	ER, PR, OMOP	Lines/Ducts	V1011 05 Sec 09		V1046 004 Seq 04			DUCTS	Joint Integrity Post Engine Installation	Aft Compartment overpressurization
AX0.020-D	E1 LO2 BLEED (JOHNT 015) UF LK CK	ER, PR, OMDP	Lines/Ducts	V1011 05 Seq 07		V1046 003 Seq 05			DUCTS	Joint Integrity Post Engine Installation	Aft Compertment overpressurization
1AX0 020 E	E1 LH2 BLEED (JOINT F4.3) UF LK CK	ER, PR, OMOP	Lines/Ducts	V1011 05 Beq 05		V1045.002 Seq 04			DUCTE	Joint Integrity Post Engine Installation	Aft Compertment overpressurization
1 <b>AXO 020</b> -F	E1 HELIUM (JOINT P1) I/F LIK CK	ER, PR, OMOP	Lines/Ducts	V1011 05 8eq 12		V1046.001 Seq 05	V1046 006 Seq 04		DUCTS	Joint Integrity Post Engine Installation	Aft Compartment overpressurization
1A)00.020-G	E1 GM2 (JOHNT N1) UF LIK CK	ER, PR, OMDP	Lines/Ducts		•	V1149 Seq 15	V1046 006 Seq 03		DUCTS	Joint Integrity Post Engine Installation	Aft Compartment overpressurization
1AX0.020-H	E1 HYD - PRESS (JOINT H1) LIF LK CK	ER, PR, OMDP	Lines/Ducts		V5E17 Seq 09		V5E18	V9002 06 Seq 05	DUCTS	- · · · · · · · · · · · · · · · · · · ·	Aft Compartment overpressurization
41AX0.020-1	E1 HYD - RETURN (JOINT H17) UF LK CK	ER, PR, OMDP	Lines/Ducts	:	V5E17 Seg 09		V5E18	V9002 06 Seq 05	DUCTS	Joint Integrity Post Engine Installation	Aft Compartment overpressurization
11AXX 050-A	E1 GOZ ORB/68ME INTERFACE FLANGE	A, ER	Lines/Ducts		·	V1046 005 Seg 05	*		DUCTS	Joint Integrity Post Engine Installation	Aft Compartment overpressurization
41BL0.031	LEAK CHECK BBME ENCAPSULATION POWER HD LEAK	EKSC & ER	Powerhead	•	V1294 007 Seq 04					Joint Integrity Post Engine Installation	Alt Compartment overpressurization
41BL0 032	BSME ENCAPBULATION FUEL 8YS 180	'F	System		V1294 007 Seq 04				ENGINE	System leak integrity check for launch - Mat 1 or Weld Thru- Crack; Seal not Seated -> Crtt. 1	Aft Compartment overpressurization
4181.0 033	TEST SSME-ENCAPSULATION OXID SYS ISO	F	System		V1294.007 Sec 04				ENGINE	Bystem leak Integrity check for launch - Mat. I or Weld Thru- Crack, Seal not Seated -> Crit. 1	Aft Compartment overpressurization
418L0.034	TEST SEME ENCAPSULATION HOT GAS SYS 180	· F	System		V1294 007 Sec 04				ENGINE	System leak Integrity check for launch - Mat 1 or Weld Thru- Crack, Seal not Sealed -> Crit 1	Aft Compartment overpressurization
18P0.010-A	TEST E1 GOZ/GCV EXT LX CK & ORIFICE VERIF	EKEC, 1	Valves	V1011 04 Sec 07	V1294 002 Seq 17	V1046 005 Sea 05			ENGINE	System leak Integrity check for launch - Mat. I or Weld Thru- Crack, Seal not Seated -> Crit. 1	Aft Compartment overpressurization
AQ0.010-A	E1 SENSOR CHECKOUT	EKBC ER LAU	Instrumentation	V1011 06 Seq 02	V1294 002 Seq 05	,	V1294 006 Seq 05			Establishes leak test of all gameous caygen system joints from the AFV to the orbiter interface on an each flight basis.	Aft Compartment overpressurization
1AU0.013-A	E1 OPERATIONAL INSTRUMENTATION VERIFICATION	A, ER	Instrumentation	47011 00 and 02	A1584 OUS Sed no	V1045.001 Seq 04 V1045.001 Seq 04		V9001VL4 Seq 02 V9001VL4 Seq 02	AVIONICS AVIONICS	Planned Preflight Checkout Instrumentation integrity checkout	Erroneous shutdown, loss of vehic
BU0.250-A	E1 SENSOR IR VERHICATIONS	EKBC, LRU	Instrumentation	V1011 02 Seq 07						• •	Erroneous shutdown, loss of vehic
18PO 020-A	E1 HEX COIL LEAK TEST	A, EKSC, PLRU	HEX	V1011.04 Seq 02	V1294 003 Seq 03	V1046.005 Seq 06			HEX	Functional check of each turbine discharge temp Mat. I (stringer) or Weld Thru-Crack, HPOTP Installation Impact	Erroneous shutdown, loss of vehicl Fire, Uncontained engine failure
418P0.030	86ME HEX COIL PROOF TEST	PLRU	HEX	V1011.04 Seq 03	V1294.003 Seq 04	V1046.005 Beq 07			HEX	Hole -> HG to Tank, Crit 1 Met. I (stringer) or Weld Thru-Crack; HPGTP Installation Impact	Fire, Uncontained engine failure
41 BU0.086	HEX EDDY CURRENT INSPECTIONS (TIME & CYCLE)	π	HEX	V1011.02 Seq 11					HEX	Hole -> HG to Tank; Crit. 1 Thin Walls from Bracket Wear, Manuf -> Thru-Crack, HG	Fire. Uncombined engine failure
41BUO 115	HEAT EXCHANGER INSPECTION	тс	HEX	•	V5E02 Sec 14				HEX	Limitage to Tank, Crit. 1  Yestble Impact Demage, Bracket Wear -> Thru-Crack -> HG to	Fire, Uncontained engine failure
41 BUO 125	HEX VISUAL INSPECTION	PLRU	HEX		V5E02 Seq 12					Tank, Crit 1; Turn. Vane Cracks -> Loss of Vane Impact Mi Post -> Damage or Crit 1.	
1BU0.075-A	E1 HPETP INTERNAL INSPECTION	PK6C	нретр	V1011 02 Seq 08					HEX TURROPUMPS	HPOTP Installation Impact Hole >> HG to Tank; Crit 1  Verify no inlet or discharge sheet metal cracking; no nozzle	Fire, Uncontained engine failure
1800.079									1011001 0411 9	cracking or erosion, no blade cracking, platform cracking, or erosion; no fishmouth seal cracking or missing pieces; no	Fire, Uncontained engine failure
1900.070	HPFTP FIRST STAGE BLADE 22X INSPECTION	TC, DCE	HPFTP		V5E06 Seq 14				TURBOPUMPS	bellows shield cracking. (All inspections completed with Verify no blade cracking due to previous occurrences of airfoli	Fire, Uncontained engine failure
1900.080 1800.087	HPFTP TURBINE INSPECTION (TIME & CYCLE)	PKSC	нетр		V5E06 8eq 14				TURBOPUMPS	cracking Varify no inlet or discharge sheet metal cracking including weld 450 and the turning vanes, no nozzle cracking or erosion, no blade cracking, statform cracking, or erosion, no fethmouth	Fire, Uncontained engine failure
	HPFTP BELLOWS HEIGHT VERIF	PLRU	НРЕТР		V5E06 08SU 2				TURBOPUMPS	seal cracking or missing pieces; no bellows shield cracking yes.  Verify bellows height adequate to provide proper preload on the bellows at installation. Incorporated as a result of a previous	Fire, Uncontained engine failure
1 CBO 060-A	E1 HPFTP TURBINE BEARING DRYING	EKBC	нетте	V1011.01 Seq 03		V9018 002 Seq 04	V1038VL2 Seg 07		TURBOPUMPS	failure of the bellows.  Ensure all moisture is removed from the bearing ares after a test/flight.	Fire, Uncontained engine failure

Table 8. Engine requirements database (Continued).

OMRSD NUMBER	OMRSD DESCRIPTION (V41 FILE III DATED 9/15/95)	OMRSD EFFECTIVITY	Component	OPF OMI's	ENGINE SHOP OMI's	VAB/PAD OMI's	OTHER OMPs	RT OMI's	SUBSYSTEM	OMRSD RATIONALE/ROOT CAUSES	Root Cause Categori
	E1 LPFD OVALITY CHECK	F	Lines/Ducts	V1011.02 Seq 10			V9018.002 Seq 10		DUCTS	Contingency test performed only when the LPFD helium berrier system has been damaged. Object is to detect potential duct collapse or separation from the layer of insulation by measuring the roundness of the duct.	Fire, Uncontained engine fai
/41BU0.400	PERFORM LPFD XRAY INSPECTION	F	Lines/Ducts	TBD					DUCTS	Contingency regnt preformed only when the ovality check indicates that some damage or collepse has occurred in the LPFD. The cross section is X-rayed in an attempt to verify	Fire, Uncontained engine fai
41850.050	HPOTP/AT TORQUE TEST	EKŞÇ, RI, PLRU	HPOTP	V1011.03 Seq 06	V5E02 Seq 25				TURBOPUMPS	Replaced by V41BS0.040-A	Fire, Uncontained engine to
/41BS0.055	HPOTP/AT INVESTIGATIVE TORQUE	F	HPOTP	V1011.03 Seq 05	V5E02 Seq 25				TURBOPUMPS	Replaced by V41BS0.042	Fire, Uncontained engine fa
418U0.405		DCE	Lines/Ducts	ТВО					DUCTS	Performed to insure LPFD structural integrity. Inspection is performed if post flight data evaluation reveals HPFTP unacceptable synchronous frequencies.	Fire, Uncontained engine fai
18U0.065-A	E1 ATD SLOCK WI HPOTP INTERNAL INSPECTION	PKSC, NRAT	НРОТР	V1011.02 Seq 08					TURBOPUMPS	No HPOTP/AT internal inspections were made during certification. Inspections of the turbine, mainstage pump and PBP intets, and all three bearings have been added only because the inspections aren't time consuming and because	
41BS0.010-A	E1 LPFTP TORQUE TEST	A, RI, PSI, ER, PLRU	LPFTP	V1011.03 Seq 04	•				TURBOPUMPS	Verify rotor is free to rotate prior to testing	Fire, Uncontained engine fa
/418U0.127	HPOTP/AT PBP TIEBOLT LOCK	F	HPOTP	V1011.03	,				TURBOPUMPS		Fire, Uncontained engine fa
41BU0.12B	HPOTP/AT CONTAMINATION INSPECTION	A, PKSC	HPOTP	V1011.07 Seq 77					TURBOPUMPS		Fire, Uncontained engine fa
/41CB0.085		PKSC	HPOTP	V1011.01 Seq 03	V1294.008 Seq 04	V9018.002 Seq 04			TURBOPUMPS	Verify all moisture is removed from the bearing area after a	Fire, Uncontained engine fa
	DRYING									test/flight.	
/41BS0.011	LPFTP INVESTIGATIVE TORQUE	F	LPFTP	V1011.03 Seq 04					TURBOPUMPS	Investigative torque check if the specification limits are exceeded - torque check failure generally lift-off seal binding or laby seal - copper plating rub	Fire, Uncontained engine fa
41BS0.030-A	E1 LPOTP TORQUE TEST	A, RI, PSI, ER, PLRU	LPOTP	V1011.03 Seq 05	V5E23				TURBOPUMPS	Done to ensure rotor is not bound up prior to start — concern over contamination if high and also start characteristics if rotor is slow to spin — contamination has been found that bound the rotor and bearing wind-up can also routinely causes failure of	Fire, Uncontained engine fa
V41BS0.031	LPOTP INVESTIGATIVE TORQUE	F	LPOTP	V1011.03 Sec 05					TURBOPUMPS	Performed to free the rotor if possible - done only if needed -	Fire. Uncontained engine fa
41BS0.032-A 41BR0.040-A	E1 LPOTP SHAFT TRAVEL	A, ER, PLRU DLP	LPOTP Main Injector	V1011.03 Seq 05 V1011.02 Seq 08	V5E23				TURBOPUMPS COMBUSTION	must make torque return to normal value or pump is removed.  Bearing weer on LPOTP thrust bearing must be monitored.  LOX Post integrity check - Impected or Defected Post Plugged.	Fire, Uncontained engine fa
	DECAY								COMBUSTION	& Plug Demaged > Loss of Plug, Increase Damage to Post > Loss of Post, Crit. 1  Under Place (cant) > Flow Emission MCC H/G Wall > Receir or	Fire Uncontained engine fa
41BU0.034-A	E1 MAIN INJECTOR LOX POST BIASING	EKSC	Main Injector	V1011.02 Seq 04					COMBOSTION	Crit. 1 Leuk; Under Biss → Combustion Performance Loss	rire, Undurtained engine is
/418Q0.165	MCC ISOLATION LEAK TEST	F	MCC		V1294.003 Seq 06				COMBUSTION	Mat.1 Debond @ Liner Aft → Repeir, UAI Performance Loss; Crit 3 to Crit 1 if incresse.	Fire, Uncontained engine fa
1BQ0.240-A		EKSC, LRU	MCC		V1294.003 Seq 05					Burst Disphragm Damage, Internal Liner To Structure Thru-	Fire, Uncontained engine for
18U0.031-A	E1 MCC BONDLINE ULTRASONIC INSPECTION MCC INJECTOR INSPECTION WITH HPFTP	EKSC	MCC	V1011.02 Seq 05	V5E06 Seq 12		V1038VL2 Seq 08		COMBUSTION	Internal Debonds -> Emplosion, Crit 1; External Leak, UAI to Crit 1 Inspect when HPFTP Removed	Fire, Uncontained engine fa
*1000.001-A	REMOVED	reno								,	-
11BU0.082-A	MCC INJECTOR INSPECTION WITH HPOTP REMOVED E1 THRUST CHAMBER NOZZLE LEAK TEST		MCC/Nozzle	V1011.05 Seq 09	V5E02 Seq 14 V1294.011 Seq 06	V1046.004 Seq 04	V1038VL2 Seq 08		COMBUSTION	Inspect when HPOTP Removed  Cold or Hot Well Thru-Crack; Degraded Liner Met.'l or Bebond-	Fire, Uncontained engine for
41BQ0.160-A	ET (HRUS) CHAMBER NOZZLE LEAK TEST	ENSC	NCC/NOZZIO	VIOTILUS SAN UN	V1254.011 344 00	¥ 1040,004 38Q 04	V1036V12 384 00			> Rapair; UAI Performance Loss; Crit 3 to Crit 1 if increese. If no action required then data used to adjust engine performance predictions	•
418Q0.200-A V418Q0.167	E1 MCC TO NOZZLE SEAL LEAK TEST SSME NOZZLE ENCAPSULATION LEAK TEST	EKSC, LRU, I F	MCC/Nozzie Nozzie	V1011.05 Seq 08	V1294.004 Seq 03 V1294.010 Seq 03	V1046.004 Seq 08			COMBUSTION	G-15 Seel Thermal Degradation -> Aft Compartment Leek, Crit. Cold or Hot Well Thru-Creck like Crown Erosion, Brazeless Tube Ends -> Reposit: UAI Performance Loss: Crit 3 to Crit 1 if	Fire, Uncontained engine fa Fire, Uncontained engine fa
/418U0.353-D	NOZZLE VISUAL INSPECTION	EKSC	Nozzle	V1011.02 Seq 05			V1038VL2 Seq 08		COMBUSTION	Erosed Tube Crowns -> Leekage up to Crit 1; Tube Bulges -> Trip HG Flow or Shock Weve -> Dyn. Destruction NZ, Crit 1; Reserby Anneeling -> Met. Degradation, Burel -> Crit. 1	Fire, Uncontained engine for
/41BU0.353-E	NOZZLE PARENT METAL DISCOLORATION INSPECTION	EKSC	Nozzłe	V1011.02 Seq 05			V1038VL2 Seq 08		COMBUSTION	Erosed Tube Crowns → Leskage up to Crit 1; Tube Bulges → Trip HG Flow or Shock Wave → Dyn. Destruction NZ, Crit 1; Reenty Annealing → Met 1 Degradation, Burst → Crit. 1	Fire, Uncontained engine for
/41RLIO 081.0	FLIFT SIDE TRANSFER TUBE INSPECTION	PLRU	Powerhead		V5E06 Seq 12	•	1		COMBUSTION	Inspect when HPFTP Removed	Fire, Uncontained engine for
418U0.082-B	OXIDIZER SIDE TRANSFER TUBE INSPECTION	PLRU	Powerhead		V5E02 Seq 14				COMBUSTION	Inspect when HPOTP Removed	Fire, Uncontained engine f
418U0.081-C	FUEL PREBURNER INSPECTION	PLRU	Prebumer		V5E06 Seq 12				COMBUSTION	Inspect when HPFTP Removed	Fire, Uncontained engine f
41BU0.081-D	FPB LINER INSPECTION	PLRU	Preburner		V5E06 Seq 12	•			COMBUSTION	Inspect when HPFTP Removed	Fire, Uncontained engine f
418U0 082-C	OXIDIZER PREBURNER INSPECTION	PLRU	Preburner		V5E02 Seq 14	•			COMBUSTION	Inspect when HPOTP Removed	Fire, Uncontained engine I
41BU0.082-D	OPB I INER INSPECTION	PLRU	Preburner		V5E02 Seq 14				COMBUSTION	Inspect when HPOTP Removed	Fire, Uncontained engine
/41BU0.085	OXID P/B INJECTOR ELEMENT INSP	TC, MSP	Preburner		V5E02 Seq 14				COMBUSTION	Demeged Poets Pinned, Loss of Pins → Increese Demage to Poet → Loss of Poet into Turbine, Crit. 1 or Internal Leakage ->	Fire, Uncontained engine
V41BU0.086	SSME FUEL P/B INJECTOR ELEMENT INSP (IF ONE OR MORE PINS FOUND MISSING)	MSP	Preburner	TBO					COMBUSTION	Overheat Turbine, Crit. 1 Demaged Posts Pinned, Loss of Pine -> Increase Demage to Post -> Plug Post & Use or Loss of Post into Turbine, Crit. 1 or Internal Leakage Overheat Turbine, Crit. 1	Fire, Uncontained engine f
V41BU0.106	FPB INJECTOR OXID POSTS INSP	тс	Prebumer		V5E06 Seq 12	•			COMBUSTION	Penned Desix Pinned, Loss of Pins > Increase Damage to Post > Plug Post & Use or Loss of Post into Turbine, Crit. 1 or Internal Leakage Overheat Turbine, Crit. 1	Fire, Uncontained engine f
V41BU0.570	FPB DIFFUSER INSPECTION	DCE	Preburner	тво					COMBUSTION	Contingency regnt performed to inspect for cracks in FPB diffuser. This regnt will be invoked only if data evaluation of HPFTP turbine discharge temp deems it necessary.	Fire, Uncontained engine f
V418U0.032	OPB FACEPLATE FLATNESS CHECKS	DCE	Preburner						COMBUSTION	Integrity check efter "POP" - "POP" Demage , Bowing Indication of Braze Cracks -> Loss of Element Into Turbine, Crit 1; of Internal Leakage -> Overheat Turbine, Crit. 1	Fire, Uncontained engine for
/41BU0.040-A	E1 COMPONENTS INTERNAL INSPECTION	EKSC	System	V1011.02 Seq 06						Boroscope inspection of accessible engine areas without diseasembly	Fire, Uncontained engine for
V41CB0.020-A	E1 ENVIR CLOSURE INSTALLATION	EKSC	System	S0026 Seq 19		!	S0026			Insure that LPFD helium berrier system is functional to preclude cryopumping in the event of a launch scrub which can lead to a collapse of the duct.	Fire, Uncontained engine for
V41BQ0.080	RN OVERRIDE SEALS LEAK TEST (TIME & CYCLE)		Valves	TBO						Penodic (every 10 starts). To verify that the RfV sheft seets meitain override opening pressure within the RfV. No LOX in HEX prestart - Crit 1	Fire, Uncontained engine for
V41BQ0,100	AFV SEAT AND SHAFT SEAL LEAKAGE	A, GP	Valves	V1011.04 Seq 07		V1046.005 Seq 05					Fire, Uncontained engine f
V41BQ0.101	AFV SHAFT AND SEAT ISOLATION E1 PROP VALVE ACT PNEU SEAL LEAK	F EKSC, LRU	Valves	V1011.04 Seq 07 V1011.05 Seq 12	V1294.002 Sec 10	V1046.005 Seq 05 V1046.006 Seq 04	V1011.06 Seq 03	V5E17 Seq 09		Isolation check if the V41BQ0.100 leakage limits are exceeded.  Valve/Seal Leakage - LRU Integrity Check.	Fire, Uncontained engine f Fire, Uncontained engine t
V41BQ0.170-A		LAGO, LAG			* (200.002 00d 10			torn on had no			
V41BQ0.171	PROP VALVE ACT PNEU SEAL ISO TEST		Valves	TBD						leolation check if the V41BQ0.170-A leakage limits are	Fire, Uncontained engine f

Table 8. Engine requirements database (Continued).

ONRSD	OMRSO DESCRIPTION (V41 FILE III DATED 9/15/95)	OMRSD	Component	OPF OMFs	ENGINE SHOP	VAB/PAD OM's	OTHER OM's	RT OME's	SUBSYSTEM	OMRSD RATIONALE/ROOT CAUSES	Root Cause Categories
V418U0.220-A	AFV FILTER INSPECTIONS	EFFECTIVITY	Valves	V1011.04 POSU 5	<b>ORF's</b> V1294.002 POSU 6	V1046.005 POSU 2			CODE		-
V418U0.220-D	AFV FILTER REPLACEMENT	A	Valves	V1011.04 Seq 07		V1046.005 Seq 05	V5005 POSU 3	V5067 Tesk 28		Contamination check to verify that filter is not plugged which could lead to a collepse of the HEX.	Fire, Uncontained engine feilure
V418Q0.010-A	E1 FUEL TP LICHMFV BALL SEAL LK TEST	EKSC. ER	HPETP, LPETP, MEV	V1011.05 Seq 05	V1294.007 Seq 03	V1046.002 Seq 03	13331 030 3	V3007 1994 28		Contemination check to verify that filter is not plugged which could lead to a colleges of the HEX.  Verify no LPFTP or HPFTP INt-off seel carbon hose leakage or	Fire, Uncontained engine failure Hazardove gee buildup
V418Q0.011 V418Q0.020-A	FUEL TP LIGHTY SEALS ISOLATION TEST		HPETP, LPETP, MEV	TBO						mein fuel valve ball seel leekage. (Fuel system pressurtzed, measure leekage into hot gas system) leoleton check if the V41BQ0.010-A leekage limits are	
		EKSC	HPETP, LPETP, MEV	V1011.05 Seq 05	V1294.005 Seq 03	V1046.002 Seq 06				Verify no LPFTP or HPFTP large diameter secondary seel leekage or Naflex or MFV isakage (Fuel system pressurized.	Hazardous ges buildup Hazardous ges buildup
V418Q0.021 V418Q0.050-A		F EKSC, LRU	HPFTP, LPFTP, MFV System	V1011.05 Seq 05 V1011.05 Seq 09	V1294.005 Seq 03 V1294.005 Seq 05	V1046.002 Seq 06 V1046.004 Seq 04				measure leakage out of the fuel component drain) leolation check if the V41BQ0.020-A leakage limits are Verify no LPFTP or HPFTP small diameter secondary seel	Hezardous gas buildup Hazardous gas buildup
V41BS0.043-6 V41BS0.043-C	E2 HPOTP IMPELLER LOCK VERIF E3 HPOTP IMPELLER LOCK VERIF	PKSC, PLRU, NRAT PKSC, PLRU, NRAT		V1011.03 Seq 06	V5E02 Seq 25 V5E02 Seq 25				TURBOPUMPS	leakage or other system leakages (Hot pas system pressurized, measure leakage out of the fuel component drain)	•
V419Q0.051 V41BQ0.052-A	SSME HOT GAS SYS SEAL LK ISO TEST E1 SSME COMB HOT GAS TO FUEL SYS	F PKSC	System	TBD V1011.06 Sec 09					TURBOPUMPS	lectation check if the V41BQ0.050-A leakage limits are	Hazardous gas buildup
	REVLKCK	rnac	System	V1011.05 Seq 09	V1294.005 Seq 06	V1046.004 Seq 04				Verify no reverse LPFTP or HPFTP carbon nose leakage (Hot ges system pressurized, measure leakage into fuel system) incorporated when the pump end to turbine end leak check did	Hazardous gas buildup
V418Q0.063 V418Q0.030-A	SSME HOT GAS REVERSE ISO LK CK E1 FUEL BLEED VALVE SEAT LEAK TEST	F FYEC I BILL	System	ТВО						not detect existing carbon nose leakage. Isolation check if the V41BQ0.052-A leakage limits are	Hazardous gas buildup
V418U0.030-B	E2 COMPONENTS EXTERNAL INSPECTION	EKSC	Valves	V1011.05 Seq 04 V1011.02 Seq 04	V1294.005 Seq 03	V1046.002 Seq 05				Valve Leakage Check Handling Damace, Clearwice Checks, Longe Sort Make 2007	Hazardous gas buildup
V41BU0.030-C	E3 COMPONENTS EXTERNAL INSPECTION	EKSC		V1011.02 Seq 04						Handling Darming, Classerone Charity I cope Sout World on or	
V41BQ0.032 V41BU0.031-B	FUEL BLEED VALVE BELLOWS LEAK TEST E2 MCC BONDLINE ULTRASONIC	LRU EKSC	Valves	V1011.05 Seq 10	V1294.005 Seq 03	V1048.002 Seq 07				Meted TPS LRU - Remove and replace verification	Hezerdoue gee buildup
V418U0.031-C	INSPECTION	EKSC		V1011.02 Seq 05			V1035VL2 Seq 08		COMBUSTION	Internal Debonds → Emplosion, Crit 1; External Leak, UAJ to Crit 1	
V418Q0.034	INSPECTION OXID BLEED VALVE BELLOWS LEAK TEST		Valves	V1011.02 Seq 05	V1294.006 Sec 03	V1046.003 Seq 09	V1038VL2 Seq 08		COMBUSTION	Internal Debonds -> Emplosion, Crit 1; External Leak, UAI to Crit 1	
V41BS0.020-A V41BS0.021	E1 HPFTP TORQUE TEST	A, RI, PLRU	HPFTP	V1011.03 Seq 09	V5E08 OSSU 1	V1046.003 Seq 09			TURBOPUMPS	LRU - Remove and replace verification Verify the rotor is free to rotate prior to teeting	Hazardoue ges buildup Improper start. Ox rich resulting in
		F	HPETP	V1011.03 Seq 09	V5E06 OSSU 1				TURBOPUMPS	Investigative torque check if the specification limits are accepted	engne fire Improper start, Ox rich resulting in
		I, ER	Avionics		·		V5005 Seq 06		AVIONICS	Verifies proper electrical grounding conditions exist between the SSME pimbel bearing and the orbitar structure. Test	engne fire Unscheduled Maintenence Action o Leunch Deley
	BONDING TEST	l, ER	Avionics	İ			V5005 Seq 06		AVIONICS	performed each time the bonding straps are disturbed.  Verifies proper electrical grounding conditions exist between the SSME electrical interface panel and the orbitar structure.	Unecheduled Maintenance Action of Launch Delay
V41AL0.030-A	E1 SSME/TVC ELECTRICAL BONDING TEST	A, I, ER	Avionica	ļ .	!	81287 OSSU 3			AVIONICS	Test performed each time the bonding straps are disturbed.  Verifies proper electrical grounding conditions exist between the SSME TVC actuator attach points and the orbitar structure.	Unecheduled Meintenence Action of Launch Delay
V41AN0.010-A	E1 SSME CONTROLLER POWER APPLICATION	A, ER	Avionics					V9001VL4 Seq 02	AVIONICS	Test performed each time the bonding straps are disturbed.  Defines the proper sequencing of cockpit switches for application of SSMF controller oneser as well as the values of	Unscheduled Maintenance Action of Launch Delay
V41AN0.020-A	E1 AC POWER REDUNDANCY VERIFICATION	A, ER	Avionics		:	V1046.001 Seq 04		V9001VL4 Seq 02	AVIONICS	the monitored responses. Identifies the constraints for cooling , air and FACOS power.  Provides for SSME AC power redundancy verification while	Unscheduled Maintenance Action of
V41AN0.022-A		A, LRU	Avionics	V1011.06 Seq 02	V1294.002 Seq 08	V1046.001 Seq 04		V9001VL4 Seq 09		controllers are under power load.  Performs a redundancy verification of the SSME controller.	Launch Delay Unscheduled Maintenance Action o
V41AN0.023-A		LRU	1							power supplies. Controller chennels A&C and 8&C are verified. This procedure also verifies the backup memory power is functional and verifies the AC supplied +10 V	Launch Delay
		A. ER. LRU	Avionics		V1294.002 Seq 03				AVIONICS	Verifies the capability of the 28 volt DC and battery systems are holding up the controller memory.	Unscheduled Maintenance Action of Launch Delay
V41ZA0.010	CHECKOUT SEME HARNESS REPLACEMENT RETEST	7-7	Avionica	V1011.06 Seq 02	V1294.002 Seq 07	V1046.001 Seq 04		V9001VI.4 Seq 09		Controller Changeout Verification. Functional hardware and software chackout.	Unacheduled Maintenence Action of Launch Delay
		A. LRU	Avionica		V5E02 Seq 27				AVIONICS	Defines the continuity and insulation resistance tests to be performed on any replacement harness installed on an engine	Unacheduled Meintenence Action o Launch Delay
V41AU0.080-A	E1 GMBAL BEARING SENSOR	ER. LRU	Instrumentation				V9001VI.4 Seq 02		AVIONICS		Unacheduled Maintenance Action o Launch Delay
	CHANNELIZATION VERIF	A. EKSC	Instrumentation	V1011.02 Seq 04		V1046.001 Seq 12		V9001VL4 Seq 02		Instrumentation integrity checkout	Unacheduled Maintenance Action of Launch Delay
V41AU0.090-D	E1 POST-FLIGHT SENSOR CHECKOUT	A, EKSC	Instrumentation					V9001VL4 Seq 02	AVIONICS	Part of this check is Weld #3 Strain Gage checkout needed to ensure electrical continuity of gage after bond is assured	Unacheduled Maintenence Action of Leunch Delay
V41AU0.016-A	ET MADS INSTRUMENTATION VERIFICATION	A, ER	Instrumentation			V1046.001 Seq 13		V9001VL4 Seq 02		Instrumentation integrity checkout	Unacheduled Maintenence Action of Launch Delay
V41AU0.020-A		ER, LRU	Instrumentation	V1011.05 Seq 08	V1294.002 POSU 11	V1045.001 Seq 13		V8001VC4 38Q 02	AVIONICS	Instrumentation integrity checkout	Unscheduled Maintenance Action of Launch Deley
V41AU0.042-A		A, PLRU, I, NRAT	Instrumentation		V5E02 Seq 27 &				AVIONICS		Unecheduled Maintenance Action o Launch Delay
V41AP0.020-A	E1 MFVA PRI HEATER POWER ON COMMAND		Vehres		V1294.002				AVIONICS	Wald #3 Strain gage in place to detect uneven bearing weer ~ debond test needed to ensure acceptable date on next flight Changeout Verification	Unecheduled Maintenance Action or Launch Delay Unecheduled Maintenance Action or
	E1 MFVA SEC HEATER POWER ON COMMAND		Valves						AVIONICS	Changeout Verification	Leunch Delay
V41BU0.351-A	E1 POST FLIGHT MCC LINER POLISHING	EKSC	MCC	V1011.02 Seq 05			V1038VL2 Seq 08		COMBUSTION		Unerheduled Meintenance Action or Leunch Delay Unerheduled Maintenance Action or
V41BU0.362-A	E1 PRELAUNCH MCC LINER POLISHING	•	MCC		1	\$1287 OSSU 9			COMBUSTION	Leakage, Performence Loss Remove Surface Oxiditation -> Erosion -> Leakage,	Performence loss Unscheduled Maintenance Action or
V41BU0.093	HIGH FUEL SIDE DYE PEN INSP (PHASE II)	тс	Powerhead		V5E06 Seq 12				COMBUSTION	Liner Met.1 & Transfer Tube Weld Thru-Cracks > By-pass Flow	Performance loss
	HGM OXID SIDE DYE PEN INSP (PHASE II)	rc	Powerheed		V5E02 Seq 14				COMBUSTION	Liner Met.1 & Transfer Tube Weld Thru-Cracks -> By-pass Flow	Performence loss
	HGM FUEL SIDE DYE PEN INSP (PHASE 1)		Powerhead	•	V5E06 Seq 12				COMBUSTION	Liner Met.1 & Transfer Tube Weld Thru-Cracks > By-pass Flow	Performence loss Unecheduled Maintenance Action or
	HGM OXID SIDE DYE PEN INSP (PHASE II+)	•	Powerhead	•	V5E02 Seq 14				COMBUSTION	Liner Met.1 & Transfer Tube Weld Thru-Cracks -> By-gass Flow	Performance loss Unscheduled Maintenance Action or
V72AQ0.040-A	VERIFY SSME 1/EIU 1 COMMAND PATH	LRU	Avionics				V9001VL4 Seq 02		AVIONICS	Performence Loss	Performence loss

Table 8. Engine requirements database (Continued).

OMRSD NUMBER	OMRSD DESCRIPTION (V41 FILE III DATED 9/15/95)	OMRSD	Component	OPF OMI's	ENGINE SHOP	VAB/PAD OMFs	OTHER OMFs	RT OMFs	SUBSYSTEM CODE	OMRSD RATIONALE/ROOT CAUSES	Root Cause Categories
V72AQ0.050-A		A, LRU	Avianica	1			V9001VL4 Seq 02		AVIONICS		
V72AQ0.080-A		LRU	Avionica			S0017VL13 Seq 42			AVIONICS	,	
V72AW0.030-A		A, LRU	Avionics				V9001VL4 Seq 02		AVIONICS	•	
V41BU0.420-A	E1 HEAT SHIELD BLANKET INSPECTION	A. LINU	Heat Shield			S1287 Seq 04			HEAT SHIELD	Thermal Deformations -> Aft Leek to Almosphere -> / Cnt. 1?	
	· ·	•				0.120. 0040.			HEAT SHIELD		
V41BU0.421-A	E1 EMHS INSPECTION	A	Heat Shield	V41-40018					HYDRAULIC		
V41BU0.050	HYDRAULIC DRAIN LINE INSPECTION (TIME & CYCLE)	†C	Lines/Ducts		V1294.002 Seq 19	V1046.001 Seq 13				Periodic inspection (every 10 tests) of hydraulic actuator shaft seels.	
V58AG0.121-A	SUPPLY OD PRE-MATE INSPECTION	ı	Lines/Ducts				V9002.06 Seq 03		HYDRAULICS	Verify Configuration :	
V58AG0.121-B	RETURN OD PRE-MATE INSPECTION	i	Lines/Ducts				V9002.06 Seq 03		HYDRAULICS	Verify Configuration	
			Lines/Ducts				V9002.06 Seq 03		HYDRAULICS		
V58AG0.123-A	SOFTE CON DEMONS ENGINEERING	•		and the second							
V58AG0.123-B	RETURN OD DEMATE INSPECTION	ı	Lines/Ducts				V9002.06 Seq 03		HYDRAULICS		
V41CB0.080-A	E1 MCC INJECTOR INSPECTION	EKSC	MCC	V1011.01 POSU 5	V1294.008 Seq 02		V1038VL2 Seq 08		COMBUSTION	H2O or Contaminants in Acoustic Cavities	
V41CB0.065-A		PLCL	Nozzie	S0028 Seq 19			S0026	V1038VL2 Seq 14	COMBUSTION	Install Protective Bumpers for Ground Transport prior to STS Stack -> Alt Manifold Impact, Thru-Crack -> Leakage to or	
V418Q0.090-A	INSTALLATION E1 PCA FUEL SIDE INTERNAL LEAK TEST	EKSC, LRU	PCA	V1011.05 Seq 12	V1294.002 Seq 10	V1046.006 Seq 04	V1011.06 Seq 03			Combined test demonstrates that the emergency shutdown PAV vent port seal is not leaking beyond acceptable limits.  Also checks fuel purge and bleed valve solenoids and fuel	
		FW00 1011	-	W1044 OF P 13	V1294.002 Seq 10	V1046.006 Seq 04	V1011.06 Seq 03			Combined test demonstrates that the emergency shutdown	
	E1 PCA LO2 SIDE INT/HPV ST/SFT SL LKG		PCA	V1011.05 Seq 12	V1294.002 Seq 10	V1046.006 Saq 04	V1011.06 Seq 03			sclenoid vent port seel is nto leaking beyond acceptable limits.  Also the HPV poppet and shaft seels are ventied.	
V41BQ0.092	FUN LOZ SIDENT T CHG IOOEN NON	F	PCA	TBD						Performed only when combined test indicates excessive	
V41AS0.020-A		EKSC, ER, LRU	Pneumatics	V1011.06 Seq 04	V1294.002 Seq 11	V1045.001 Seq 05			ENGINE	Plenned Preflight Checkout	
V41BU0.073-A	E1 PNEUMATIC VENT FLANGE VERIFICATION	TC, LRU	Pneumatics		V1294.002 Seq 10					Flow Verification	
V41BU0.030-A	E1 COMPONENTS EXTERNAL INSPECTION		System	V1011.02 Seq 04						Handling Demage, Clearence Checks, Loose Spot Welds on or Meltad TPS	
V41BU0.033	FUEL SYSTEM LAI INSPECTION	EKSC	System	V1011.02 Seq 04							
V41BU0.380-A	E1 HELIUM BARRIER SYS INSPECTION	A, LRU	System			S1287 Seq 06	V9018.002 Seq 07		DUCTS	Verify Beg Intact	
V418U0.510-A		ER, MÓD, LRU	System	V1063 Seq 14						Interference Check	
V41BU0.520-A		ER, MOD, LRU	System	V1063 Seq 14							
V418U0.530-A	E1 SSME-TO-EMHS CLEARANCE CHECK	A	System	V41-50024					HEAT SHIELD	'	
V418W0.031-A	E1 PREPS FOR OPF ROLLOUT	Ā	System	V41-20003						Varifies that the angine is configured for transfer from the OPF.  TVC actuator locks restrain engine movements and covers protect against contamination.	
V41BW0.034	INSTL SSME STORAGE/SHIPPING COVERS		System	V5057						Defines the conditions governing use of the subject protective covers	
V41BW0.050	, Dr. Edwice Separates . September .	ENV	System	V5057			******			Minimize rain or other contaminants entry into the nozzle	
V41CB0.010		PLCL	System				\$0026				
V41CB0.012-A	E1 HE BARRIER SYS INSPECTION POST FLIGHT	EKSC	System	V1263 Seq 04		V9018.002 Seq 07	V1038VL2 Seq D6		DUCTS	Verify Bag Intact	
V41CB0.030	FERRY FLIGHT SET INSTALLATION	FF	System				V1038VL2 Seq 06			Install Protective Covers, etc. for "Piggy-Back" Fly	
V41CB0.080-D	ENGINE DRYING - 1ST PURGE (PHASE II )		System		V1294.008 Seq 04		•		COMBUSTION	Controls the criteria used to perform engine drying operations following each flight. Pressures, temperatures, minimum	
V41CB0.080-E	ENGINE DRYING - 2ND PURGE (PHASE II)	EKSĈ	System		V1294.008 Seq 04				COMBUSTION	durations and configurations are defined Controls the criteris used to perform angine drying operations following each flight. Pressures, temperatures, minimum	
V41CB0.081	DRYNESS VERIFICATION (PHASE II)	EKSC	System		V1294.008 Seq 05				COMBUSTION	durations and configurations are defined  Requires a verification of dryness, defined by a maximum	
			i i						ENGRIE	moisture criteria, to be performed following completion of drying	
V41AS0.030-A	E1 FRT CHECKOUT	EKSC, ER, LRU	Systems	V1011.06 Seq 06	V1294.002 Seq 13	V1046.001 Seq 08			ENGINE	Planned Preflight Checkout	
V41AS0.030-D	E1 FRT PNEUMATIC SHUTDOWN SEQ DATA VERIF	EKSC, ER. LRU	Systems	V1011.05 Seq 08	V1294.002 Seq 19	V1046.001 Seq 13			ENGINE	Plenned Preflight Checkout	
V41BU0.130-A		LRU, 1ST	TVC	TBO							
V418U0.130-B		LRU, 1ST	TVC	ТВО						•	
V41800.130-8	E1 ACTUATOR CHECKOUT	EKSC, ER, LRU	Verves	V1011.06 Seq 05	V1294.002 Seq 12	V1046.001 Seq 07			ENGINE	Planned Preflight Checkout	
V41AS0.010-A V41BQ0.040-A	E1 OXIDIZER PROP VILVS/PRG C/V LEAK	EKSC, I	Valves	V1011.05 Seq 09	V1294.012 Seq 04	V1046.004 Seq 04	V1294.005 Seq 06			Check Valve Failure - Contamination; STS-55 abort	
V41BQ0.041	TEST OXIDIZER PROP VLVS/PRG C/V ISOLATION	F	Valves		V1294.012 Seq 04					investigation risk mitigation leolation check if the V41BQ0.040-A leakage limits are exceeded	
	TEST		Valvas	V1011.05 Seq 07	V1294.007 Sec 03	V1046.003 Seq 04				Valve Leakage - LOX system integrity check	
V41BQ0.120-A	E1 LO2 PROP VALVE BALL SEAL LEAK	EKSC, ER		71011.05 Seq 07	¥120=1007 0#Q 03	V 1040.003 304 04				Isolation check if the V41BQ0.120-A leakage limits are	
V41BQ0.121	LO2 PROP VALVE BALL LKG ISOLATION	<u>-</u>	Valves								
V41BQ0.130	RIV SHAFT SEAL LEAK TEST (TIME &	TC	Valves	TBO						Valve Leakage	
V41BQ0.140-A	E1 RIV SEAT FLOW TEST	EKSC	Valves	V1011.05 Seq 06	V1294.006 Seq 03	V1046.003 Seq 06				Valve Leekage	
V41BQ0.141-A	E1 OBV SEAT LEAK TEST	EKSC, LRU	Valves	V1011.05 Seq 06	V1294.006 Seq 03	V1046.003 Seq 06				Valve Leakage	
V41BQ0.150-A	E1 GCV CHECK VALVE LEAK TEST	EKSC, LRU	Valves	V1011.04 Seq 06	V1294.006 Seq 03	V1046.003 Seq 06				Valve Leakage	
V419Q0.180	HPV CHECK VALVE LEAK TEST	TC	Valves	TBD						Valve Leakage	
V418Q0.190	OPOV SLEEVE TEST & WINDOW CALIB	I, LRU	Valves		V1294.002 Seq 14	V5E17 Seq 09				Sets Open Loop Commend % - Used to adjust start sequence	
V41BQ0.191	FPOV SLEEVE TEST & WINDOW CALIB	I, LRU	Valves		V1294.002 Seq 14	V5E18				Sets Open Loop Command % - Used to adjust start sequence	
						S1287 OSSU 8				Final look before launch	
V41BU0.070-A	E1 AFT CLOSEOUT INSPECTION	^	Valves			31207 0330 0				I THE CONTRACTOR THE CONTRACTOR	

Table 8. Engine requirements database (Continued).

NUMBE	OMRSO DESCRIPTION (V41 FILE IN DATED	OMRSO EFFECTIVITY	Component	OPF DMI's	ENGME SHOP	VAB/PAU OMES	OTHER OMI's	RT OMI's	SUBSYSTEM CODE	OMRED RATIONALE/ROOT CAUSES	Root Cause Categories
R	9/15/95)								- CODE		ì
V418L0.060-A	SSME WELD 22 & 24 LEAK CHECK	PKSC, NRAT	нРотр	V1011 05 Seq 07	V1294 007 Seq 04	V1046.003 Seq 07				Due to poor processing, HPOTP belance cavity standoff welds are leak chacted — No leate over verified, but lack of weld penalization up to 90%, no been found on these welds. Standoffs have been suspected of leating and caused return to Caroga.	Aft Compartment overpressurization or fire
	E1 HPOTP PLUG WELD LEAK CHECK	PKSC. NRAT	HPOTP	V1011 05 Seq 09	V1294 004 Seq 04	V1045.004 Seq 04	V1294.005 Seq 07			Plug weld leak occurred on a unit — Concern over these welds leaking either Gowhellum/Hot gas wito bouttail — therefore all sciennal plug welds on the housing are checked	Aft Compartment overpressurization or fire
V41AXX 020-A V41AXX 020-6	E1 LO2 FEED (JOINT 01) VF LK CK	ER, PR, OMOP	Lines/Ducts	V1011.05 Seq 07		V1046 003 Seq 05			DUCTS	Ensure joint integrity of LPOTP to pump inlet ducting after engine is installed	Aft Compartment overpressurization or fire
	E1 LH2 FEED (JOINT F1) VF LK CX	ER, PR. OMOP	Lines/Ducts	V1011 05 Seq 05		V1046 002 Seq 04			DUCTS	Verify pump inlet joint integrity after metalling the LPFTF	Aft Compartment overpressurtzetion or fire
V41AXD 020-C	E1 GH2 PRESS (JOINT F9 3) UF LX CX	ER, PR, DMOP	Lines/Ducts	V1011.05 Seq 09		V1046 004 Seq 04			DUCTS	Joint Integrity Post Engine Installation	Aff Compartment
V41AX0.020-0	E1 LOZ BLEED (JONNT 015) VF LK CK	ER, PR, OMOP	Lines/Ducts	V1011 05 Seq 07		V1046.003 Seq 05			DUCTS	Joint Integrity Post Engine Installation	Aft Compartment overpressurization or fire
V41AXD.020-E	E1 LH2 BLEED (JOINT F4.3) VF LK CX	ER, PR, OMOP	Lines/Ducts	V1011.05 Seq 05		V1046 002 Seq 04			DUCTS	Joint Integrity Post Engine Installation	Aft Compartment
V41AX0.020-F	E1 HELRING (JOINT P1) OF LICCK	ER, PR, OMOP	Lines/Ducts	V1011 05 Seq 12		V1046 001 Seq 05	V1046 006 Seq 04		DUCTS	Joint Integrity Post Engine Installation	Overpressurization or fire Aft Compartment
V41AX0.020-G	E1 GN2 (JOINT N1) VF LK CK	ER, PR, OMOP	Lines/Ducts			V1149 Seq 15	V1046 006 Seq 03		DUCTS	Joint Integrity Post Engine Installation	Aft Compartment
V41AX0.020-H	E1 HYD - PRESS (JOINT H1) UF LK CK	ER, PR, OMOP	Lines/Ducts		V5E17 Seq 09		VSE18	V9002 06 Seq 05	DUCTS	Joint Integrity Post Engine Installation	Overpressurization or fire Aft Competiment
V41AX0.020-I	E1 HYD - RETURN (JOINT H17) VF LK CX	ER, PR, OMOP	Lines/Ducts		V5E17 Seq 09	_	V5E18	V9002 06 Seq 05	DUCTS	Joint Integrity Post Engine Installation	overpressurization or fire AR Compartment
V41AX0.050-A	E1 G02 ORB/SSME INTERFACE FLANGE LEAK CHECK	A, ER	Lines/Ducts			V1846 005 Seq 05			DUCTS	Joint Integrity Post Engine Installation	overpressurization or fire Aft Compertment
V418L0.031	SSME ENCAPSULATION POWER HO LEAK CX	EKSC & ER	Powerhead		V1294.007 Seq 04				ENGINE	System leak integrity check for leunch - Mst 1 or Weld	Overpressurization or fire Aft Compartment
V41BL0.032	SSME ENCAPSULATION FUEL SYS ISO TEST	F	System	1	V1294 007 Seq 04	•		<u> </u>	ENGINE	Thru-Crack; Seel not Seated -> Crit. 1 System teak Integrity check for launch - Mat 1 or Weld	Overpressurization or fire Aft Compartment
V418L0.033	SSME ENCAPSULATION OXID SYS ISO TEST	F	System		V1294 007 Seq 04				ENGINE	Thru-Crack; Seal not Seated -> Crit 1 System leak Integrity check for leunch - Mat. 1 or Weld	Overpressurization or fire Aft Compartment
V41BL0 034	SSME ENCAPSULATION HOT GAS SYS ISO TEST	F	System		V1294.007 Seq 64		1		ENGINE	Thru-Crack, Seal not Seated -> Crit. 1  System leak integrity check for launch - Mat 1 or Weld	Overpressurization or fire Aft Compartment
V418P0.010-A	E1 G02/GCV EXT LK CK & DRIFICE VERIF	EKSC, I	Valves	V1011.04 Seq 07	V1294 002 Seq 17	V1046.005 Seq 05	V1294 006 Seq 05		+	Thre-Great, Seal not Sealed -> Crit. ( Establishes leak test of all gaseous oxygen system joints.	AR Compenses
V41A00 010-A	E1 SENSOR CHECKOUT								<u> </u>	from the AFV to the orbiter interface on an each flight basis	Overpressurization or fire
V41ALD 013-A		EKSC, ER, LRU	Instrumentation	V1011.06 Seq 02	V1294.002 Seq 06	V1046.001 Seq 04		V9001V1.4 Seq 02	AVIONICS	Planned Preflight Checkout	Erroneous shutdown, loss of vehic
V418U0.250-A	E1 OPERATIONAL INSTRUMENTATION VERIFICATION		Instrumentation			V1046 001 Seq 04		V9001VL4 Seq 02	AVIONICS	Instrumentation integrity checkout	Erronsous shutdown, loss of vehi
	E1 SENSOR IR VERIFICATIONS	EKSC, LRU	Instrumentation	V1011 02 Seq 07						Functional check of each turbine discharge temp	Erroneous shutdown, lose of vehic
V418P0 020-A	E1 HEX COIL LEAK TEST	A, EKSC, PLRU	HEX	V1011 04 Seq 02	V1294.003 Seq 03	V1046 005 Seq 06			HEX	Mist.1 (stringer) or Weld Thru-Crack; HPOTP Installation Impact Hole -> HG to Tank; Crit. 1	Fire, Uncontained engine failure
V418P0.030	SSME HEX COIL PROOF TEST	PLRU	HEX	V1011.04 Seq 03	V1294 003 Seq 04	V1046 005 Seq 07			HEX	Mat. 1 (stringer) or Weld Thru-Crack; HPOTP Installation Impact Hole >> HG to Tank; Crit. 1	Fire, Uncontained engine failure
V418U0.086	HEX EDOY CURRENT INSPECTIONS (TIME & CYCLE)		HEX	V1011.02 Seq 11					HEX	Thin Walls from Bracket West, Manuf -> Thru-Crack, HG Leslage to Tank, Crit. 1	Fire, Uncontained engine failure
V418U0.115	HEAT EXCHANGER INSPECTION	TC	HEX		V5E02 Seq 14				HEX	Visible Impact Damage, Bracket Weer -> Thru-Crack -> HS to Tank, Crit 1; Turn, Varia Cracks -> Loss of Varia Impact	Fire, Uncontained engine tellure
V418U0 125	HEX VISUAL INSPECTION	PLRU	HEX		V5E02 Seq 12				HEX	MI Post -> Demage or Crit 1 HPOTP Installation Impact Hole -> HG to Tank, Crit. 1	Fire, Uncontained engine tailure
V41BU0.075-A	E1 HPFTP INTERNAL INSPECTION	PKSC	нетр	V1011.02 Seq 08					TURBOPUMPS	Verify no inlet or discharge sheet metal cracking, no nozze cracking or stated or discharge sheet metal cracking, no nozze cracking or stated or nozze cracking or seroseor, no flushrowth seel cracking or miseing paces, no ballows shield cracking. (All imagescions completed with turbourum ins	Fire, Uncontained engine failure
V41BU0.079	HPFTP FIRST STAGE BLADE 22X INSPECTION	TC, DCE	HPFTP		V5E06 Seq 14				TURBOPUMPS	Verify no blade cracking due to previous occurrences of air oil cracking	Fire, Uncontained engine failure
V418U0 080	HPFTP TURBINE HISPECTION (TIME & CYCLE)	PKSC	НРЕТР		V5E06 Seq 14				TURBOPUMPS	Venity no inter or discribange abset metal cracking including wated 450 and the turning venes; no neutre cracking, or arceland, no feathmouth seel cracking, pletform cracking, or evenes, no feathmouth seel cracking or me	Fire, Uncontained engine failure
V41BU0.067	HPFTP BELLOWS HEIGHT VERIF	PLRU	нетр		V5E06 OSSU 2				TURBOPUMPS	Verify beliows height adequate to provide proper preload on the believes at installation. Incorporated as a result of a previous failure of the believes.	Fire, Uncontained engine failure

Table 8. Engine requirements database (Continued).

OMRSD NUMBER	OMRSD DESCRIPTION (V41 FILE I# DATED 9/15/05)	OMRSD EFFECTIVITY	Component	OPF ONI's	ENGINE SHOP OMPs	VAB/PAD OMI's	OTHER OMI'S	RT OMF's	SUBSYSTEM CODE	OMRSD RATIONALE/ROOT CAUSES	Root Cause Categories
V41CB0.050-A	E1 HPFTP TURBINE BEARING DRYING	EKSC	нРГТР	V1011.01 Seq 03		V9018 002 Seq 04	V1038VL2 Seq 07		TURBOPUMPS	Ensure all moisture is removed from the bearing area after a test/flight	Fire, Uncontained engine failure
V418Q0.110-A	E1 HPOTP PRIMARY OXID SEAL LEAK TEST	PKSC. HRAT	нротр	V1011 05 Seq 07	V1294 006 Seq 03	V1046 003 Seq 07				Checks for excessive leakage of LOX/GDX from the HPOTP seal ··· Protects against excessive flow overcoming the barrier seal and from having excessive lankage lossed using the child having of the engine. Kelf seal does wear during operation	Fire, Uncontained angine failure
V41BS0 040-A	E1 HPOTP TORQUE TEST	EKSC, RI, PLAU, NRAT	нротр	V1011 03 Seq 06	V5E02 Seq 25				TURBOPUMPS	Done to ensure rotor is not bound up prior to start— concern over contamination if high and also start— characteristics if rotor is slow to spin—contamination has been found around the rotor but only once enough to effect start (rusted P/E beerings)	Fire, Uncontained engine failure
V418S0 042	HPOTP INVESTIGATIVE TORQUE	F. NRAT	HPOTP	V1011.03 Seq 06	V5E02 Seq 25				TURBOPUMPS	Done only to run in a high torque pump to bring the torque value below spec requirements	Fire, Uncontained engine failure
V41BS0.043-A	E1 HPGTP IMPELLER LOCK VERIF	PKSC, PLRU, NRAT	HPOTP	V1011.03 Seq 06	V5£02 Seq 25				TURBOPUMPS	Locking feature was overcome on a MPOTP PSP impeller both tock during torque seatu/spinning of pump for inspections. Recurrence control is to only turn the pump in the both tiphening discondium grapections and to check the locking feature after al	Fire, Uncontained engine failure
V418S0.045	HPOTP MICROSHAFT TRAVEL	PKSC, NRAT	неоте	V1011.03 Seq 06					TURBOPUMPS	Turbine bearings have worn very quickly in past — this measurement is to ensure that the bearings are still capable of 1 flight prior to a leunch.	Fire, Uncontained engine failure
V41BQ0.110-A	E1 ATD BLOCK VII HPOTP PRIMARY OXID SEAL LEAK TEST	PKSC, NRAT	HPQTP	V1011.05 Seq 07	V1294.005 Seq 03	V1046.003 Seq 07				This teak check was never performed during HPOTP/AT certification. The data obtained is erratic and a probably indicative of only gross sail imperfections (which would most likely be detected through torque checks). It is currently an OMRSO requirement.	Fire, Uncontained engine failure
V418U0.065-A	ET HPOTP INTERNAL INSPECTION	PKSC, NRAT	нРОТР	V1011 02 Seq 08					TURBOPUMPS	Visual inspections of turbine hardware (sheetmets/ nozzied blades) due to crecking and crosson seen in the past, of the main pump liner, induced due to caretation damage and contamination found in the past, of the PBP impetire intelled but to locking the	Fire, Uncontained engine failure
V41BU0.066-A	E1 HPOTP TIP SEAL RETAINER INSPECTION	PKSC, NRAT	неоте					i	TURBOPUMPS	Verifies 1st stage tip seal retainer screws have not rotated. Could lead to blade failure.	Fire, Uncontained engine failure
V41BUG 390-A	ET LPFO OVALITY CHECK	F	Lines/Ducts	V1011.02 Seq 10			V9018 002 Seq 10		DUCTS	Contingency test performed only when the LPFD helium barrier system has been damaged. Object is to detect potential duci collapse or separation from the layer of insulation by measuring the roundness of the duct	Fire, Uncontained engine failure
V418U0 400	PERFORM LPFD XRAY INSPECTION	F	Lines/Ducts	TBD					DUCTS	Contingency reamt preformed only when the ovality check indicates that some damage or collapse has occurred in the LPFD. The cross section is X-rayed in an attempt to verify presence of damage.	Fire, Uncontained engine failure
V41BS0.050	HPOTP/AT TORQUE TEST	EKSC. RI. PLRU	HPQTP	Y1011.03 Sep 06	V5E02 Sec 25		<u> </u>	<b>_</b>	TURBOPUMPS	Replaced by V418S0.04G-A	Fire. Lincontained engine failure
V41850.055 V418U0.405	HPOTP/AT INVESTIGATIVE TORQUE SSME LPFD TRIPOD LEGS INSPECTION	F OCE	HPOTP Lines/Oucts	V1011.03 Seg 06 T9D	V3.E02 Seq 25		<del>                                     </del>		DUCTS	Replaced by V41850.042 Performed to insure LPFD structural integrity Inspection is performed if post flight data evaluation reveals HPFTP unacceptable synchronous frequencies.	Fire Uncontained engine failure Fire, Uncontained engine failure
V418UC 055-A	E1 ATD BLOCK VII HPOTP INTERNAL INSPECTION	PKSC, NRAT	неоте	V1011.02 Seq 08					TURBOPUMPS	No HPOTP/AT internal inspections were made during certification. Inspections of the furbine, mainstage pump and PBP inlets, and all three bearings have been added only because the inspections aren 1 time consuming and because some "human error" could be	
V41BS0.010-A	E1 LPFTP TORQUE TEST	A. RI. PSI. ER. PLRU	LPFTP	V1011.03 Sec 04					TURBOPUMPS	Verify rotor is free to rotate prior to testing	Fire, Uncontained engine failure
V41BU0.127	HPOTP/AT PBP TIEBOLT LOCK INSPECTION	f	HPOTP	V1011 03					TURBOPUMPS		Fire, Uncontained engine failure
V41BU0.12B	HPOTP/AT CONTAMINATION INSPECTION	A. PKSC	нротр	V1011.07 Sea ??					TURBOPUMPS		Fire, Uncontained engine failure
V41C90.085	SSME HPOTP/AT TURBINE BEARING DRYING	PKSC	неоте	V1011.01 Seq 03	V1294.008 Seq 04	V9018.002 Seq 04			TURBOPUMPS	Verify all moisture is removed from the bearing area after a test/flight	Fire, Uncontained engine failure
V41850.011	LPFTP INVESTIGATIVE TORQUE	f	LPFTP	V1011 03 Seq 04					TURBOPUMPS	Investigative torque check if the specification limits are exceeded - torque check failure generally lift-off seal binding or laby seal - copper plating rub	Fire, Uncontained engine failure

Table 8. Engine requirements database (Continued).

OMPRED	OMPSO DESCRIPTION	OMRSD	Component	OPF OMI's	ENGINE SHOP	VAR/PAD DIMYs	OTHER OMI's	RT OMI's	SUBSYSTEM	OMINER RATIONAL FRANCISCO	T
NUMBER	(V41 FILE III DATED 8/15/86)	EFFECTIVITY	,		OMI's		OTHER OWN'S	AT UMIS	CODE	OMRSD RATIONALE/ROOT CAUSES	Root Cause Cutegories
(41 PBD 030 A	E' LPOTF TORQUE TERT	A RI, PRI, ER, PLRU	Legre	V1811 83 8eq 65	V\$[23		+		TURBOPUMPS	Dans to ensure rate: it has sowned up arms to start	<del></del>
				1		i				Assert over contem molion of high and also start	FIRE, L. REBITS had angine failure
					ļ					sharestermines fireter is even to sein contemptation	<b>\$</b>
							1		1	has been found that bound the reter and begring wind	ļ.
¥41 <b>966</b> 921		<u> </u>		<b>+</b>	<del></del>				<u> </u>	up can also rewinding coupes failure of	
74.566 177	LPOTP INVESTIGATIVE TORQUE	1'	LPGTF	V1811 83 6rq 85					TURBORUMPS	Partermad to frac the rater if pupping stand any if	Fire, Uncontained engine failure
741884 022 A	ET LPOTF BHAFT TRAVEL	A, ER, FLRU								needed must make tarque feture to permativalise or pump m remayed	
AT 1882 035 Y	to the same same	A, EN, PLAU	LPOTP	91811 83 844 85	APE 52	}			7148046WF6	Bearing wear on LPOTP thrust bearing must be	Fire, Unsertaines engine takura
Y41888 848 A	ET MAIS INJECTOR LOS POST VACUUM	DLP	Wais injector	V1811 02 Beg 84			-			M g A Tig rigg	
	DECAY								COMBUSTION	LOX Past integrity sheet Impactual or Defector Past Plugged & Plag Damaged -> Lass of Plug, Incress	Fire, Uncents-ned angine review
V41 BUB 634-A	ET MAIN HISECTON LOX PORT BIABING	FKBC	Main injector	VIG11 82 944 84				ļ	COMPUBTION	Damage to Pool > Loss of Post, Crit 1	
									COMPUSATION	Under Bist (1245) > Firm Ersein MCG (110 Wall > Regair er Crq 1 Lesk, Under Biss > Cambustion Performance	fire, unconstitues engine follors
V418Q8 185	MEC HOLATION LEAK TEST	,	wcc .	1	V1294 007 Beg 05		-		COMBUSTON	Mat   Deband @ Liner Att   > Repair, UA: Performance	
			<b></b>							Look, Drit 3 to Crif 1 H regresse	Fire, Uncontained angine failure
441 BOE 248 A	ET MCC LINER CAVITY DECAY CHECK	PERC, LAU	wcc.		V1294 D03 B44 P5				COMPUSTION	Burat Disphragm Damage, interest Liner To Structure Teru-Great	Fire, Unsentained engine failure
4418UB 831-A	ET MICE BORDLINE ULTRASQUIC	E48C	ecc.	Y'8'1 82 604 85			A. 016A '3 8+0 01		COMPUBTION	Internal Datanda -> Employen, Crait; External Lake, UA-	Fire, Uncontained engine failure
941 BU 8 881 - A	MEC NIECTOR IRSPECTION WITH HAFTS	PLRU	wcc .	<del> </del>						10 014 1	
	REMOVED		1		APESS 004 15		<u> </u>		COMBUSTION	Inspect when HFITP Removes	Fire, Uncontained engine feiture
7418U8 882-A	MCC INJECTOR IMPRECTION WITH HROTE REMOVED	P1.90	MCC		V6C02 Beg 1A				COM #U \$ TIO 9	respect stan HPOTP Removad	Fire, Uncentained angine failure
41 PGB 188 A	ET THRUST CHAMBER BOZZLE LEAK TEST	EXBC	₩ C C/R +33 ₩	V1811 St 0+2 SP	V1294 811 844 88	V1848 884 844 14	V1038V.2 Bre 08		COMBUSTION	Cuid ar mat Wall foru Creas, Degraded Liner Wat 11er	Fire, Uncentained engine failure
					ļ					Basand > Regert, UAI Performance Leas, Cre 3 to Cnt 1  if increase. If no setton required then data used to	- No. Contend and angine ignore
	ET MCC TO NOZZLE GEAL LEAK TERT								1	tilpel engine performanse productions	
V41900 200 A	ET GCC TO HOZZELE GEAL LEAK TEGT	ERBC, LRU, F	M CC/Nezza	A101. DE B16 DE	V1294 994 Bre 42	V1848 804 840 88		Ţ.	COMBUST-OR	B 16 Best Thermal Degranature a Aft Compartment	Firs, uncantained angine faxure
¥418Q8 187	SOME HOZZLE ENCAPOULATION LEAK		<del></del>	<b></b>						Leas, Crit. 1	
	TEST	1'	4+214		V1284 818 800 62				COMBUSTION	Cold or Not Wall Thre Creek like Graws Erector, Brazones	Fire, Umas ntained angine failure
		1	ł				ì			Tube Ends: > Repair, UA: Parformance Lose, Crit 3 to Crit	
V419UB.963-D	MOZZLE VIBUAL INSPECTION	fasc	Bezzin	V1011 02 8eg 86		<del></del>	V1838V.2 844 53		ļ	1.2 demand.	
		i · · ·	****				A. 0 38A 7 5 844 03		COW9USTION	Erwood Tube Growns -> Lessage up to Grt 1, Tube	Fire, uncentained angine failure
		i	i							Buigne -> Trig NG floor or Shook Wave -> Oya	
				1	· '	l				Destruction NZ, Cre 1, Asiantry Annealing in Mac I	
V418U8 363 E	HOZZLE PARENT METAL SISCOLORATION	EXEC	\$ + 12 4	9181: 82 614 85			A.039AF5 844 08		COMBUSTION	Degradation, Bernt -> Crit 1	
	INSPECTION		1				1			Erunnt Tube Gromes -> Lonnage up to Cre 1; Tube	Fire, Uncontained angine fairure
									1	Beigne -> Trip HG Flow or Shook Ways -> Dyn Geotresian RZ, Cro 1, Se entry Annacing -> Mat 1	
		1					[				1
441 But 881-9	FUEL BIDE TRANSFER TUBE INSPECTION	PLRU	Powerhood		V5E86 8ex 12				COMPUBTION	Degradation, Burst -> Erd, 1	<del></del>
741 EUR 642 E	OR DIZER BIDE TRANSFER TUBE	PLAU	Powerhood		V5 E02 Beg 14		<u> </u>		COMBUSTION	Indeed when HPDTP Removed	Era, Uncontained engine fullure
	INSPECTION				l						Fire, wheentured anging topyre
419U9,881-C	FUEL PREBURNER INSPECTION	FLAU	Proburser		V5E00 Beq 12		T		COMBUSTICA	Report when HPFTP Removed	<u> </u>
4: BUS.E61-0	FPO LIBER INSPECTION	PLAU	Presures		V6 E04 044 12				COM BUBTIDA	Tapast when HPFTP Remared	Fire, Uncontained engine failure
741848.862 C	DEIDIZER PREBURNER INSPECTION	PLAU	Preburner	1	VACUE Eng 14				COMPUSTION	Indeed when HPOTP Removed	Fire, Uncantained engine failure
V41808.882 D	OPE LINER INSPECTION	PLAU	Presurage		V5ED2 Beg 14		<del> </del>		COMBISTICA	Imper men HPOTP Removed	Ете шпавота пев егу по заниго
V418U8.065	DX:D P/B :NUCCTOR ELEMENT INSP	TC. WSP	Preburner	<del>                                     </del>	V5E81 Beg 14						Fire, Uncontained engine favore
		1							COMPUSTION	Demaged Peats Printed, Last of Pint: > Increse Damage to Past > Last of Past into Turbine, Crd. 1 or leternal	Firs, Uncontained ongoe failure
										- natinge > Overheat Turbine, Crit 1	
A4. 6/0 419	BONE FUEL PIR INJECTOR ELEMENT INSP	*67	Prakurner	790					SOM BUR'ON	Damaged Foote Finned, Laus of Fine > Increase Camage	<del></del>
	I' DEC ON BORE PIEC TOURG MISSING!	1								to Feet > Plug Feet & Use or Lose of Post-into Tarbing	Fire, Uncentained engine failure
	<del> </del>	<del></del>	ļ	ļ			ļi		1	Cell 1 er. Aternal Leutuge Overhear Turbine, Cre	1
V41808 186	CHE INJECTOR OXID POSTS -NOP	TG	Preharmer		V5{88 8eq 12				COMBUSTION	Dameged Burte Fienen, aus af Fire Increase Damege	Fire, Unicontained engine failure
			1				1		i	to Past is Plug Past & Cas or Lass of Past into Turbine,	Characters and the state
	TPB DIFFUSES INSPECTION		<del> .                                      </del>						1	Crd 7 or internal Lankage Overheat Turbing, Crit 1	
¥418u6 576		DCE	Presures	190					COMPUBLICA	Contingency reamt performed to respect for process in	Fire, Uncontained angine fellure
	1		}	i					1	EPE effuser. The region will be invested unity if data.	
		1		1						everustion or HPFTP furbing discharge temp deeme 1	
								i e		'entrery	1

Table 8. Engine requirements database (Continued).

OMPRSD Mumber	OMRSD DESCRIPTION (V41 FILE III DATED	OMRSD EFFECTIVITY	Compenent	OPF OMI's	ENGINE SHOP OMI's	VAB/PAD OMI's	OTHER OMI'S	RT OM!'s	SUBSYSTEM	OMRSD RATIONALE/ROOT CAUSES	Roet Cause Categories
MAMBEH	9/15/96)	EFFEGIIVITY			OMI'S				CODE	1	
V418U0.032	OPB FACEPLATE FLATNESS CHECKS	DCE	Preburner						COMBUSTION	Integrity check after 'POP' - 'POP' Damage , Bowing Indication of Braze Cracks -> Loss of Element into Turbine, Crit 1, of Internel Leskage -> Overheat Turbine, Crit	Fire, Uncontained engine failure
418U0.046-A	E1 COMPONENTS INTERNAL INSPECTION	EKSC	System	V1011 02 Seq 08						Boroscope inspection of accessible angine areas without disassembly	Fire, Uncontained engine failure
41CB0.020-A	E1 ENVIR CLOSURE INSTALLATION	EKSC	System	S0028 Seq 19			50026			Insure that LPFD helium barrier system is functional to practude cryopumping in the event of a launch scrub which can lead to a collapse of the duct.	Fire, Uncontained engine failure
V418Q0.080	RIV OVERRIDE SEALS LEAK TEST (TIME & CYCLE)	тс	Valves	TBID						Periodic (every 10 starts). To verify that the RIV shaft seeks maltain override opening pressure within the RIV.	Fire, Uncontained engine failure
V41B00.100	AFV SEAT AND SHAFT SEAL LEAKAGE	A. GP	Vahree	V1011 04 Sec 07		V1046.005 Sec 05			T	No LOX in HEX prestart - Crit 1	Fire, Uncontained applies tailure
V41BQ0 101	AFV SHAFT AND SEAT ISOLATION	F	Valves	V1011.04 Seq 07		V1046 905 Seq 05				feotation check if the V418Q0.100 leakage limits are exceeded	Fire, Uncontained engine failure
1800.170-A	E1 PROP VALVE ACT PNEU SEAL LEAK JEST	EKSC, LRU	Valves	V1011 05 Seq 12	V1294 002 Seq 10	V1046 006 Seq 04	V1011 06 Seq 03	V5E17 Seq D9		Valve/See/ Lesiage - LRU Integrity Check	Fire, Uncontained engine failure
41800.171	PROP VALVE ACT PNEU SEAL 180 TEST	F	Valves	180						I solution check if the V41800.170-A leakage limits are exceeded	Fire, Uncontained engine failure
418P0.030-A	E1 APV CRACKING PRESSURE TEST	EKSC. LRU	Valves	V1011.04 Sec 07	V1294.002 Sec 17	V1046.005 Sec 05	<del> </del>	<del>†</del>	1	Verify proper AFV operation - Crit 1	
41BU0.220-A	AFV FILTER INSPECTIONS	A	Valves	V1011.04 POSU 5	V1294 002 POSU 6	V1046 005 POSU 2		1		Contamination check to verify that filter is not plugged which could lead to a collapse of the HEX.	Fire, Uncontained engine failure Fire, Uncontained engine failure
41800.220-0	AFV FILTER REPLACEMENT	A	Valves	V1011.04 Seq 07		V1046.005 Seq 05	V5005 POSU 3	VS087 Task 28		Contamination check to verify that filter is not plugged which could lead to a collapse of the HEX.	Fire, Uncontained engine failure
V41BQ0.010-A	E1 FUEL TP L/O/MFV BALL SEAL LX TEST	EKSC, ER	HPFTP, LPFTP, MFV	V1011.05 Seq 05	V1294.007 Seq 03	V1046.002 Seq 03				Verify no LPFTP or HPFTP RR-off seel carbon nose leakage or main fuel valve ball seel leakage. (Fuel system pressurized, messure leakage into hot gas system)	Hazardous gas buildup
V418Q0.011	FUEL TP L/Q/MFV SEALS ISOLATION	f	HPFTP, LPFTP, MFV	TBO						Isolation check if the V41BQC 010-A leekage limits are acceeded	Hazardous gas buildup
V41800.020-A	E1 FUEL TP PIST/MAPLEX/MFV LX CK	EKSC	HPETP, LPETP, MEV	¥1011 05 Seq 05	V1294 005 Seq 03	V1046 002 Seq 06				Verify no LPFTP or HPFTP large districtor secondary seal leakage or Neffex or MFV leakage (Fuel system preseutrand, measure leakage out of the fuel component drain)	Hazardous gas buildup
V418Q0:021	PUEL TP PISTANAFLEXAMPV ISO TEST	F	HPFTP, LPFTP, MFV	V1011 05 Seq 05	V1294.005 Seq 03	V1046 002 Seq 06		-		Isolation check if the V41BQ0.020-A leakage limits are	Hazardous gas buildup
/41800 050-A	E1 COMB HOT GAS SYS SEAL LEAK TEST	EKSC, LRU	System	V1011.05 Seq 09	V1294 005 Seq 06	V1046 004 Seq 04				Verify no LPFTP or HPFTP small diameter secondary seal leakage or other system leakages (Hot gas system preseutized, measure leakage out of the fuel component drain)	Hazardous gas buildup
41880.043-B	E2 HPOTP IMPELLER LOCK VERIE	PKSC PLRU NRAT		V1011.03 Sec 06	V5E02 Sep 25			+	TURBOPUMPS		
41BS0.043-C	E3 HPOTP IMPELLER LOCK VERIF	PKSC, PLRU, NRAT	1	V1011.03 Sec 06	V5E02 Seq 25		<b></b>		TURBOPUMPS		
V41BQ0.051	BSME HOT GAS BYS SEAL LK ISO TEST	f F	System	180	1.4.02.000.23				lungurumra	Isotation check if the V418Q0.050-A lealage limits are acceeded	Hazardous gas buildup
/41800.052·A	E1 86ME COMB HOT GAS TO FUEL SYS REV LX CX	PKSC	System	V1011 05 Seq 09	V1294 005 Seq 06	V1046.004 Seq 04				Verify no reverse LPFTP or HPFTP carbon nose testage (Hot gas system presented, messure stetage into fuel system) incorporated when the pump and to turbine and test chack did not distact sossting carbon nose testage	Hazardous gas buildup
V41B020.053	SSME HOT GAS REVERSE ISO LK CK	F	System	TBO						teoletion check if the V41B00 052-A leakage firmits are exceeded	Hazardous gas buildup
/41B00.030-A	ET FUEL BLEED VALVE SEAT LEAK TEST	EKSC, LRU	Valves	V1011.05 Sep 04	V1294.005 Seq 03	V1046.002 Seq 05				Valve Leakage Check	Hazardous gas buildup
M18U0.030-B	EZ COMPONENTS EXTERNAL INSPECTION	EKSC		V1011 02 Seq 04						Handling Darrage, Clearence Chacks, Loose Spot Welds on or Meltad TPS	
418U0.030-C	E3 COMPONENTS EXTERNAL INSPECTION	EKSC		V1011 02 Seq 04						Handling Darrage, Clearence Checks, Loose Spot Welds on or Melted 7PS	
V418Q0.032	FUEL BLEED VALVE BELLOWS LEAK TEST	LAU	Valves	V1011.05 Seq 10	V1294 005 Seq 03	V1046 002 Seq 07				LRU - Remove and replace verification	Hazardous gas buildup
418U0.031-B	E2 MCC BONDLINE ULTRASONIC INSPECTION	EKSC		V1011.02 Seq 05			V1038VL2 Seq 08		COMBUSTION	Internal Debonds -> Emplosion, Crit 1, External Laak, (JA) to Crit 1	
W418U0.031-C	E3 MCC BONDLINE ULTRASONIC INSPECTION	EKSC		V1011 02 Seq 05			V1038VL2 Seq 08		COMBUSTION	Internal Debonds -> Emplosion, Crit 1; External Leak, UAI to Crit 1	
V418Q0.034	OXIO BLEED VALVE BELLOWS LEAK TEST	LRU	Valves	V1011.05 Seq 11	V1294.006 Seq 03	V1046.003 Seq 09				LRU - Remove and replace verification	Hazardous gas buildup
V41B50 020-A	E1 HPFTP TORQUE TEST	A, RI, PLRU	<b>НР</b> ЕТР	V1011 03 Seq 09	V5606 085U 1				TURBOPUMPS	Verify the rotor is free to rotate prior to testing	Improper start, Ox rich resulting in engos fire
V41850 021	HPFTP INVESTIGATIVE TORQUE	F	HPFTP	¥1011.03 5eq 09	V5E06 0SSU 1			:	TURBOPUMPS	Investigative torque check if the specification limits are exceeded	Improper start, Ox rich resulting in engne fire

Table 8. Engine requirements database (Continued).

OMRSD NUMBER	CMRSD DESCRIPTION (V41 FILE HI DATED 9/15/95)	OMRSO Effectivity	Compenent	OPF DMI's	ENGINE SHOP OMI's	VAR/PAD OMI's	OTHER OMI's	RT OMI's	SUBSYSTEM CODE	OMRSD RATIONALE/ROOT CAL/SES	Root Cause Categories
V41AL0.010-A	ET GIMBAL ELECTRICAL BONDING TEST	i, ER	Avionica				V5005 Seq 06		AVIONICS	Verifies proper stactmost grounding conditions assist between the SSME girobal bearing and the orbiter structure. Test performed each time the bonding strape and delatined.	Unscheduled Maintenance Action or Launch Delay
V41AL0.020-A	E1 ELECTRICAL INTERFACE PANEL BONDING TEST	I, ER	Avionica				V5005 Seq 06		AVIONICS	Verifies proper electrical grounding conditions exest between the SSME electrical interface panel and the orbitar allucture. Test performed each time the bonding stripe are delectrical.	Unscheduled Maintenance Action or Launch Delay
W1AL0 030-A	E1 SSME/TVC ELECTRICAL BONDING TEST	A, I, ER	Avionics			51287 DSSU 3			AVIONICS	Verifies proper electrical grounding conditions exist between the SSME TVC actuator attach points and the orbiter structure. Test performed each time the bonding structure or described.	Unscheduled Maintenance Action or Launch Delay
V41AN0.010-A	E1 SSME CONTROLLER POWER APPLICATION	A, ER	Awtonics					V9001VL4 Seq 02	AVIONICS	Defines the proper asquancing of cockpit ewritches for application of SSME controller power as well as the values of the monitored responses. Identifies the constraints for cooling as and FACOS power.	Unscheduled Maintenance Action or Launch Delay
V41AN0.020-A	E1 AC POWER REDUNDANCY VERIFICATION	A, ER	Avionics			V1046.001 Seq 04		V9001VL4 Seq 02	AVIONICS	Provides for SSME AC power redundancy verification while controllers are under power load.	Unecheduled Maintenance Action
V41ANO.022-A	ET CONTROLLER POWER SUPPLY REDUNDANCY VERIF	A, LRU	Avionica	V1011.06 Seq 82	V1294 002 Sag 08	V1046.001 Seq 04		V9001VL4 Seq 09	AVIONICS	Performs a redundency verification of the SSME controller power supplies. Controller charmels A&C and B&C are verified. The procedure sets overfiles the backup memory power is functional and verifies the AC supplied -	or Launch Delay Unacheduled Maintenance Action or Launch Ostay
V41AN0.023-A	E1 CONTROLLER 20V MEMORY TEST	LRU	Avionics		V1294.002 Seq 03				AVIONICS	Verifies the capability of the 28 volt DC and battery systems are holding up the controller marrory.	Unscheduled Maintenance Action or Launch Delay
V41ANO.035-A	E1 COMMANDED CONTROLLER CHECKOLIT	A, ER, LRU	Avionics	V1011 06 Seq 02	V1294 002 Seq 07	V1046.001 Seq 04		V9001VL4 Seq 09	AVIONICS	Controller Changaout Varification. Functional hardware and software chackeut	Uracheduled Maintenance Action or Launch Delay
V41ZA0.010	SSME HARNESS REPLACEMENT RETEST	LRU	Avionics		V5E02 Seq 27				AVIONICS	Defines the continuity and mediction resestance tests to be performed on any replacement herness installed on an engine	Unscheduled Maintenance Action or Launch Delay
V72A00.020-A	ENJ 1 READINESS TEST	A, LRU	Avionics				V9001VL4 Seq 02		AVIONICS		Unscheduted Maintenance Action
V41AU0.060-A	E1 GIMBAL BEARING SENSOR CHANNELIZATION VERIE	ER, LRU	Instrumentation			V1046 001 Seq 12		V9001VL4 Seq 02	AVIONICS	Instrumentation integrity checkout	Unacheduled Maintenance Action
V41AU0.090-A	E1 POST-FLT STRAIN GAGE CHECKOUT	A. FKSC	Instrumentaitun	V1011 02 Ser 04					AVIONICS	Part of this should in Weld #3 Strain Gags checkout needed to ensure electrical continuity of gags after bond is sesured	or Launch Delay Unscheduled Maintenance Action or Launch Delay
V41AU0.090-D	E1 POST-FLIGHT SENSOR CHECKOUT	A, EKSC	instrumentation					V9001VL4 Sep 02	AVIONICS	Instrumentation integrity checkout	Unscheduled Maintenance Action
V41AU0.016-A	E1 MADS INSTRUMENTATION VERIFICATION	A, ER	Instrumentation			V1046.001 Seq 13		V9001VL4 Seq 02	AVIONICS	Instrumentation integrity checicust	Or Launch Dalay Unecheduled Maintenance Action
V41AU0.020-A	E1 SKIN TEMP CHANNELIZATION VERIFICATION	ER, LRU	Instrumentation	V1011.06 Seq 08	V1294 002 POSLI 11	V1046 001 Seq 13		1	AVIONICS	Instrumentation integrity checkout	or Launch Delay Unacheduled Maintenance Action
V41ALI0.042-A	E1 HPOTP STRAIN GAGE DEBOND TEST	A, PLRU, I, NRAT	Instrumentation		V5E02 Seq 27 & V1294 002				AVIONICS	Weld F3 Strain gage in place to detect uneven bearing weer — debond test needed to ansure acceptable data on next light	or Launch Delay Unecheduled Maintenance Action or Launch Delay
V41AP0.020-A	E1 MFVA PRI HEATER POWER ON COMMAND	ı	Valves						AVIONICS	Changeout Verification	Unscheduled Maintenance Action
V41APO 020-D	E1 MFVA SEC HEATER POWER ON COMMAND	ı	Valves						AVIONICS	Changeout Verification	Or Launch Delay Unacheduled Maintenance Action
V418U0.351-A	E1 POST FLIGHT MCC LINER POLISHING	EKSC	MCC	V1011 02 Seq 05			V1038VL2 Seq 08	<u> </u>	COMBUSTION	Persone Liner Roughness from Intense Environ>	or Launch Delay Unacheduled Maintenance Action
V418U0.352-A	E1 PRELAUNCH MCC LINER POLISHING	A	MCC		T	S1287 OSSU 9		· †	COMBUSTION	Erosion -> Lestage, Performence Loss Remove Surface Oxiditation -> Erosion -> Lestage,	or Performance loss Unachaduled Maintenance Action
V418U0.093	HGM FUEL SIDE DYE PEN INSP (PHASE II)	TC	Powerhead		V5E06 Seq 12			<u> </u>	COMBUSTION	Performance Loss Liner Mat. I & Transfer Tube Weld Thru-Cracks -> By-pass	or Performance loss Unscheduled Maintenance Action
V416U0.096	HGM 0000 SIDE DYE PEN INSP (PHASE II)	тс	Powerhead		V5E02 Seq 14		-	<del> </del>	COMBUSTION	Flow Performance Loss Liner Mat 1 & Transfer Tube Weld Thru-Cracks -> By-pass	or Performence loss Unscheduled Maintenance Action
V418U0.097	HGM FUEL SIDE DYE PEN INSP (PHASE II+)	TC	Powerhead		V5E06 Seq 12		1	<del> </del>	COMBUSTION	Flow Performance Loss  Liner Mat. 1 & Transfer Tube Weld Thru-Cracks -> By-pass	or Performance loss Unacheculed Maintenance Action
V418UD.098	HGM OXID SIDE DYE PEN INSP (PHASE II+)	TC	Powerhead	<u> </u>	VSE02 Seq 14		<del>                                     </del>	-	COMBUSTION	Flow Performance Loss Liner Mat 1 & Transfer Tube Weld Thru-Cracks -> 8v-oses	or Performence loss Unecheduled Mentenance Action
V72AQQ 040-A	VERIFY SSME 1/EIU 1 COMMAND PATH	A LRU	Autonius	ļ			-	<b>.</b>		Flow Performance Loss	or Performance loss.
V72AQD.050-A	VERHEY SSME 1/EIU 1 STAT CHANNEL PATH	A, LRU	Avionica	†			V9001VL4 Sep 02 V9001VL4 Sep 02		AVIONICS		
V72A00.060-A	EIU 1 PM SYSTEM INTERFACE DATA	LRU	Avionica			50017VL13 Seq 42		1	1	<u> </u>	1

Table 8. Engine requirements database (Continued).

OMRSO NUMBE R	OMRSD DESCRIPTION (V41 FILE IN DATED 9/15/95	OMRSD Effectivity	Component	OPF OMI's	ENGINE SHOP OMI's	VAB/PAD OMI's	OTHER OMI's	RT OMI's	SUBSYSTEM CODE	OMRSD RATIONALE/ROOT CAUSES	Root Cause Categories
Y7ZAW0 030-A	EIU I POWEN REDUNGANCY VERIFICATION	A. LRU	Avence				¥8001¥L4 8+e 02		AV-ONICS		
7418UB 420 A	ET HEAT SHIELD SLANKET INSPECTION	A	Heat Shard			\$1287 See 04			46A7 SH 610	Thermai Defermations > Aft Leaft to Atmosphere >	
V418U0 4Z1 A	£1 EMHS   NSPECTION	A	Heat Shald	V41 40018			<del></del>		HEAT BHIELD	16vi 12	+
V41 EUO 850	HYDRAULIC DRAID LINE INSPECTION (TIME & CYCLE)	TC	L-nee/Ducts		V1294 002 649 18	V1046 001 Sec 13			HYDRAUL-C	Periodic inspection (every 10 texts) of hydrautic satuster shaft same	
V55AG0.121-A	BUPPLY OD PRE MATE INSPECTION	1	Lines/Duets				V9002 06 Sec 03		HYDRAULICS	Verify Configuration	
V58AG0.121-0	RETURN OD PRE MATE INSPECTION		Lines/Ducts		-		V9002 06 See 01		HYDRAULICS	Verify Configuration	<del></del>
V98AGQ 121 A	SUPPLY OR DEMATE INSPECTION		L-nee/Dusts	· · · · · · · · · · · · · · · · · · ·			V\$002 06 844 02	-	HYDRAULICS		
Y98AG0 121 B	RETURN OD DEMATE INSPECTION		L-man/Duesa	<u> </u>			Y9007 D8 Bes 01		+	· · · · · · · · · · · · · · · · · · ·	+
V41080 060-A	E1 MCC INJECTOR INSPECTION	EKBC	wcc		V1294 005 844 02				COMBUSTION	<u> </u>	
			<del></del>	V1011.01 P09U 5	***************************************		V1036YL2 See DA			H2O or Contaminante in Acquete Cavitae	
V41C90.004-A	E2 BBME NOZZLE BUMPER INSTALLATION	PLCL	Mozzie	80024 814 19			80026	V1035VL2 Sre 14	COMBUSTION	Install Protester Bumpers for Graund Transport prior to STS Stock > Alt Manifold Impact, "http://cack > Leakage to or Burst, Crit. 1	
V41BQ8,088-A	ET PCA FUEL BIDE INTERNAL LEAK TEST	EKSC, LRU	PCA	V*011 05 Sec 12	V1294 002 Seq 10	V1046 386 844 04	V1011 06 Sec 03	The state of the s		Com kones test demonstrates that the amergency shutdown PAV went part and is not leasing beyond acceptable limits. Also chooks fuel purge and bland	
Y41800.381-A	E1 PCA LOZ BIDE INT/HPV ST/EFT BL	ECOC. LAU	PCA	VT011 09 8+q 12	V1294 002 844 10	Y1045 306 3ee 04	V:01: 35 Een 03			valve and haids and flust jurge PAV.  Combined best down entropies that the emergency should be supported by the second of the s	
V418G0 002	PCA LO2 BIDE/HPV LKG IBOLATION	•	PCA	TBD			<del> </del>	1		are verified.  Performed anny water combined test indicates second- labelege	
V41450 020-A	E1 PREUMATIC CHECKOUT	EKAC, ER, LAU	Presmatice	V1011 05 8ec 04	V1284 002 Bug 11	V1046 001 844 06	1	<u> </u>	540.45	Planned Prelight Cheateut	
V41BUG 073-A	ET PREUMATIC VERT FLARGE VERIFICATION	TC, LRU	Presmatee		V1294 002 Bee 10					Flaw Ventioation	************
Y418U0 030-A	E1 COMPONENTS EXTERNAL INSPECTION	EKBC	tystem	V1011 02 544 54				<u> </u>		Manding Damage, Cwarence Chocca, Lanes Spot Weide an or Marted TPS	
V41Bu0.023	FUEL BYSTEM LAI (MEPECTION	Exac	System	V1011 02 Bes 04			1	-	<b>†</b>		
V41BUE 200-A	ET HELIUM BARRIER SYS HEMPECTION	A. LRU	System			\$1257 Seg 06	V9018 002 8ea 07	Ť	риств	Varify Bag littgat	1
941860 110 A	ET BOME TO UNOTER GIMBAL CLEARANCE	ER, MOD, LRU	Byeten	V1063 8em 14					1	contriberana Chaex	
7418U0.520-A	EI GIMBAL GLEARANCE CHECK	E4. #00, LRU	System	V1063 See 14	<b>†</b>		<del>                                     </del>	<del> </del>	+	+	
V41 BU 0.530-A	ET BRME-TO ENHS CLEARANCE CHECK	A	System	V41-50024			<u> </u>	1	HEAT SHIELD		<del> </del>
V418W8 831-A	EI PREPS FOR OPT ROLLOUT	*	Вуртан	V41 20003					nta-santep	Verfice that the angune is an figured for transfer from the OPF. TVC actuator locks restrain angular movements.	
V419WG 034	INSTL BOWE STORAGE/SHIPPING COVERS	ERB	Bysnim	V5017						and severe pretest against contemination  Defines the conditions governing use of the subject	
V418W0 060	OPENING CLOSCOUT COVERS	ENV	tyson .	V90s7	1		<del> </del>	†	1	3'diptime cavers	+
¥41C80 010	BAME POSITIONING POST LANDING	PLGL	\$1100				80026			Winners rain an either sentaminante entry into the	
941088 812 A	ET HE BARRIER BYS INSPECTION POST	Exac	System	V1263 Req G4		VSD1 8 002 Sec 07	V1038VL2 Seq 06		DUC'S	nazzia Verify Bag Intset	<del>                                     </del>
V41 C DE 020	FERRY FLIGHT BET INSTALLATION	11	1 prome	T	<del>                                     </del>	· · · · · · · · · · · · · · · · · · ·	W. 434W. 3 444 05	t	<u> </u>		+
V41680 880 D	ENGINE DAVING - 187 PURGE (PHANE III)	ECSC	System		Y1284.608 Sag G4		A-036AFS gad 00		COMBUST DR	Treath Postation Course, as her "Pages Bash" by Control the came used to partie majors drying astronome fortuning such flight: Pressures, the partiers, immove durations and configurations are defined.	

Table 8. Engine requirements database (Continued).

OMRSO NUMBER	OMRSD DESCRIPTION (W41 FILE IN DATED	OMRSD Effectivity	Component	OPF OMI's	ENGINE SHOP DMI's	VAR/PAD OMI's	OTHER OMI's	RT OMI's	SUBSYSTEM CODE	OMPSD RATIONALE/ROOT CAUSES	Root Cause Categorius
V41CB0.080-E	ENGINE DRYING - 2ND PURGE (PHASE II)	EKSC	System		V1294 006 Seq 04				COMBUSTION	Controls the criteria used to perform engine drying operations following such flight Pressures, temperatures, minimum durations and configurations are defined	
V41C80.061	DRYNESS VERIFICATION (PHASE II)	EKSC	System		V1294 008 Seq 05			V - 1.	COMBUSTION	Requires a verification of dryness, defined by a misomum mosture criteria, to be performed following completion of drying operation	
V41A50.030-A	E1 FRT CHECKOUT	EKSC. ER, LRU	Systems	V1011.06 Seq 06	V1294,002 Seq 13	V1046.001 Sec 08			ENGINE	Planned Preflight Checkout	
V41A80.030-D	E1 FRT PNEUMATIC SHUTDOWN SEQ DATA VERIF	EKSC, ER, LRU	Systems	V1011.06 Seq 08	V1294 002 Seq 19	V1045.001 Seq 13			ENGINE	Plenned Preflight Checkout	
V41BLID 13D-A	E1 YAW MPS TYCA ALIGNMENT	LRU, 1ST	TVC	TRO				1			
V418U0.130-B	E1 PITCH MPS TVCA ALIGNMENT	I RUL 18T	TVC	IBD							
V41ASC-010-A	E1 ACTUATOR CHECKOUT	EKSC, ER, LRU	Valves	V1011.06.8eq.05	V1294 002 Seq 12	V1046.001 Sec 07			ENGINE	Plenned Preflicht Checkout	
V418Q0.040-A	E1 OXIOIZER PROP VLVS/PRG C/V LEAK TEST	EKSC, I	Valves	V1011 05 Seq 09	V1294 D12 Seq D4	V1046 004 Seq D4	V1294 005 Seq 06			Check Velve Failure - Contamination; 8TS-55 abort	
V418Q0.041	OXIDIZER PROP VLVS/PRG C/V	F	Valves	1	V1294.012 Seq 04		1			Isolation check if the V41BQ0.040-A leakage limits are exceeded	
V41B00.120-A	E1 LO2 PROP VALVE BALL SEAL LEAK TEST	EKSC, ER	Valves	V1011.05 Seq 07	V1294 007 Seq 03	V1046 003 Seq 04				Valve Leakage - LOX system integrity check	
V418Q0.121	LOZ PROP VALVE BALL LKG ISOLATION TEST	F	Valves	TBO						Isolation check if the V41800 120-A leakage limits are exceeded	
V418Q0.130	RIV SHAFT SEAL LEAK TEST (TIME & CYCLE)	TC	Varives	TBD						Valve Leakage	
V41B00.140-A	E1 RIV SEAT FLOW TEST	FKSC	Vahen	V1011.05 Seq 06	V1294.006 Seq.03	V1046.003 Seq.06				Value Lesians	
V41800.141-A	E1 OBV SEAT LEAK TEST	EKSC LRU	Valves	V1011.05 Seq.06	V1294,006 See 03	V1046.003 Seq.06	ļ.,,,,	I		Valve Lankage	
V41800 150-A	E1 GCV CHECK VALVE LEAK TEST	EKSC, LRU		V1011.04 Seq 06	V1294 006 Sea 03	V1046 003 Sec 06				Valve Lealings	
¥41B00.180	HPV CHECK VALVE LEAK TEST	IC	Valvas	TBO					1	Valve Leakage	
V418Q0.190	OPOV SLEEVE TEST & WINDOW CALIS	I, LRU	Valves		V1294.002 Seq 14	V5E17 Seq 09	1			Sets Open Loop Command % - Used to adjust start sequence	
V41800.191	FPOV SLEEVE TEST & WINDOW CALIB	I, LRU	Valves		V1294.002 Seq 14	V5E18				Sets Open Loop Commend % - Used to adjust start sequence	
V41BU0.070-A	ET AFT CLOSEOUT INSPECTION		Valves		t	\$1287 OSSU 8	† · · · · · · · · · · · · · · · · · · ·	<del> </del>	† · · · · · · · ·	Final look before leunch	

## **APPENDIX B—Scheduled SSME Operations Data**

The following spreadsheets present the detailed data collection from SSME processing experience at KSC relative to scheduled activities. Tables 9–12 present the summary information relative to figures 6 through 9. Following that, the specific processing tasks for the four flows appear in tables 13–16. Finally, an example of the existing level of detail supporting the flow layouts is presented in table 17. Note also that a zero in a work column only reflects that no engine processing personnel are required for that task.

Table 9. OPF SSME postflight planned operations.\*

OMRED WUMBE R	OMPSO DESCRIPTION (V41 FILE III DATED \$(14/98)	GMRSO EFFECTIVITY	Component	OPF OMI's	ENGINE SHOP	VAB/PAD OMF:	OTHER DMI's	RT OMI's	CODE	OMRSO RATIONALE/ROOT CALIBES	Rest Cause Estaportes
V418L0 080	BOANE WELD 22 & SA LEAK CHECK	PREC, NRAT	HPOYP	V1011 06 deq 07	V1294 007 Box 04	V1048 003 8ag 0/				Due to poor proceeding, 19POTP belance confly element. while are teak-shouldered. No leaks over yerfleet, but suck or wide previous team or over the providence of the second of the second over the second ov	Aft Comparine t overpressurfaction or fire
V41BL2 080 A	E1 HPOTP PLUG WELD LEAK CHECK	PKSC, NRAT	неоте	V1011 06 See 06	V1264 004 Bag 04	V1046 004 844 04	V1294 005 Bug 07			Plug wold look consured on a unit. Concern over those wolds leaking althor Gou/Hollum/Hot gas into trooping.  therefore all enternel plug wolds on the housing are an extent.	All Competends overpressurtation of the
V41AXD GPS A	E1 LDE FEED (JOINT 01) UF LK CK	ER. PR. OMOP	Unes/Ducte	V1011 08 Beq 07		V1046 003 8eq 05			DUCTE	Errours joint integrity of LPOTP to pump inter ducting other engine to installed	Aft Compartment preference better or fire
V41AX0.000-8	E1 LHZ FEED (JOINT F1) UF LK CK	ER, PR, OMOP	Limes/Ducto	V1011 06 Beq 05		V1048 002 Beq 04			DUCTO	Verify pump infet joint integrity after metalling the LPFTF	Aft Compartment
V41AX0.020 C	E1 GHZ PRESS (JOINT PS 3) UF LK CK	ER, PR. DMOP	Lines/Ducts	V1011 05 Beq 00		V1049 004 See 04	1	1	DUCTS	Joint Integrity Post Engine Installation	Aft Comportment
94 1AKG 000 D	ETILOS BLEED (JOINT 015) UT LK CK	ER, PR. OMOP	Limes/Ducts	V1011 05 Bee 07	·	V1048 003 Seq 06	T		DUCTS	Joint Integrity Post Engine Installation	Aft Compartment
V41AX0 000 #	E1 LIG BLIED (JOINT F4 3) UF LE CK	ER, PR, DMDP	Unes/Duste	V1011 05 Beq 05		V1040 000 See 04	†	<b>†</b>	DUCTS	Joint Integrity Post Engine Installation	At Compartment averpressurfattion or fire
V41AX0 020-F	ET HELIUM (JOINT PT) UF LK CK	EN, PR. OMOP	Umes/Duele	V1011 05 0va 12		V7048 001 Beq 05	V1048.008 Burg 04		DUCTS	Joint Integrity Post Engine Installation	Aft Compartment
V41AX0.000-8	E1 GNE (JOINT N1) VT LK CK	ER, PR, OMOP	Linea/Dueta	1	† ·	V1149 8eo 15	V1046 006 Beg 03		DUCTS	Joint Integrity Post Engine Installation	Aft Compertment
V41AX0 020-H	E1 HVD - PRESS (JOINT H1) UF LK CK	ER, PR, DMOP	Unes/Duste	·	VSE17 Box 00		VSE18	V9002 06 8mg 05	DNCTA	Joint Integrity Post Engine Installation	Aft Compartment
V41AE0 020-1	E1 HYD - RETURN (JOINT H17) UF LK CK	ER. PR. OMOP	Lines/Ducte	-	V6E17 Beg 00		V0E 10	V9002 08 Beg 05	DUCTS	Joint Integrity Post Engine Installation	Aft Compartment
V41AX0.050 A	E1 GOZ ORB/BBANE INTERPACE FLANGE	A. ER	Lines/Chuite			V1049 005 Sec 05			DUCTO	Joint Integrity Post Engine Installation	overpressurtaution or fire
V418L0 001	BONE ENCAPOLICATION POWER HO LEAR CK	EKAC & ER	Commitment	·	V1294 007 Sen 04		-		ENGINE	System leak integrity object for learneh Max I or Ward	Aft Compartment overpressurigation or fire Aft Compartment
V418L0 039	SOME ENCAPSULATION FUEL BYS 180 TEST		System		V1994 007 Beg 04		ļ. ·		FAGINE	Thru Crack, See not Sected -> Crit 1 System less integrity check for leaneh - East 1 or West	everpressurbatton or fire
V418L0 003	SSME ENCAPSULATION OXID BYS ISO TEST	,	Bystom		V1204.007 See 04				· · · · · · · · · · · · · · · · · · ·	Thru Crash, Goal not Booted -> Crit 1	AR Companions overpressurtation or fire
VATEL O COM	SEASE ENCAPSILLATION HOT GAS SYS ISO TEST		Brotom	<b>.</b>	V1254 007 8m 04				ENGINE	System leek integrity check for learnth - Mat 1 or Weig Thru-Creek, Seel not Seeled -> Crit 1	Aft Compartment overpressurigation or fire
V418F0 010 A	ET GOS/GCV ENT LK CK & DRIPCE VERIF	BIGBG. I	Vehree						EMQ INC	System lank integrity check for leanesh - Mat 1 or Waid Thru Creek, Seel not Seated -> Crit. 1	AR Compartment overpressurteston or fire
4418-0.010 X	ET GODGET EN EN EN EN EN EN EN EN EN EN EN EN EN	ERAC, I	Velvas	V1011 04 Bug 07	V1264 002 Beg 17	V1046 005 Beq 05	V1204 000 Beq 05	-		Established test test of all generous copygan system juints from the AFV to the urbitar interface on an east. Fight begin	Aft Compartment overpressurgation or fire
V41A00 010-A	E1 SENSOR CHECKOUT	EKAC, ER, LRU	Instrumentation	V1011 08 8mg 02	V1294 002 Sug 09	V1045 001 848 04	<b>†</b>	V9001VL4 844 89	AVIONICS	Planned Profigiti Chaeliout	Erromeove shutdown, take of vehicle
V414U0 018-A	ET OPERATIONAL INSTRUMENTATION VERIFICATION	A. ER	Instrumentation			V1048 001 8mg 04	*	V9001VL4 Beq 02	AVIDNICS	instrumentation integrity checkout	Erronoous shubdown, lago of vehicle
V418U0 250-A	E1 SENSOR IR VERIFICATIONS	EKBC, LAU	Instrumentation	V1011 02 000 07				T		Functional cheek of each turbina deeparge tomp	Erromatous shutdown, loss of vehicle
V418P0.020 A	E1 HEX COIL LEAK TEST	A, EKSC, PLRU	HEX	V1011 04 844 02	V1294 003 6+4 03	V1048 005 Box 05			HEX	Mat 1 (otringer) or Weld Thru-Crast, HPOTP Intestigation Impact Hole -> HS to Tank, Crt. 1	Fire, Uncontained engine feature
V419P0 000	BAME HEX COIL PROOF TERT	PL/IU	HEX	V1011 04 Bee 02	V1284 005 Bee 04	V1046 005 Beg 0/	†	1	HEX	Med 1 (estringer) or West Thru-Crook, HPOTP Installation	Fire, Uncontained engine faiture
V4180.00.004	HEX EDDY CURRENT INSPECTIONS (TIME & CYCLE)	TC TC	HEX	V1011 02 800 11				1	нех	Impass Hale > HS to Yenk, Grit 1 Thin Walls from Braston Weer, Manut > Thru Grank, HS	Fire, Uncentained angles failure
V418U0 118	HEAT EXCHANGER INSPECTION	tc	HEX		V5E02 See 14		T		nex	Leakage to Yank, Crit. 1 Visite Impact Demage, Bracket Wear :> Thru-Crack :> 165 Tank, Crit. 1, Turn. Vanc Cracke :> Leas of Verse Impact All Poot :> Demage or Crit. 1	Fire, Uncombined engine failure
V41 BU0 126 V41 BU0 076-A	HEX VIBUAL INSPECTION  EX HIPPYP INTERNAL INSPECTION	PLRU PKBC	HEX		V5002 Baq 12		t	1	HEX	HPOTP Installation Impost Hole -> HS to Tank, Crs. 1	Firs, Uncontained angine future
V41800 076-A	ET HAVE MEMBER MADE CTION		, marrie	V1011 02 8-4 08					TURBORUMPS	Verify he linkt or dreahlarge sheet metal creaking, he nossis areaching or arrosion, no blade creaking, pletform or aching, or wowen, no fel-mouts seed creaking or making places, no belowe sheet or aching (All inspections acong lates) with fur-begung ine	Fire, Uncontained engine failure
V418U0 079	IMPTER PRINT STAGE BLACK 28X	TC, DCE	HOPTO		V5208 8eq 14		<del> </del>	1	TURBOPUMPE	Verify no blade cracking due to provious popurranees of all oil cracking	Fire, Uncontained engine failure
V418U0 000	HATTP TURBING INSPECTION (TIME & CYCLE)	PRINC	lette		VSCOR Bue 14				fultaceumps	Varify no inlet or disease sheet motel enacting including wold 450 and the turning series, no noggle oracting or enature, no their creating, selection enabling, or enation, no flathmouth seal enabling selecting or miseling pleases, no before shield creating year by	Fire, Uncommence angine feliare
V418U0 087	HPFTP BELLOWS HEIGHT VERIF	PLAN	HETE		VSEOR DOMU 2		1	ľ	TURROPUMPS	Verify betteres height dissults to provide proper prehad on the believe of installation. Incorporated as a result of a previous failure of the bulleurs.	Fire, Uncombined angles failure

<sup>\*</sup>Based upon three-engine set

Table 10. OMEF SSME planned operations.\*

OMRSD NUMBER	OMRAD DESCRIPTION (V41 FILE IN DATED 9/15/95)	OMRSO EFFECTIVITY	Compenent	OPF OMPs	ENGINE SHOP OMI's	VAB/PAD DMCs	OTHER OMI's	AT OMI's	SUBSYSTEM CODE	OMRAD RATIONALE/ROOT CAUSES	Reel Cause Catagories
V41CB0 060-A	E1 HPFTP TURBINE BEARING ORVING	EKSC	неете	V1011 01 Beg 03		V9016.002 Beq 04	V1036VL2 \$eq 07	•	TURBOPUMPS	Ensure all mosture is removed from the bearing area other a teat/flight	Fire, Uncontained engine fallure
/41800 110-A	ET HPOTP PRIMARY OXID SEAL LEAK TEST  ET HPOTP TORQUE TEST	PKBC, NRAT	неоте	V1011 06 Sea 07	V1294 006 Reg 03	V1046 003 Seq 07				Cheeks for assessive leakage of LOX/GOX from the HPDTP ceal.—Protects against exceeding flow overcoming the barrier seal and from heaving exceeding the tarking all the seal and from of the arigine. Kat-F ceal doce were during operation.	Fire. Uneoritained angine failure
V41 RBO 042	HPOTP INVESTIGATIVE TORQUE			V1011 03 Beq 08	VSECT Bog 25				TURBOPUMPS	Dank to ensure rotor is not bound up prior to start— consern over commanisation if high and also start sharasteristics of loser is elieute to self-contamination has been found afound the rotor but only ones enough to effect start (rusted Iff bearings)	Fixe, Uncontained engine failure
		F, NRAT	HPOTP	V1011 03 \$mq 08	VBEQ2 Beg 25				TURBOPUMPS	Done only to run in a high torque pump to bring the torque value below ages requirements	Fire, Uncontained angine failure
/41880.042 A	ET HPOTP IMPELLER LOCK VERIF	PKSC, PLRU, NRAT	неоте	V1011 03 Beq 08	VSEOZ Beq 25				TURBOPUMPS	Leading feature was oversome on a HPOTP PBP impariar both took during torque testerispinning of pump for inspections. Resurrance central is to only turn the pump in the both tightening direction during inspections and to eleven the location feature state at	Fire, Uncontained angine failure
		PKSC, NRAT	неоте	V1011 03 Seq 06					TURBOPUMPS	Turbrier bearings have worn very quickly in past—this measurement is to ensure that the bearings are still expelled of 1 flight prior to a launch	Fire, Uncomained angine falture
418G0 110-A	ET ATD BLOCK VII HPOTP PRIMARY OXID BEAL LEAK TEST	PKBG, NRAT	неотя	V1011 05 Sec 07	V1294 006 Eeq 03	V1046 003 Beg 07				This look shook was never performed during HPDTP/AT sertification. The deta obtained be errate and is probably indicatine of only grose seal imperfections (which would most little) be detected through breque shocks). It is ourself as OMR80 requirement.	Fire, Uncontained engine fallure
/419U0 064-A	E1 HPOTP INTERNAL WISPECTION	PKBC, NRAT	неоте	V1011 02 24q 08					TURBOPUMPS	Visual inspections of turbine hardware (ehestmetal/ MEXISSE bladles) due to erasking and ercelon essen in the pect of the main purp initial follows due to assistation damage and sontamination found in the past, of the PBP impeter inter due to locking heat	Fire, Uncontained engine failure
7418UD 066-A	ES HPOTP TIP BEAL RETAINER	PKSC. HRAT	неоте						TURBOPUMPS	Verifier 1st stage tip seat retainer sersers have not retained. Could lead to black fally:	Fire, Uncontained engine failure
/419U0 390-A	E) LPFD DVALITY CHECK	ľ	Linea/Dusts	V1011 02 Seq 10			V9018 002 Seq 10		DUCTS	Contingency that performed only when the LPFC helium barrier cyclem has been damaged. Object is to detect potential dust colleges or separation from the layer of insulation by massuring the roundness of the dust	Fire, Uncontained engine failure
V41BUG 400	PERFORM LPFD XRAY INSPECTION	•	Lines/Duets	ТӨО					DUCTE	Contingency recent preformed only when the evality sheek indicates that come damage or softgoes has cocurred in the LPFD. The croce section is X-rayed in an attempt to verify presence of damage.	Fire. Uncontained angine tallura
Y41880.060 Y41880.066	HPOTP/AT TORQUE TEST HPOTP/AT INVESTIGATIVE TORQUE	EKRC. Rt. PLRU	HPOTP	Y1911.93 Sec 98	VALUE Bon 25				TURBOPUMPS	Benieged by V41880.040 A	Fire, Uncontained engine failure
741 QUO 406	BOME LPFD TRIPPOD LEGS INSPECTION	DCE	HPOTP Lines/Ouese	V1011 03 844 08	YBEGE BOAZS		+		TURBOPUMPS	Registed by V41580 042	Fire. Unpopularized engine failure
				Teo					DUCTS	Performed to insure LPFO structural integrity Inspection is performed if your flight data swelliation reveals HPFTP unabsoptishts symbolronous fraquencies	Fire, Uncontained angine failure
41 BUO 006 A	ET ATD BLOCK WITHOUTP INTERNAL INSPECTION	PKSC. NRAT	неств	V1017 02 Bes od					TURBOPUMPS	No HPOTP/AT internal inapentions were made during outfloation. Inspections of the turbine, mainstage pump and PRP inter, and sit three bearings have been added only because the inspections aren't time one unit of the properties	
41880.01D-A	E1 LPFTP TORQUE TEST	A. RI, PRI, ER, PLRU	LPETP	VID11.03 See 04	I		·		TURBOPUMPS		
V418UQ 127	HPOTP/AT PER TEROLT LOCK	· ·	HPOTP	V1011 03					TURBOPUMPS	Yatife total is free to retain arior to testing	Fire. Uncontained angine failure Fire. Uncontained engine failure
¥418U0.128	HPOTP/AT CONTAMINATION INSPECTION	A.PKeG	нротр	¥1011.07 Seu 77		1	1		TURBOPUMPS		<del></del>
V41080 005	SOME HPOTP/AT TURBINE BEARING ORYING LPFTP INVESTIGATIVE TORQUE	PKBC	неоте	V1011 01 Seq 03	V1294 DOS Seq D4	V9018 002 Beq 04	L		TURBOPUMPS	Verify all moleture to removed from the bearing area after a teet/flight	Fire, Uncontained engine failure
V-1000 011	LPF /P INVESTIGATIVE TORQUE		LPFTP	V1011 03 Beg 04			1	. —	TURBOPUMPS	Investigative forque wheek if the epocification limits are succeeded forque sheek feliure generally lift-off see! binding or laby see! - copper plating rup	Fire, Unpontained engine failure

<sup>\*</sup> OMEF data reflects single-engine processing. For complete model, processing timelines must consider number of engines per vehicle.

Table 11. OPF post-SSME installation planned operations.\*

Process	Sub-Process	Process Description	Duration (PD)	Tech MHrs	QC MHrs	Engr MHrs	Total MHrs
V5005		SSME Installation Preps	24.00	31	37	13	81
	V5057	Stiffarm Bracket & TVCA Support Installation	4.00	8	4	0	12
V5087		Engine 1 Installation Handling GSE Operations	5.00	19	4	11.5	34.5
V5005		Engine 1 Installation Operations	7.00	42	12	25	79
V5087		Engine 3 Installation Handling GSE Operations	5.00	19	4	11.5	34.5
V5005		Engine 3 Installation Operations	7.90	42	12	25	79
V5087	i i	Engine 2 Installation Handling GSE Operations	5.00	19	4	11.5	34.5
V5005		Engine 2 Installation Operations	7.00	42	12	25	79
V5005		Post-SSME Installation Operations	32.00	88	56	0	144
	, V9002.06	SSME Hydraulic QD Demate Operations	4.00	4	4	0	
V1011.03 Run 3		LPOTP Post-Installation Torque Check	12.00	12	12	12	36
V1011.03 Run 3		LPFTP Post-Installation Torque Check	6.00	6	6	6	18
V1011.05		Orbiter/SSME Interface Verification	72.25	59	50.5	24.5	134
	V1011.04	SSME GOX System Leak Checks	. 14.00	20	12	10.5	42.5
	V9001VL4	Orbiter/SSME Electrical Interface Verification	8.00	0	8	8.	16
V41/G41/V80 JC's		Heat Shield Installation Operations	126.00	704	352	0.	1056
V1063		SSME Gimbal Clearance Checks	17.50	34.5	31.5	42	108
	V5057	TVCA Pinning Operations	4.00	8.	4	0	. 12
	V9002.06	SSME Hydraulic QD Leak Checks	1.00	1	1,	1.	3
V41-20003		SSME OPF Roll-Out Inspections	19.00	11	11 .	6.	28
	V5057	Thrust Chamber & Miscellaneous Cover Installation	4.00	4	4	0;	8
	V5057	TVCA Midstroke Lock Installation	4.00	8	4	0	12

<sup>\*</sup> Based upon three-engine set

Table 12. SSME VAB/pad processing planned operations.\*

Process	Sub-Process	Process Description	Duration (PD)	Tech MHrs	QC MHrs	Engr MHrs	Total MHrs
S0008		Shuttle Interface Testing	38.00	o	0	0	0
	V1149	GN2 Interface Leak Check & Trickle Purge Ops	30.00	9.75	11.25	12.75	33.75
	V5057	Thrust Chamber Cover Removal & Installation	1.00	1	0	0	1
\$0009		Launch Pad Validation	44.00	4	4	4	12
V1046.001		SSME Flight Readiness Test & Checkout	21.00	2	9	12	23
	V9002.06	Preps for SSME Hydraulic Operations	3.00	2	0	1	3
	V5057	TVCA Midstroke Lock Removal	4.00	8	4	0	12
	V9001VL4	SSME Controller Power-Up Operations	2.00	o	6	8	14
V1046,002		LH2 System Ball Seal Leak Check	3.00	6	5.5	4	15.5
	V9002.06	SSME/TVC Actuator Hydraulic Power Dwon Securing Rqmts	2.00	1	0	1	2
	V5057	TVCA Midstroke Lock Installation	1.50	3	1.5	0	4.5
V1046.003		LO2 System Ball Seal Leak Check	1.00	1	2	2	5
V9002.06		SSME Hydraulic QD X-Rays	4.00	4	4	0	8
V1202		Orbiter Aft Helium Signature Test	34.00		5.5	5.5	18
81005		LO2 Propellant System Conditioning	6.50	3.75	. 0	0	3.75
	V5057	SSME Chamber Cover Removal/Drain Line Adapter Installation	2.00	2	2	0	4
\$1006		LH2 Propellant System Conditioning	9.50	0	0	0	0
	V9001VL4	SSME Controller Power-Up Operations	2.00	0	2	4	6
81287		Orbiter Aft Closeout for Flight	100.00	48	42	66	156
	V9018.001	MPS & SSME Initial Preps for Propellant Loading	8.00	8	8	8	24
	V5057	TVCA Midstroke Lock Removal	34.00	68	34	0	102
	V5057	SSME Protective Cover Removal	8.00	8	0	0	8
S0007		Shuttle Launch Countdown Operations	181.37	12	83	153	248
	V9018.001	MPS & SSME Final Preps for Propellant Loading	8.00	3	3	0.25	6.25
	S1003	LO2 Propellant System Loading Operations	24.87	0	24.87	49.75	74.62
	S1004	LH2 Propellant System Loading Operations	24.87	0	0	0	

<sup>\*</sup> Based upon three-engine set

Table 13. OPF rollin to SSME removal tasks.

ID	Task Name	Duration	Work	Predecessors	Resource Names
1	OPF Roll-in to SSME Removal	271.9h	1305h		
2	Orbiter at OPF Door/S0028	0h	Oh		
3	HPFTP Bearing Drying Operations/V1011.01	24.75h	98.25h		
4	Extend Platforms 10S and 19S/V1011.01/V35xx	0.5h	1.5h		Tech[2],QC
5	Remove SSME Environmental Closures	0.5h	0.5h	4	Tech
6	Mate Bearing Drying Flexhoses	2h	4h .	5	Tech,QC
7	Retract Platforms 10S and 19S/V1011.01/V35xx	0.5h	1.5h	6	Tech[2],QC
8	MCC Acoustic Cavity Inspections/Install Throat Plugs	4h	8h		Tech,QC
9	Mate Bearing Drying Exhaust Duct	4h	12h	8	Tech[2],QC
10	Install SSME Bellows and Miscellaneous Covers/V5057	3h	<b>6</b> h	19	Tech,QC
11	Establish Safety Clears	0.25h	1.25h	9	Tech[2],QC,Safety,Engr
12	HPFTP Bearing Drying Purge Initiated	0h	0h	11	
13	Perform SSME Bearing Drying	8.5h	42.5h	12	Tech[2],QC,Safety,Engr
14	Perform Filter Inspection and Cleaning	2.5h	5h	13	Tech,QC
15	Disassemble Test Setup and Remove Throat Plugs	8h	16h	13	Tech[2]
16	Establish Aft Access	5h	0h		· · · · · · · · · · · · · · · · · · ·
17	Install Entry Level Platforms/V35-00001	2h	0h		
18	Install Floor Level Platforms/V35-00001	3h	0h	17	
19	Aft Access Available	Oh	0h	16,18	
20	OPF Bay Open for Normal Work	0h	0h	19	
21	Orbiter Initial Power-Up	Oh	Oh		
22	Helium Baggie Leak Check/V1263	12.5h	43.75h	20	
23	Install TVCA Midstroke Locks/V5057	3h	<b>9</b> h	20	Tech[2],QC
24	Verify Throat Plugs Removed and MPS/SSME Helium Tanks Pressurized	0.25h	0.75h		QC,Engr[2]
25	SSME Controller Initial Power-Up/V9001VL4	4h	8h		Engr,QC
26	Establish Safety Clears for Helium System Activation	0.25h	1.5h	24,25	Tech,QC[2],Safety,Engr[2]
27	Perform SSME 750 psi Helium System Activation	0.75h	4.5h	26	Tech,QC[2],Safety,Engr[2]
28	Perform LPFD Helium Barrier Inspection per V41CB0.012	3h	15h	27	Tech,QC[2],Engr[2]
29	Perform SSME 750 psi Helium System Securing	0.5h	1h	28	QC,Engr
30	Install LPFD Purge Blanking Plate Adapter/Remove Baggies	4h	4h	29	Tech
31	SSME Drying Operations/V1011.01	45.5h	173h	22	
32	Mate GN2 Purge QD to Orbiter @ PD14	4h	12h		Tech[2],QC
33	Install Heise Gages @ TP24 and TP25	1h	2h	32	Tech,QC
34	Assemble/Mate 15 Purge Hose/Filter Assemblies	8h	16h	20	Tech.QC
35	Remove Joint F6.10/F6.11 Plugs/Boroscope for Moisture	2h	4h		Tech,QC
36	Install Joint F6.10/F6.11/G4.3/N16 Adapters	1h	2h	35	Tech,QC
37	Loosen Bolts @ Joint N14 Plate	0.5h	1h	36	Tech,QC
38	Install LPFTP Anti-Rotation Tool	0.75h	1.5h	37	Tech,QC
39	Install Shim @ Joint D35.2/N11.2 Transducer Stack	0.75h	1.5h	38	Tech,QC
40	Install Shim @ MCC Pc Transducer/Inspect for Moisture	3h	6h	39	Tech,QC

Table 13. OPF rollin to SSME removal tasks (Continued).

ID	Task Name	Duration	Work	Predecessors	Resource Names
41	Install Throat Plug/Monitor Gage/Drain Line Adapters	3h	6h	34	Tech,QC
42	Mate Flexhoses @ HPOTP Turbine Primary Drain Adapters	1h	2h	41	Tech,QC
43	Mate Flexhoses @ Joints F6.10/F6.11/G4.3/N16 Adapters	2h	4h	42	Tech,QC
44	Mate Throat Plug/HPOTP Ox Seal/Turb Sec Seal to OPF Vent System	3h	6h	41	Tech,QC
45	Perform Engineering/Safety Walkdown of Drying Setup	2h	6h	44	Safety,Engr[2]
46	V1011.01 Call to Station	1h	7h	45	Tech[3],QC,Engr[3]
47	Configure/Prep GSE Panels	1h	7h	46	Tech[3],QC,Engr[3]
48	Establish Safety Clears for SSME Pneumatics Activation	0.25h	2h	46	Tech[3],QC,Safety,Engr[3]
49	Activate SSME Pneumatics/Verify SSME Valve Positions	0.5h	3.5h	48,47	Tech[3],QC,Engr[3]
50	Apply MPS LO2 and LH2 System Blanket Pressure	1h	7h	49	Tech[3],QC,Engr[3]
51	Establish Safety Clear of Level 10/19 Platforms	0.25h	2h	50	Tech[3],QC,Safety,Engr[3]
52	Initiate HPOTP Turb Pri Seal/Ox System Drying Purge per V41CB0.080	0.75h	5.25h	51	Tech[3],QC,Engr[3]
53	HPOTP Turb Pri Seal/Ox System Drying Purge Active Monitoring	2h	6h	52	Tech,QC,Engr
54	Secure HPOTP Turb Pri Seal/Ox System Drying Purge	0.25h	1.75h	53	Tech[3],QC,Engr[3]
55	Switch Flexhose from Turbine Primary to Turbine Secondary Adapters	0.5h	3.5h	54	Tech[3],QC,Engr[3]
56	Mate Turbine Secondary Seal to OPF Vent System	0.5h	3.5h	55	Tech[3],QC,Engr[3]
57	Initiate MCC/FPB/Nozzle Drying Purge per V41CB0.080	0.75h	5.25h	56	Tech[3],QC,Engr[3]
58	MCC/FPB/Nozzle Drying Purge Active Monitoring	<b>2</b> h	6ի	57	Tech,QC,Engr
59	Secure MCC/FPB/Nozzle Drying Purge	0.25h	1.75h	58	Tech[3],QC,Engr[3]
60	Perform HPOTP Dryness Verification per V41CB0.081	2h	6h	59	Tech,QC,Engr
61	Demate Flexhoses @ Joints F6.10/F6.11/G4.3/N16 Adapters	0.5h	1h	60	Tech,QC
62	Torque Joint N14 Plate	0.25h	0.5h	61	Tech,QC
63	Remove Shims/Torque MCC Pc Transducer and D35.2/N11.2 Stack	1h	2h	62	Tech,QC
64	Tee-Connect Turb Pri to Turb Sec/Connect to Lo Press Manifold	1h	2h	63	Tech,QC
65	Perform MCC/FPB/Nozzle Dryness Verification per V41CB0.081	<b>2</b> h	6h	64	Tech,QC,Engr
66	Disassemble Test Setup/Route Filters for Bubble Point Analysis	12h	24h	65	Tech,QC
67	SSME Inspections and Checkouts in OPF/V1011.02	44h	140h	31	
68	Perform Megger GR1864 Setup	8h	8h		Tech
69	Perform E1 External Inspections (excluding Nozzle) per V41BU0.030	4h	8h	68	QC,Engr
70	Remove E1 Internal Inspection Port Hardware	4h	4h	69	Tech
71	Perform E1 Quick Look Internal Inspections	8h	16h	70	QC,Engr
72	Secure E1 Inspection Port Hardware	4h	8h	71	Tech,QC
73	Perform E2 External Inspections (excluding Nozzle) per V41BU0.030	4h	8h	68,69	QC,Engr
74	Remove E2 Internal Inspection Port Hardware	4h	4h	73	Tech
75	Perform E2 Quick Look Internal Inspections	8h	16h	74,71	QC,Engr
76	Secure E2 Inspection Port Hardware	4h	8h	75	Tech,QC
77	Perform E3 External Inspections (excluding Nozzle) per V41BU0.030	4h	8h	68,69,70	QC,Engr
78	Remove E3 Internal Inspection Port Hardware	4h	4h	77	Tech
79	Perform E3 Quick Look Internal Inspections	8h	16h	78,75	QC,Engr
80	Secure E3 Inspection Port Hardware	- 4h	8h	79	Tech,QC

Table 13. OPF rollin to SSME removal tasks (Continued).

0	Task Name	Duration	Work	Predecessors	Resource Names
1	Perform HPOTP Strain Gauge Bonding Inspections per V41AU0.090	4h	12h	68	Tech,QC,Engr
2	Perform TDT Sensors Resistance Measurements per V41BU0.250	4h	12h	81	Tech,QC,Engr
3	SSME Post-Flight Low Pressure Pump Torque Checks	18h	54h	67	·
4	Engine 1,2,3 LPFTP Torque Checks/V1011.03 Run 1	6h	18h		Tech,QC,Engr
5	Engine 1,2,3 LPOTP Torque and Travel Checks/V1011.03 Run 1	12h	36h	84	Tech,QC,Engr
8	SSME Heat Shield Removal Operations/V41-40021,22,23,24,25,26	58h	276h	67	
7	Remove DMHS Carrier Panels/V80-05907,33,35	40h	120h	23	Tech[2],QC
3	Remove DMHS Splice/Perimeter Hardware/V41-40021,22,23	4h	12h		Tech[2],QC
)	Install E1 Lower Splice Platform	0h	Oh		· · · · · · · · · · · · · · · · · · ·
)	Position Davit Crane to 19W Platform	<b>2</b> h	6h		Tech[2],QC
1	Begin Heat Shield Removal Operations	0h	0h	87,88,89,90	
2	Remove E1 Left Hand DMHS/V41-40021	1h	10h	91	Tech[6],QC,Safety,Engr[2]
3	Remove E1 Lower Splice Platform	0h	0h	92	
1	Remove E2 Left Hand DMHS/V41-40022	<b>1</b> h	10h	93	Tech[6],QC,Safety,Engr[2]
5	Remove E2 Right Hand DMHS/V41-40022	1h	10h	94	Tech[6],QC,Safety,Engr[2]
3	Remove E2 Right Hand EMHS/V41-40025	1h	10h	95	Tech[6],QC,Safety,Engr[2]
	Remove E2 Left Hand EMHS/V41-40025	1h	10h	96	Tech[6],QC,Safety,Engr[2]
3	Reposition Davit Crane to 19E Platform	2h	6h	97	Tech[2],QC
	Remove E3 Right Hand DMHS/V41-40023	1h	10h	98	Tech[6],QC,Safety,Engr[2]
	Remove E3 Left Hand DMHS/V41-40023	1h	10h	99	Tech[6],QC,Safety,Engr[2]
	Remove E3 Left Hand EMHS/V41-40026	1h	10h	100	Tech[6],QC,Safety,Engr[2]
	Remove E3 Right Hand EMHS/V41-40026	1h	10h	101	Tech[6],QC,Safety,Engr[2]
	Install E2/E3 Lower Splice Platform	Oh	0h	102	
	Remove E1 Right Hand DMHS/V41-40021	1h	10h	103	Tech[6],QC,Safety,Engr[2]
	Remove E1 Right Hand EMHSV41-40024	1h	10h	104	Tech[6],QC,Safety,Engr[2]
	Reposition Davit Crane to 19W Platform	2h	6h	105	Tech[2],QC
	Remove E1 Left Hand EMHS/V41-40024	1h	10h	106	Tech[6],QC,Safety,Engr[2]
	Remove E2/E3 Lower Splice Platform	Oh	0h	107	
	Stow Davit Crane	2h	6h	108	Tech[2],QC
	SSME Removal Operations	64h	520h	109,86	· · · · · · · · · · · · · · · · · · ·
	Engine Removal Preps	12h	129h		· · · · · · · · · · · · · · · · · · ·
	Demate SSME Hydraulic QD's/Y9002.06	7h	29h	86	
	Perform Orbiter Hydraulic System Venting	. 4h	20h		Tech,Safety,Engr[3]
	Demate E1 Hydraulic Return QD @ Joint H17	0.25h	0.75h	113	Tech,QC,Engr
	Perform E1 Hydraulic Return QD Demate Inspection per V58AG0.123-D	0.25h	0.75h	114	Tech,QC,Engr
	Demate E1 Hydraulic Supply QD @ Joint H1	0.25h	0.75h	115	Tech,QC,Engr
	Perform E1 Hydraulic Supply QD Demate Inspection per V58AG0.123-A	0.25h	0.75h	116	Tech,QC,Engr
	Demate E2 Hydraulic Return QD @ Joint H17	0.25h	0.75h	117	Tech,QC,Engr
	Perform E2 Hydraulic Return QD Demate Inspection per V58AG0.123-E	0.25h	0.75h	118	Tech,QC,Engr
	Demate E2 Hydraulic Supply QD @ Joint H1	0.25h	0.75h	119	Tech,QC,Engr

Table 13. OPF rollin to SSME removal tasks (Continued).

ID	Task Name	Duration	Work	Predecessors	Resource Names
121	Perform E2 Hydraulic Supply QD Demate Inspection per V58AG0.123-B	0.25h	0.75h	120	Tech,QC,Engr
122	Demate E3 Hydraulic Return QD @ Joint H17	0.25h	0.75h	121	Tech,QC,Engr
123	Perform E3 Hydraulic Return QD Demate Inspection per V58AG0.123-F	0.25h	0.75h	122	Tech,QC,Engr
124	Demate E3 Hydraulic Supply QD @ Joint H1	0.25h	0.75h	123	Tech,QC,Engr
125	Perform E3 Hydraulic Supply QD Demate Inspection per V58AG0.123-C	0.25h	0.75h	124	Tech,QC,Engr
126	Orbiter Interface Hardware Verification (Aft)	4h	8h		Tech,QC
127	LH2 Foam Removal (Aft)	8h	16h		Tech,QC
128	Terminate Aft Compartment ECS Purge Air per V3555	0h	0h		1
129	PVD Controller Duct Removal (Aft)	6h	18h	128	Tech[2],QC
130	Reinitiate Aft Compartment ECS Purge Air per V3555	0h	: Oh	129	
131	Calibrate Force Gages (Roc)	8h	16h		Tech,QC
132	Orbiter Preps (Roc)	4h	8h		Tech,QC
133	Electrical Interface Demates (Aft)	4h	8h		Tech,QC
134	Engine Preps (Roc)	4h	8h		Tech,QC
135	Orbiter Helium Handvalve Installation (Aft)	2h	4h	133	Tech,QC
136	Terminate Aft Compartment ECS Purge Air per V3555	0h	0h	135	
137	Demate Fluid System Interfaces (Roc)	<b>2</b> h	8h	136,131,127	Tech[3],QC
138	Reinitiate Aft Compartment ECS Purge Air per V3555	0h	0h	137	
139	Install Interface Support Panel (Roc)	2h	6h	138	Tech[2],QC
140	Engine 2 Removal GSE Handling Operations (Roc)/V5087	8h	36h	111	1
141	Verify Lift Truck, Carrier and Rail Table Proofload Validations	0.5h	1h		Tech,QC
142	Install Lift Spoon	0.5h	1h	141	Tech,QC
143	Mount Rail Table on Lift Truck	1h	. 4h	142	Tech[2],QC,Engr
144	Mount Carrier on Rail Table/Lift Truck	<b>2</b> h	8h	143	Tech[2],QC,Engr
145	Perform Dummy Load Brake Test without Engine	3h	21h	144	Tech[4],QC,Safety,Engr
145	Transport Lift Truck/Hyster to OPF for Engine 2 Removal	1h	1h	145	Engr
147	Engine 2 Removal Operations	8h	75h	140	· · · · · · · · · · · · · · · · · · ·
148	Position Installer for Engine 2 Removal	2h	10h	111	Tech[2],QC,Engr[2]
149	Mate Installer to Engine 2	2h	30h	148	Tech[7],QC[2],Safety[2],Engr[4]
150	Terminate Aft Compartment ECS Purge Air per V3555	0h	: <b>0</b> h	149	
151	Demate Engine from Orbiter	2h	30h	150	Tech[7],QC[2],Safety[2],Engr[4]
152	Reinitiate Aft Compartment ECS Purge Air per V3555	0h	Oh	151	· · · · · · · · · · · · · · · · · · ·
153	Transport Engine 2 to VAB	: 1h	1h	152	Engr
154	Install Orbiter Engine 2 Interface Covers	<sub>:</sub> 2h	4h	151	Tech,QC
155	Rotate Engine 2 to Horizontal Handler/V5087	2h	14h	153	
156	Install Rotating Sling and Unload Carrier/Engine	0.5h	3.5h		Tech(4),QC,Safety,Engr
157	Mount Carrier on Skid	0.5h	3.5h	156	Tech[4],QC,Safety,Engr
158	Transfer Engine 2 to Horizontal Handler	1h	7h	157	Tech[4],QC,Safety,Engr
159	Engine 3 Removal GSE Handling Operations (Roc)/V5087	6h	30h	158	. ,
160	Mount Carrier on Rail Table/Lift Truck	2h	8h		Tech[2],QC,Engr

Table 13. OPF rollin to SSME removal tasks (Continued).

ID	Task Name	Duration	Work	Predecessors	Resource Names
161	Perform Dummy Load Brake Test without Engine	3h	21h	160	Tech[4],QC,Safety,Engr
162	Transport Hyster to OPF for Engine 3 Removal	1h	1h	161	Engr
163	Engine 3 Removal Operations	8h	75h	147	
164	Position Installer for Engine 3 Removal	2h	10h	162	Tech[2],QC,Engr[2]
165	Mate Installer to Engine 3	2h	30h	164	Tech[7],QC[2],Safety[2],Engr[4]
166	Terminate Aft Compartment ECS Purge Air per V3555	Oh	Oh	165	
167	Demate Engine from Orbiter	<b>2</b> h	30h	166	Tech[7],QC[2],Safety[2],Engr[4]
168	Reinitiate Aft Compartment ECS Purge Air per V3555	0h	Oh	167	
169	Transport Engine 3 to VAB	1h	1h	168	Engr
170	Install Engine 3 Interface Covers	<b>2</b> h	4h	167	Tech,QC
171	Rotate Engine 3 to Horizontal Handler/V5087	2h	14h	169	
172	Install Rotating Sling and Unload Carrier/Engine	0.5h	3.5h		Tech[4],QC,Safety,Engr
173	Mount Carrier on Skid	0.5h	3.5h	172	Tech[4],QC,Safety,Engr
174	Transfer Engine 3 to Horizontal Handler	1h	7h	173	Tech[4],QC,Safety,Engr
175	Engine 1 Removal GSE Handling Operations (Roc)/V5087	6h	30h	174	
176	Mount Carrier on Rail Table/Lift Truck	2h	8h		Tech[2],QC,Engr
177	Perform Dummy Load Brake Test without Engine	3h	21h	176	Tech[4],QC,Safety,Engr
178	Transport Hyster to OPF for Engine 1 Removal	1h	1h	177	Engr
179	Engine 1 Removal Operations	8h	75h		
180	Position Installer for Engine 1 Removal	2h	10h	178	Tech[2],QC,Engr[2]
181	Mate Installer to Engine 1	2h	30h	180	Tech[7],QC[2],Safety[2],Engr[4]
182	Terminate Aft Compartment ECS Purge Air per V3555	Oh	Oh	181	(oon() ], ao[2], oanoty[2], Engi[4]
183	Demate Engine from Orbiter	2h	30h	182	Tech[7],QC[2],Safety[2],Engr[4]
184	Reinitiate Aft Compartment ECS Purge Air per V3555	Oh .	0h	183	Toom(1), wo(2), our oty(2), engr[4]
185	Transport Engine 1 to VAB	1h	1h	184	Engr
186	Install Engine 1 Interface Covers	2h	4h	183	Tech,QC
187	Rotate Engine 1 to Horizontal Handler/V5087	6h	30h	185	Teon, QO
188	Install Rotating Sling and Unload Carrier/Engine	0.5h	3.5h		Tech[4],QC,Safety,Engr
189	Mount Carrier on Skid	0.5h	3.5h	188	Tech[4],QC,Safety,Engr
190	Transfer Engine 1 to Horizontal Handler	1h	7h	189	Tech[4],QC,Safety,Engr
191	Stow SSME Handling GSE/V5087	4h	16h	190	Tech[2],QC,Engr
192	Post-Engine Removal Operations	6h	12h	179	recit[2],QU,Etigt
193	Interface Hardware Inspections	4h	8h	186	Tech.QC
194	Gimbal Bolt/Nut Torque Cycle	2h	4h	186,193	Z
195	SSME Removal Operations Complete/OK to Proceed with MPS Operations	: 211 Oh	0h	193,194	Tech,QC

Table 14. Engine shop turnaround tasks.\*

ID	Task Name	Duration	Work	Predecessors
1	Engine Shop Turnaround!	252.75h	1330h	
2	Nozzle Tube Leak Checks/V1294.005!	<b>3</b> h	6.5h	k - gran
3	SSME Inspections in Engine Shop (continued)/V1011.02!	252.75h	135.75h	
4	Vertical Stand Available	Oh	Oh	V v v v v v v v v v v v v v v v v v v v
5	Transfer Engine to Vertical Stand/V5087!	3h	32.5h	4
6	HPOTP Post-Flight Torque Check/V1011.03 Run 1!	3.75h	11.25h	5
7	HPFTP Post-Flight Torque Check/V1011.03 Run 1!	3.5h	10.5h	6
8	HEX Coil Post-Flight Leak Check/V1294.003!	8h	9h	7
9	MCC Liner Cavity Decay Check/V1294.003!	3.25h	8.25h	8
10	HPOTP Removal and Replacement/V5E02!	97.75h	<b>43</b> 5h	6,8,9
11	HPFTP Removal and Replacement/V5E06!	101.25h	375.75h	7,8,9
12	Fuel and Hot Gas System Internal and External Leak Checks/V1294.005!	8.75h	21.25h	11
13	LOX System Internal and External Leak Checks/V1294.006!	8.5h	20.25h	12
14	SSME Flight Readiness Test and Checkout/V1294.002!	50.25h	124h	13
15	GOX System Internal and External Leak Checks/V1294.002!	2.75h	12h	14
16	Rotate Engine to Horizontal Handler/V5087!	4.25h	38.5h	15
17	Fuel and LOX Ball Seal Leak Checks/V1294.007!	3.5h	7.5h	16
18	Move Engine to VAB Transfer Aisle!	0h	0h	17
19	Engine Encapsulation Leak Check/V1294.007!	23.5h	68.5h	18
20	Move Engine to Engine Shop!	0h	0h	19
21	LPFTP Torque Check!	1.25h	3.75h	20
22	LPOTP Torque and Shaft Travel!	3.25h	9.75h	21

<sup>\*</sup> Lowest level of detail not shown but available for all subtasks. See table 17 for examples.

Table 15. Engine installation to OPF rollout tasks.

ID	Task Name	Duration	Work	Predecessors	Resource Names
1	Engine Installation to OPF Roll-Outi	40.09d	2207h		
2	Engine Installation Operations/V50051	11.5d	733.5h		
3	Engine Installation Preps!	3d	241h	TY TOTAL STREET, STREE	;
4	Installation Preps in OPF!	3d	93h		
5	Remove/Inspect Orbiter Interface Covers (Aft)!	24h	0h		······································
6	Terminate Aft Compartment ECS Purge Air per V3555	0h	0h		
7	Remove PVD Controller Duct	<b>2</b> h	4h	6	Tech.QC
8	Photograph Fluid Interface Panels per V41DC0.030	1h	2h	7	QC,Engr
9	Remove Test Plate/Inspect Orbiter LO2 Feedlines per V41BU0.360	4h	12h	8	Tech,QC,Engr
10	Remove Test Plate/Inspect Orbiter LH2 Feedlines per V41BU0.360	4h	12h	9	Tech,QC,Engr
11	Inspect SSME Controller Purge Line	1h	2h	10	Tech,QC
12	Reinitiate Aft Compartment ECS Purge Air per V3555	0h	Oh	11	
13	Remove Test Plate/Inspect Orbiter LO2/LH2 Bleed Lines	4h	8h	12	Tech,QC
14	Remove Test Plate/Inspect Orbiter LO2/LH2 Pressurization Lines	4h	<b>8</b> h	13	Tech,QC
15	Remove Test Plate/Inspect Orbiter GHe/GN2 Supply Lines	4h	8h	14	Tech,QC
16	Perform MPS Test Requirements (Aft)	4h	8h		QC,Engr
17	Perform Engine Interface Flange Leak Check Port Verification (Aft)	4h	8h		Tech,QC
18	Perform Orbiter Preps for SSME Installation (Roc)!	0.5d	21h	<u></u>	
19	Verify Body Flap Full Down	Oh	Oh		
20	Perform Gimbal Interface Nut/Bott Verification	1h	1h		QC
21	install Stifarm Brackets and TVC Actuator Supports per V5057	4h	12h		Tech(2),QC
22	Perform Pre-Installation Inspection of Joint 01/F1 Interface Seals	4h	8h		Tech.QC
23	Installation Preps in Engine Shop1	1.5d	148h	<u> </u>	rodi, ao
24	Install AFV/Helium Baggie Purge Adapters	4h	8h		Tech,QC
25	Install Liquid Air Insulators	12h	24h		Tech.QC
26	Perform SSME Engineering Walkdowns	12h	108h		lech[3],QC[3],Engr[3]
27	Remove/Inspect Engine Interface Covers	4h	8h		Tech,QC
28	Engine 1 Installation GSE Handling Operations/V5087!	0.63d	34.5h	5	Tuoniao
29	Verify Lift Truck, Carrier and Rail Table Proofload Validations	0.25h	0.5h		Tech,QC
30	Transfer Engine to Carrier from Horizontal Handler	1.5h	6h	29	Tech[2],QC,Engr
31	Establish Safety Clears for Engine Lifting Operations	0.25h	3h	30	Tech[7],QC,Safety,Engr[3]
32	Mount Carrier/Engine on Rail Table/Lift Truck	2h	24h	31	Tech[7],QC,Safety,Engr[3]
33	Transport Hyster to VAB for Engine 1 Installation	1h	1h	32	Engr
34	Engine 1 Installation Operations!	0.88d	79h	28	Eligi
35	Position Hyster/Installer for Engine 1 Installation	2h	26h	20	Toob[7] OC[0] Cafab. Faca[0]
36	Terminate Aft Compartment ECS Purge Air per V3555	Öh	2011 Oh	35	Tech[7],QC[2],Safety,Engr[3]
37	Engine 1 Mate to Orbiter	4h	52h	36	Tash [7] OC(0) C-4-4 (Fa10)
38	Reinitiate Aft Compartment ECS Purge Air per V3555	0h	0h		Tech[7],QC[2],Safety,Engr[3]
39	Transport Hyster to VAB		=:-	37	
40	Engine 3 installation GSE Handling Preps/V5087!	1h	1h	38	Engr
41	Verify Lift Truck, Carrier and Rail Table Proofload Validations	0.63d	34.5h	39	
42		0.25h	0.5h		Tech,QC
43	Transfer Engine to Carrier from Horizontal Handler	1.5h	6h	41	Tech[2],QC,Engr
	Establish Safety Clears for Engine Lifting Operations	0.25h	3h	42	Tech[7],QC,Safety,Engr[3]
44	Mount Carrier/Engine on Rail Table/Lift Truck	2h	24h	43	Tech[7],QC,Safety,Engr[3]
45	Transport Hyster to OPF for Engine 3 Installation	1h	1h	44	Engr

Table 15. Engine installation to OPF rollout tasks (Continued).

ID	Task Name	Duration	Work	Predecessors	Resource Names
46	Engine 3 Installation Operations!	0.88d	79h	34	
47	Position Hyster/Installer for Engine 3 Installation	2h	26h	40	Tech[7],QC[2],Safety,Engr[3]
48	Terminate Aft Compartment ECS Purge Air per V3555	0h	Oh	47	
49	Engine 3 Mate to Orbiter	4h	52h	48	Tech[7],QC[2],Safety,Engr[3]
50	Reinitiate Aft Compartment ECS Purge Air per V3555	0h	0h	49	
51	Transport Hyster to VAB for Engine 2 Installation	1h	1h	49	Engr
52	Engine 2 Installation GSE Handling Preps/V5087!	0.63d	34.5h	51	***************************************
53	Verify Lift Truck, Carrier and Rail Table Proofload Validations	0.25h	0.5h		Tech,QC
54	Transfer Engine to Carrier from Horizontal Handler	1.5h	6h	53	Tech[2],QC,Engr
55	Establish Safety Clears for Engine Lifting Operations	0.25h	3h	54	Tech[7],QC,Safety,Engr[3]
56	Mount Carrier/Engine on Rail Table/Lift Truck	2h	24h	55	Tech[7],QC,Safety,Engr[3]
57	Transport Hyster to OPF for Engine 2 Installation	1h	1h	56	Engr
58	Engine 2 Installation Operations!	9.88d	79h	52	······································
59	Position Hyster/Installer for Engine 2 Installation	2h	26h		Tech[7],QC[2],Safety,Engr[3]
60	Terminate Aft Compartment ECS Purge Air per V3555	Oh	Oh	59	
61	Engine 2 Mate to Orbiter	4h	52h	60	Tech[7],QC[2],Safety,Engr[3]
62	Reinitiate Aft Compartment ECS Purge Air per V3555	Oh	0h	61	
63 .	Transport Hyster to VAB	1h	1h	62	Engr
64	Aft Swings Closed	Oh	Oh	63	
65	SSME 1,2,3 Interface Securing Operations!	4d	152h	84	
66	Interface Hardware Installation/GSE Removal	32h	96h		Tech[2],QC
67	Controller Coolant Duct Installation	8h	16h	64	Tech,QC
68	Electrical Interface Connection	16h	32h	64	Tech,QC
69	Mate Hydraulic QD's per V58AG0.121/V9002.06	4h	8h	64	Tech.QC
70	SSME Interface Securing Complete	Oh	Oh	66	
71	SSME/MPS integrated Testing!	11.28d	246.5h	70	
72	Low Pressure Pump Post-Installation Torque Checks/V1011.03 Run 3	2.25d	54h	600 V (	
73	Engine 1,2,3 LPFTP Torque Checks	6h	18h		Tech,QC,Engr
74	Engine 1,2,3 LPOTP Torque Checks	12h	36h	70,73	Tech,QC,Engr
75	Orbiter/SSME Interface Verification!	9.03d	192.5h		
76	GSE Configuration for Leak Checks/V1011.04	: 4h	4h	74	Tech
77	Fuel Interface Leak Check/V1011.051	0.44d	11h	76	
78	Install Throat Plugs	2h	2h		Tech
79	Activate MPS 750 psi Pneumatics	0.25h	1.5h	78	Tech[2],QC[2],Engr[2]
80	Pressurize MPS LH2 Manifold	0.25h	1.5h	79	Tech[2],QC[2],Engr[2]
81	Perform Fuel Feed Joint F1 I/F Leak Checks per V41AX0.020/.030/.040	0.5h	3h	80	Tech[2],QC[2],Engr[2]
82	Perform Fuel Bleed Joint F4.3 I/F Leak Checks per V41AX0.020/.030/.040	0.5h	3h	81	Tech[2],QC[2],Engr[2]
83	LH2 Manifold Decay Test/V1009.051	1d	Oh	77	
84	Perform LH2 Manifold Decay Test per V41	8h	Oh		
85	Vent Fuel System Manifold	0.25h	Oh		
86	Secure MPS 750 psi Pneumatics	0.25h	Oh	82	
87	SSME Electrical Interface Verification/V9001VL4	8h	16h	86	QC,Engr
88	GOX System interface Leak Check/V1011.041	1d	33.5h	87	GO,ENY
89	Mate Pneumatic Flexhoses/Leak Check Setup	2h	6h	υ,	Toob!O! OO
90	Close LO2 Prevalves and Pressurize GO2 Pressurization System		3h	90	Tech[2],QC
3TU	CIUSE LOZ FIEVAIVES AND FIESSUNZE GOZ PIESSUNZAUCH SYSTEM	0.5h	. <b>3</b> П	89	Tech[2],QC[2],Engr[2]

Table 15. Engine installation to OPF rollout tasks (Continued).

ID	Task Name	Duration	Work	Predecessors	Resource Names
91	Power Up SSME Controllers per V9001VL4	0.5h	3.5h	90	Tech[2],QC[2],Engr[3]
92	Perform AFV Crack/Full Open Test per V41BR0.030	0.5h	3.5h	91	Tech[2],QC[2],Engr[3]
93	Power Down SSME Controllers per V9001VL4	0.5h	3.5h	92	Tech[2],QC[2],Engr[3]
84	Perform G02/GCV Ext Leak Check and Orifice Verif. per V41BP0.010	0.5h	3h	93	Tech[2],QC[2],Engr[2]
95	Perform GO2 I/F Temperature Xducer Leak Check per V41AY0.320	0.5h	3h	94	Tech[2],QC[2],Engr[2]
96	Perform GO2 I/F Flange Leak Check per V41AX0.050	0.5h	3h	95	Tech[2],QC[2],Engr[2]
97	Perform Combined AFV Seat/Shaft Seal Flow Test per V41BQ0.100	0.5h	3h	96	Tech[2],QC[2],Engr[2]
98	Disassemble Test Setup	2h	2h	97	Tech
99	Install Joint 018.1 Flight Plates/V1011.04!	2h	5h	88	
100	Install AFV Filter/Seal per V41BU0.220	1h	3h		Tech,QC,Engr
101	Secure Joint 018.1's	1h	2h	100	Tech,QC
102	LOX Interface Leak Check/V1011.051	7h	32h	99	
103	Configure SSME Drain Lines	1h	1h		Tech
104	Perform MPS 750 psi Pneumatic System Activation	0.5h	3h	103	Tech[2],QC[2],Engr[2]
105	Perform LO2 Manifold Pressurization	0.5h	3h	104	Tech[2],QC[2],Engr[2]
106	Perform LO2 Feed Joint 01 I/F Leak Checks per V41AX0.020/.030/.040	1h	6h	105	Tech[2],QC[2],Engr[2]
107	Perform LO2 Bleed Joint 015 I/F Leak Checks per V41AX0.020/.030/.040	1h	6h	106	Tech[2],QC[2],Engr[2]
108	Perform LO2 System Interface Mass Spec Leak Checks	1h	6h	107	Tech[2],QC[2],Engr[2]
109	Perform Joint 018.1 External Leak Check	0.5h	3h	108	Tech[2],QC[2],Engr[2]
110	Vent LO2 Feed and MPS 750 psi Systems	0.5h	3h	109	Tech[2],QC[2],Engr[2]
111	Secure LO2 Leak Check Setup	1h	1h	110	Tech
112	GSE Configuration for Hot Gas Leak Checks/V1011.05	2h	2h	102	Tech
113	Install Throat Plugs/V1011.05	2h	4h	112	Tech,QC
114	Hot Gas System Interface Leak Checks/V1011.051	6h	22.5h	113	
15	Configure SSME Drain Lines	0.5h	0.5h		Tech
116	Configure GH2 Pressurization System for Flow Test	0.5h	0.5h		Tech
117	Perform GH2 Pressurization System Flow Test per V41BZ0.080	0.5h	1.5h	116	Tech,QC,Engr
118	Perform GH2 I/F Pressure Xducer Leak Check per V41AY0.350	1 h	6h	117	Tech[2],QC[2],Engr[2]
119	Perform GH2 Press Joint F9.3 I/F Leak Check per V41AX0.020/.030/.040	1h	6h	118	Tech[2],QC[2],Engr[2]
120	Perform GH2 System Interface Mass Spec Leak Checks	0.5h	3h	119	Tech[2],QC[2],Engr[2]
121	Vent Hot Gas System	0.5h	3h	120	Tech[2],QC[2],Engr[2]
122	Perform PD16 Hardware Installation	1h	1h	121	Tech
123	Secure Hot Gas Leak Check Setup	1h	1h	122	Tech
24	Throat Plug Removal/V1011.05	2h	2h	114	Tech
25	Pneumatic System Interface Leak Checks/V1011,05	3.5h	12.5h	124	16611
26	Configure SSME Drain Lines	0.5h	0.5h		Tech
27	Perform SSME 750 psi Pneumatic System Activation	1h	5h	126	Tech,QC[2],Engr[2]
28	Perform Pneumatic I/F Joint P1 Leak Check per V41AX0.020/.030/.040	1h	5h	127	Tech,QC[2],Engr[2]
129	Secure SSME 750 psi Pneumatic System	1h	2h	128	QC,Engr
30	Fuel System Interface Insulation Installation/V1011.05	24h	48h	125	Tech,QC
131	SSME Engine and Dome Mounted Heat Shield Installation Operations!	126h	1056h	125	recii, go
132	Position Davit Crane on 19R/G41-20017	2h	12h	120	Tech[4],QC[2]
33	Install E-1 R/H EMHS/V41-50024	2h	12h		
134	Install E-3 L/H EMHS/V41-50026	2h	12h	133	Tech[4],QC[2]
				134	Tech[4],QC[2]
135	Install E-3 R/H EMHS/V41-50026	2h	12h		Tech[4],QC[2]

Table 15. Engine installation to OPF rollout tasks (Continued).

ID	Task Name	Duration	Work	Predecessors	Resource Names
137	Install E-3 R/H DMHS/V41-50023	2h	12h	136	Tech[4],QC[2]
138	Install E-3 L/H DMHS/V41-50023	2h	12h	137	Tech[4],QC[2]
139	Position Davit Crane on 19L/G41-20017	1h	6h	138	Tech[4],QC[2]
140	Install E-1 L/H EMHS/V41-50024	2h	12h	139	Tech[4],QC[2]
141	Install E-2 L/H EMHS/V41-50025	2h	12h	140	Tech[4],QC[2]
142	Install E-2 R/H EMHS/V41-50025	2h	12h	141	Tech[4],QC[2]
143	Verify E-1 EMHS Splice Line Hardware Torque Complete/Verify Bolt Protrusion Complete	Oh	Oh	142	Tech[4],QC[2]
144	Verify E-2 EMHS Splice Line Hardware Torque Complete/Verify Bolt Protrusion Complete	0h	0h	143	Tech[4],QC[2]
145	Install E-1 L/H DMHS/V41-50021	2h	12h	144	Tech[4],QC[2]
146	Instail E-2 R/H DMHS/V41-50022	2h	12h	145	Tech[4],QC[2]
147	Install E-2 L/H DMHS/V41-50022	2h	12h	146	Tech[4],QC[2]
148	Position Davit Crane on 19R/G41-20017	1h	6h	147	Tech[4],QC[2]
149	Install E-1 R/H DMHS/V41-50021	2h	12h	148	Tech[4],QC[2]
150	Lower Davit Crane from Level 19/G41-20017	2h	12h	149	Tech[4],QC[2]
151	Heat Shield Securing/Splice Line Configuration/V41-5002x	48h	288h	150	Tech[4],QC[2]
152	Install Carrier Panels/V80-95907,33,35	98h	588h	150	Tech[4],QC[2]
153	SSME Gimbal Clearance Checksl	17.5h	123h		
154	Pin TVC Actuators/V1063/V5057	4h	12h	152	Tech[2],QC
155	Install Marking Tape on SSME Nozzle Tubes	<b>2</b> h	2h	154	Tech
156	Perform SSME Heat Shield Verification	1h	1h	155	Tech
157	Hydraulic System Power-Up/V1063/V9002.01	2h	20h	156	Tech[3],QC[3],Engr[4]
158	MPS TVC Full Excursion Gimbal Clearance Checks/V1063	4.5h	45h	157	Tech[3],QC[3],Engr[4]
159	SSME TVC Toe-In Clearance Checks/V1063	1.5h	15h	158	Tech[3],QC[3],Engr[4]
160	SSME TVC Actuator Drift Test/V1063	1.5h	15h	159	Tech[3],QC[3],Engr[4]
161	Orbiter Hydraulic Power-Down/V1063/V9002.01	1h	10h	160,162	Tech[3],QC[3],Engr[4]
162	Hydraulic QD Leak Checks per V41AX0.020/.030/.040/V9002.06	1h	3h	157	Tech,QC,Engr
163	SSME OPF Roll-Out Inspections/V41-20003!	19h	48h	153	
164	Perform SSME Valve Position Verification	2h	10h		Tech,QC,Safety,Engr[2]
165	TVC Actuator Midstroke Lock Installation/V5057	4h	12h	164,162	Tech[2],QC
166	Thrust Chamber Cover Installation/V5057	2h	4h	165	Tech,QC
167	Verify Thrust Chamber Covers Installed per V41BW0.031	0.25h	0.5h	166	Tech,QC
168	Verify Bellows Covers Installed per V41BW0.031	0.25h	0.5h	167	Tech,QC
169	Verify TVC Actuators Connected per V41BW0.031	0.25h	0.5h	168	Tech,QC
170	Verify Midstroke Locks Installed per V41BW0.031	0.25h	0.5h	169	Tech,QC
171	Install Miscellaneous Covers per V5057	2h	4h	170	Tech,QC
172	Visually Inspect Engine Components for Damage	8h	16h	171	Tech,QC
173	Aft Closeout for OPF Roll-Out Complete	Oh	Oh	163	
174	Orbiter Roll-Out to VAB	Oh	Oh	173	

Table 16. VAB rollin to launch tasks.

ID	Task Name	Duration	Work	Predecessors	Resource Names
1	VAB Roll-in to Launchi	484.87h	592.35h	·!	
2	Orbiter/ET Mate Operations/\$0004!	144h	Oh		
3	Orbiter in Transfer Aisle	0h	0h		
4	Connect Sling/Preps for Orbiter Lift	8h	Oh	3	
5	Rotate Orbiter to Vertical/Disconnect Aft Sling	8h	0h	4	
6	Orbiter/ET Softmate	8h	Oh	5	
7	Orbiter/ET Hardmate	<b>4</b> h .	0h	6	
8	Sling Removal	4h	0h	7	
8	TSM Connect	16h	0h	8	
10	Umbilical Mate	16h	Oh	8	·
11	Monoball Connect/Closeout	24h	<b>0</b> h	9	·
12	Hazardous Gas Leak Checks	8h	<b>O</b> h	9	· 
13	Ultrasonic Inspections	4h	0h	10	
14	TSM Static Measurement	8h	<b>O</b> h	9	
15	External Umbilical Can Closeout	8h	<b>O</b> h	12,14	
16	Ready for Orbiter Power-Up	Oh	Oh	15	
17	Umbilical Foaming	40h	0h	15	
18	Purge Curtain Installation	40h	Oh	17	
19	Shuttle Interface Testing/80008!	38h	Oh		
20	Shuttle Interface Testing Preps	18h	0h		
21	Orbiter Power-Up	Oh	Oh	20	
22	Orbiter System Checks	8h	0h	21	
23	S0008 Testing	4h	0h	20	· /************************************
24	ET/SRB Power-Up	Oh	0h	23	· 
25	ET/SRB System Checks	8h	Oh	24	
26	SRB TVC Actuator Testing	4h	0h	25	
27	Connect SRB TVC Actuators	4h	0h	26	
28	Umbilical Interface Leak Checks/V1149!	30h	33.75h	20	
29	Umbilical Interface Leak Check Preps!	12h	2h	1	
30	Perform GN2 Flowmeter Setup	4h	0h	<u>}</u>	
31	Perform LO2/LH2 TSM Line Verification	4h	Oh		
32	Perform SSME Trickle Purge Activation	1.5h	2h	31	, , , , , , , , , , , , , , , , , , , ,
33	Verify PD14 GN2 Purge T-0 Disconnect Mated	0h	0h	·	
34	Perform Thrust Chamber Cover Removal/V5057	1h	1h		Tech
35	Activate/Verify SSME Trickle Purge per S00000.100	0.5h	1h	34	Tech,QC
36	Perform TP8 Configuration	4h	Oh	31	1 5011,440
37	Perform PD4/PD5 HUMS Leak Check Preps	8h	Oh	31	
38	Perform Mass Spec Leak Check Preps	8h	Oh	31	
39	Perform Mass Spec Leak Check Machine Preps	2h	Oh	31	
40	Umbilical Interface Leak Check Operations!	18h	31.75h	29	

Table 16. VAB rollin to launch tasks (Continued).

D	Task Name	Duration	Work	Predecessors	Resource Names
11	Orbiter MPS Helium Fill QD Leak Check	2h	0h		
2	17 Inch Disconnect Timing Checks/200 psi Leak Checks	8h	0h	41	
13	MPS LOX Fill and Drain QD Leak Check	4h	0h	42	
14	MPS LH2 Fill and Drain QD Leak Check	4h	0h	43	# W. W. W. W. W. W. W. W. W. W. W. W. W.
15	SSME GN2 Heater Checkout/GN2 Leak Checks!	4h	25.75h	,	
16	Configure Heater Power Circuit Breakers	0.25h	1h		Tech,QC,Engr[2]
7	Verify Panel Valve Configuration	0.25h	1h	46	Tech,QC,Engr[2]
8	Perform Automated GN2 Panel Valve Checkout	0.5h	2h	47	QC,Engr[2],Tech
.9	Close TSM GN2 Supply Valve	0.25h	1.25h	48	Tech[2],QC,Engr[2]
iO	Pressurize GN2 Panel	0.25h	1h	49	Tech,QC,Engr[2]
i1	Establish Safety Clears	0.25h	2h	50	Tech[2],QC[3],Safety,Engr[2]
52	Open TSM GN2 Supply Valve	0.25h	2h	51	Tech[2],QC[3],Engr[2],Safety
<b>i</b> 3	Verify No Leakage ❷ PD14 GN2 Purge Interface per S00000.020	0.25h	2h	52	Tech[2],QC[3],Engr[2],Safety
54	Perform Bubble Soap Leak Check of TSM GN2 Lines	0.25h	<b>2</b> h	53	Tech[2],QC[3],Engr[2],Safety
i5	Perform Orbiter GN2 Joint Leak Check	0.25h	2h	54	Tech[2],QC[3],Engr[2],Safety
56	Perform SSME GN2 Joint Leak Check	0.25h	2h	55	Tech[2],QC[3],Engr[2],Safety
i7	Perform GN2 I/F Joint N1 Leak Check per V41AX0.020/.030/.040	0.25h	2h	56	Tech[2],QC[3],Engr[2],Safety
8	Perform SSME GN2 Heater Checkout	0.5h	4h	57	Tech[2],QC[3],Engr[2],Safety
i9	Secure GN2 Flow	0.25h	1.5h	58	Tech[2],QC[2],Engr[2]
iO	SSME MFV Heater T-0 Interface Verification!	2h	6h	59	
51	Power Up Distributor Panels	0.25h	0.75h		QC,Engr[2]
2	Close Panel Circuit Breakers	0.25h	0.75h	61	Tech,QC,Engr
33	Perform MFV Heater Checkout per S00000.101	1h	3h	62	Tech,QC,Engr
34	Open Panel Circuit Breakers	0.25h	0.75h	63	Tech,QC,Engr
35	Power Down Distributor Panels	0.25h	0.75h	64	QC,Engr[2]
56	VAB Roll-Out Operations/A5214!	44h	Oh		
37	Roll-Out Preps	24h	Oh	2	
8	Shuttle Transfer to Launch Pad	12h	0h	67	
9	Crawler Transport Operations	8h	0h	68	
10	Launch Pad Validation Preps/S0009 POSU's	12h	Oh	67	: :
71	Shuttle 1st Motion to Pad	Oh	0h	68	
12	MLP Harddown at Pad1	Oh	0h	71,69	
73	Launch Pad Validation/80009!	44h	12h	72	
74	Perform PD15/PD16 Connect	44h	0h		
75	Perform A2202 Firex Verification	8h	Óh	1 - 1 - 2 - 2 - 1 - 1 - 1 - 1 - 1 - 1 -	
76	Activate Pad Helium Supply Panel	8h	<b>O</b> h		
77	Activate SSME Trickle Purge	4h	12h		Tech,QC,Engr
78	Activate T-0 Trickle Purge	8h	<b>O</b> h		
79	Perform LDB Safing Panel Verification	8h	0h		
30	Perform Propellant System Switch Validation	8h	0h	.,	

Table 16. VAB rollin to launch tasks (Continued).

ID	Task Name	Duration	Work	Predecessors	Resource Names
81	Perform Recirc Pump Switch Validation	8h	Oh	<u></u>	
82	Perform ET OI Power Up	8h	Oh -		
83	Perform ET OI Instrumentation Checks	<b>8</b> h	Oh		· · · · · · · · · · · · · · · · · · ·
84	Perform ET Level Sensor Cals	8h	0h		
85	Perform Valve Verifications for G2340 LO2/LH2 Checkouts	8h	Oh		
86	Perform ET OI Power Down	8h	Öh .	and the second of the second o	
87	Extend RSS	Oh	Oh	73	
88	Engine Flight Readiness Testing/V1046.001!	21h	52h		
89	Preps for 88ME Hydraulic Operations/V9002.06	7h	15h		
90	SSME Engineering Determine Configuration Required Configuration for Hydraulics	1h	1h		Engr
91	Perform TVC Actuator Preps for Hydraulic Operations/V5057	4h	12h	90	Tech[2],QC
92	Remove Drain Line Adapters and Environmental Throat Plugs	1h	1h	91	Tech
93	Perform SSME LPFD Helium Barrier Purge System Venting	1h	1h	92	Tech
94	SSME Controller Power-Up/V9001VL4	1հ	7h	89	QC[3],Engr[4]
95	Shuttle Flight Control System Activation Complete	0h	Oh	94	(-)'A.(-)
96	SSME Controller Load and Sensor Checkout/V9001VL4	1h	7h	95	QC[3],Engr[4]
97	Hydraulic System Pressurization Complete	0h	<b>0</b> h	96	a o [o] i E i i i i
98	Activate SSME 750 psi Pneumatics	0.5h	3.5h	97	QC[3],Engr[4]
99	SSME Hydraulic System Conditioning and Actuator Checkout	0.5h	3.5h	98	QC[3],Engr[4]
100	SSME Flight Readiness Test	2h	16h	99	Tech,QC[3],Engr[4]
101	SSME Controller Power-Down	0h	<b>O</b> h	100	
182	Hydraulics and Flight Control Closeout Operations!	9h	Oh	101	······································
103	Aerosurface and SSME Cycling/V1308	3h	0h		
184	Hydraulic System Compressibility/V9002.07	1.5h	Oh	103	
105	Frequency Response Testing/V1034	3h	0h	103	
106	Hydraulic System Closeouts and Securing/V9002.02	3h	0h	105	
107	SSME Pneumatics Secured	0h	Oh	105	
108	SSME Ball Seal Leak Check Operations/V1046.002/V1046.003I	4h :	27h	88	
109	Install Base Heat Shield Access Ladder/V35-00008	1.5h	4.5h	106	Tech[2],QC
110	SSME/TVC Actuator Hydraulic Power-Down Securing Requirements/V9002.06	3.5h	6.5h		·
111	SSME Engineer Determine Required Power Down Configuration	1h	1h		Engr
112	Install Midstroke Locks/V5057	1.5h	4.5h	111	Tech[2],QC
113	Vent Bleeder Plug at Joint P20.2	1h	1h	112	Tech
114	Install SSME Throat Plugs/V1046.002	2h	6h	\$\$	Tech, QC, Safety
115	Fuel Valve Bali Seal Leak Check/V1046.002	1h	5h	114	Tech,QC[2],Engr[2]
116	Oxidizer Valve Ball Seal Leak Check/V1046.003	1h	5h	115	Tech,QC[2],Engr[2]
117	SSME Hydraulic QD X-Rays/V9002.06	4h	8h	116	Tech,QC
118	LO2 Feed/SSME Pneumatics Vented	0h	Oh	114	
119	LH2 Feed Vented	Oh	0h	115	
120	GO2 Blanking Plate Installation/T1402!	6h	Oh	119	

Table 16. VAB rollin to launch tasks (Continued).

1D	Task Name	Duration	Work	Predecessors	Resource Names
121	GH2 Blanking Plate Installation/T1401!	6h	0h	120	
122	Orbiter/ET 17 inch Disconnect Cavity Purge Verification/V1149!	8h	0h	120,121	
123	Helium Signature Test/V1202!	34h	18h	120,121	
124	SSME Preps for Hellum Signature Testi	7h	18h	1	
125	Install Drain Line Closures	1h	1h		Tech
126	Establish Safety Clears/OK for Thrust Chamber Entry	1h	3h	125	Tech,QC,Safety
127	Perform MCC Liner Taping	2h	6h	126	Tech,QC,Safety
128	Install Throat Plug and Monitor Gage Manifold	2.5h	7.5h	127	Tech,QC,Safety
129	Mate Flexhose Between Supply Panel and Manifold	0.5h	0.5h	128	Tech
130	Perform PV13 GN2 Panel Setup	7h	0h	127	
131	Haz Gas Detection System Preps	3h	0h	130	
132	Pre-Test Helium Intrusion Test	4h	0h	131	
133	MPS GH2/LO2 Feed and SSME Hot Gas System Test	3h	0h	132	
134	GO2 System Test	2h	0h	133	
135	LH2 Feed System	2h	0h	134	
136	Orbiter Post-Test Operations	9h	0h	135	
137	GO2 Blanking Plate Installation/T1402!	6h	0h	135	
138	GH2 Blanking Plate Installation/T1401!	6h	0h	137	
139	Ordnance Installation Operations - Part 1!	40h	Oh	Walter to a construction	
140	Ordnance Installation/PIC Resistance Checks/S5009	16h	Oh	138	· · · · · · · · · · · · · · · · · · ·
141	Ordnance Closeouts/S5009	24h	0h	140	
142	Pre-Launch Hypergolic Propellant Loading Operations/80024!	64h	Oh		
143	Propellant Loading Operations/S0024	40h	Oh	141	
144	Propellant Loading Closeouts/S0024	24h	0h	143	
145	Ordnance Installation Operations - Part 2!	48h	Oh		······································
146	SRSS System Test	8h	0h	144	
147	Ordnance Connect/PIC Resistance Checks/S5009	16h	0h	146	
148	Ordnance Closeouts/S5009	24h	0h	147	
149	LOX System Dewpoint and Conditioning/81005!	6.5h	7.75h	148	
150	SSME Thrust Cover Removal/Drain Line Adapter Installation/V5057	2h	4h	147	Tech,QC
151	Rocketdyne Tech on Station for Dewpoints	2.75h	2.75h	150	Tech
152	Orbiter and ET OI Power-Up	0.5h	0h	150	
153	SSME Trickle Purge Securing	1h	1h	152	Tech
154	MPS 750 psi Pneumatics Activation	1.5h	<b>O</b> h	152	
155	ET LOX Tank, SSME, TSM Vent and Engine Bleed Dewpoint	1.5h	0h	153	
156	Main Fill and Drain Dewpoint	1.75h	0h	154	
157	LOX ET Pressure Maintenance	2.5h	0h	154	
158	LH2 System Dewpoint and Conditioning/\$1006!	9.5h	6h	149	
159	LH2 and MPS/SSMEC Power-Up	2h	6h	150	QC,Engr[2]
160	ET/Orbiter Purge and Sample	5h	Oh	159	GO,EHGI[2]

Table 16. VAB rollin to launch tasks (Continued).

ID	Task Name	Ouration	Work	Predecessors	Resource Names
161	Transfer Line Purge and Sample	1.5h	0h	160	
162	Vaporizer Purge	1h	0h	161	
163	Orbiter Aft Closeout/81287!	100h	290h	148	
164	Aft Confidence Test - Pre-Door Installation	12h	<b>O</b> h	148	
165	SSME MCC Polishing	8h	24h	164	Tech,QC,Safety
166	TVC Actuator Flight Closeout and Insulation Installation/V5057	34h	102h	164	Tech[2],QC
167	MPS Engineering Verification and Walkdown	<b>8</b> h	0h	164	
168	MPS Initial Preps for Flight/V9018.001	8h	Oh	167.	
169	PD15/PD16 ET Standby Pressure Monitor Securing	8h	<b>O</b> h	167	
170	EMHS Insulation Inspection per V41BU0.420	. 8h	24h	168,169	Tech,QC,Safety
171	SSME Engineering Walkdown	8h	40h	170	Engr[5]
172	SSME Initial Preps for Flight/V9018.001	<b>8</b> h	24h	171	Tech,QC,Engr
173	SSME Quality Walkdown per V41BU0.070	16h	32h	171	Tech,QC
174	MPS VJ Line Checks/V9019	8h	<b>O</b> h	173	
175	Verify Midstroke Locks Removed	0h	0h	173	
176	LPFD Baggie Installation	6h	18h	173	Tech,QC,Engr
177	LPFD Baggie Leak Check per V41BU0.380	2h	10h	176	Tech,QC[2],Engr[2]
178	EMHS Debris Shield Removal	8h	8h	177	Tech
179	MPS Protective Cover Removal/V35-00002	16h	0h	176,174	
180	SSME Protective Cover Removal/V5057	8h	8h	179	Tech
181	MPS Solenoid Protective Cover Removal/V35-00003	8h	Oh	179	
182	Install Aft 50-1/50-2 Doors for Flight	4h	0h	181,180,181	
183	MPS Functional Verification for Flight - Post-Door Installation/V9018.001	8h	0h	181	
184	S0007 Launch Countdown Operations!	364.87h	137.85h	· · · · · · · · · · · · · · · · · · ·	
185	80007 Launch Countdown Preps!	80h	36h	163	
186	S0007 Launch Countdown Preps	80h	0h	163	
187	SSME Drag On Panel Purge Preps/S0007VL1 POSU 8	12h	36h	*	Tech,QC,Engr
188	S0007 Seq 14: T-43 hours to T-11 hours!	64h	6.25h	163,186	QC,Engr[2]
189	S0007 Seq 15: T-11 hours to T-6 hours!	7h	21h	188	QC,Engr[2]
190	S0007 Seq 16: T-6 hours to Launch!	8.87h	26.6h	189	QC,Engr[2]
191	Shuttle Liftoff!!	0h	Oh	190	
192	S0007 Seq 17: Post-Launch Securing Operations	16h	48h	191	QC,Engr[2]

Table 17. Example of detailed data for scheduled processing in OMEF.

ID	Task Name	Duration	Work	Predecessors	Resource Names
1	SSME Inspections in Engine Shop (continued)/V1011.02!	67.98h	135.75h		
2	External Inspections!	67.98h	36h		
3	Perform Nozzle External Inspections per V41BU0.030	8h	24h		Tech,QC,Engr
4	Perform Liquid Air Insulator Inspections per V41BU0.033	2h	4h	3	QC,Engr
5	Perform Main Injector LOX Post Bias Checks per V41BU0.034	4h	8h	4	QC,Engr
6	MCC and Nozzie Inspections!	17.5h	34.5h		
7	Install Thrust Chamber Protective Liner	0.5h	0.5h		Tech
8	Perform Post-Flight Nozzle Inspections per V41BU0.353	2h	4h	7	QC,Engr
9	Perform Post-Flight MCC Liner Inspection per V41BU0.351	4h	8h	8	QC,Engr
0	Perform Post-Flight MCC Liner Polishing per V41BU0.351	8h	16h	9	Tech,QC
1	Post-Polishing MCC Liner Inspection per V41BU0.351	1h	2h	10	QC,Engr
2	Perform MCC Bondline Ultrasonic Inspection per V41BU0.031	<b>2</b> h	4h	11	QC,Engr
13	Internal inspectionsi	16.25h	65.25h	6	
14	Perform Flow Recirculation Inhibitor Inspection per V41BU0.040	1h	1h		Engr
5	Perform Main Injector Face Side Inspections per V41BU0.040	4h	4h	14	Engr
6	Perform Main Combustion Chamber Inspections per V41BU0.040	2h	4h	15	QC,Engr
7	Perform Fuel Preburner Internal Inspection per V41BU0.040	4h	8h	, , , , , , , , , , , , , , , , , , , ,	QC,Engr
18	Perform Oxidizer Preburner Internal Inspections per V41BU0.040	4h	4h		Engr
19	Perform Main Injector Internal Inspections per V41BU0.040	4h	4h	17,18	Engr
20	Verify Heat Exchanger Coils Internal Inspection performed per V5E02	0.25h	0.25h	19	QC
21	Perform HPFTP Internal Inspections per V41BU0.075	8h	24h		Tech,QC,Engr
22	Perform HPOTP Internal Inspections per V41BU0.065	8h	16h		Tech,Engr

ID	Task Name	Duration	Work	Predecessors	Resource Names
1	HPFTP Post-Flight Torque Check/V1011.03 Run 1!	3.5h	10.5h		
2	Remove HPFTP Thrust Bearing Housing @ Joint F3.1	0.5h	1.5h		Tech,QC,Engr
3	Install HPFTP Torque Tool	0.5h	1.5h	2	Tech,QC,Engr
4	Perform HPFTP Torque Check per V41BS0.020	0.5h	1.5h	3	Tech,QC,Engr
5	Perform HPFTP Shaft Position and Axial Travel per V41BS0.020	1.5h	4.5h	4	Tech,QC,Engr
6	Install Protective Cover @ HPFTP Joint F3.1	0.5h	1.5h	5	Tech,QC,Engr

ID	Task Name	Duration	Work	Predecessors	Resource Names
1	HPOTP Post-Flight Torque Check/V1011.03 Run 1!	3.75h	11.25h		
2	Remove HPOTP Torque Access Plate @ Joint 09.1	0.25h	0.75h		Tech,QC,Engr
3	Perform HPOTP Torque Check per V41BS0.040	0.5h	1.5h	2	Tech,QC,Engr
4	Perform HPOTP Shaft Travel Measurement per V41BS0.044	<b>2</b> h	6h	3	Tech,QC,Engr
5	Perform PBP Impeller Bolt Lock Inspection per V41BS0.043	0.5h	1.5h	4	Tech,QC,Engr
6	Install HPOTP Torque Access Plate @ Joint 09.1	0.5h	1.5h	5	Tech,QC,Engr

# **APPENDIX C—Unscheduled SSME Operations Data**

Figures 20–24 and tables 18–19 present the detailed data collected from SSME processing experience at KSC relative to unscheduled activities. Figures 20–24 present the remaining unscheduled processing classification types. The sixth, base R&R, is presented in section 5. Following these figures, an unscheduled summary data table (table 18) is presented. Finally, an example of the existing level of detail supporting the flow layouts is presented in table 19.

	Duration		y	Wet	ine	day	/ I	ſhı	ırsı	lay	Ţ	F	rida	y		Sa	itur	day		S	und	ay	
ID	(hr)	Man-hr	4	12	8	4	1	2	8	4		12	8	4	1	12	8	4		12	8	4	12
1	24.43	1		1			1h	•	_		÷		<b>-</b>	MR	À	ссе	ot P	erfo	rit	an	ce T	ime	
2	0.25	0.25	ļ	! !			QC	;	Det	ern	nin		RC										
3	0.25	0.25	İ	!			QC		Init	iate	P	R P	ape	rwc	rk	(			i				į
4	0.5	0.5		į			i				Ó.	5h		٩pp	ly	MR	ID	(if F	Rea	uir	ed)		:
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6	0.5	0.5		1			Eng	ır I	Q	E Re	ese	earc	:h/V	alid	at	e P	R		i				
7	11.98	12		1		1	2h	•				<b>v</b> 1	ИR	Acc	ер	t D	iagr	ost	ics	Tir	ne!		t t
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9	4	4		1			1													tiv	e Ac	tion	
10	13.9	0					;											Del					
11	1 :	0								0	Er	ngr	Dis	pos	itic	on I	PR/I	MR.	Ac	сер	t Ra	ition	ale
12	8	0					1			(	+	<b>□</b> E	ng	Ro	ut	e P	R th	rou	gh	Sig	nat	ure l	Loop
13	2	0					1					0h	0 8	ng	r D	)isp	osit	ion	PF	l Ci	osu	re	:
14	0.5	0					i					0	h I	QE	CI	ose	PR	1					

Figure 20. Base MR accept.

-	Duration		y	Wei	ine	day	Th	urs	day	T	Fric	lay		S	atur	day		Su	nd	ay		7
ID	(hr)	Man-hr	4	12	8	4	12	8	4	12	2 8		4	12	8	4	12	2	8	4	12	7
1	33.42	1		1			1h	_	_	+		_	,	ЙR	Repa	air P	erfo	rn	nan	ce ·	Time	7
2	0.25	0.25		:		0.	25h	∃D€	eterr	nine	PR						1				-	
3	0.25	0.25				0.	25h	ı İni	itiate	PF	Pa	erv	vo	rk			ì				į	ļ
4	0	0		į			i			•	·	•	T	ime	/Res	our	es f	or	Co	rre	ctive	Action (Varie
5	0.5	0.5					1			-	0.5					l ID						1
6	11.98	12		! !			121	-		<b>-</b>	Mr F									,	1	ŀ
7	8	8		! !			81	ı							-							
8	4	4					;	4	lh C	j E	ngr	Mg	t I	Dete	rmir	ne C	orre	cti	ve	Act	idn	1
9	32.43	12.5				12	.5h				Ť										Time	el.
10	0.5	0.5					0.51	1 C	DE R	ese	arch	/Val	id	ate	PR						ŀ	
11	4	4					† †	4	h c			Engi	r [	)isp	ositi	on P	R/M	1R	Re	pai	r Rat	ionale (Varie
12	8	8					( (			8h		<u></u>	n	gr R	oute	PR	thro	ou	gh.	Sigi	natu	re Loop
13	2.5	0					1			i	0	h 🔻	7	ИR	Rep	air [	Delay	y T	im	e!	1	1
14	2	0					•			;	-	Oh 🛭	E	ngr	Disp	osit	ion	PF	R C	losi	ıře	
15	0.5	0								!		0h	1	DE C	lose	PR					į	

Figure 21. Base MR repair.

T	Duration	Man ba		Wed	ines	day	Th	ursc	lay	F	rida	y	S	atu	rda	ay	S	und	ay	
	(hr)	Man-hr	4	12	8	4	12	8	4	12	8	4	12	8		4	12	8	4	12
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3	0.25	0.25		1 1		0.5	25h	1	nitiat	e PF	R Pap	erw	ork				i I			I I
4	0.5	0.5		l I		0.	.5h '	▼ P	R A	lmin	istra	tive	Tim	е			l I			;
5	0.5	0.5		 		0.	,5h	1 C	E Re	sea	rch/\	/aild	ate !	PR			 			I I
6	5	5		) 			¦5h ¹	•	PR	Diag	gnos	tics	Tim	е			 			1
7	4	4		] }			¦ 4h		Eng	r/Mg	t Re	view	/As	ses	s P	PR	1			1
8	1	1		t t			1	<b>1</b> h [	Eng	r/Mg	jt De	tern	nine	Со	rre	ectiv	/e A	ction	1	-
9	9.48	9.5		l I			9.5	ih ▼	_	<b>⋫</b> PF	R De	lay 1	ime				 			
10	4	4		l I				4h c	E	ngr	Disp	ositi	on F	PR			1			
11	4	4	-					4	h _	Eng	r Rt	PR ·	thro	ugh	S	ign	atur	e Lo	ор	j i
12	1	1		 			 		1h g	Eng	ır Di:	spos	itio	ı Pf	٦ (	Clos	ure			
13	0.5	0.5		 			    -	0	. <b>5</b> h (	En	gr D	ispo	sitic	n P	R	Clo	sure			i I

Figure 22. Base PR accept.

	Duration			We	dnes	day	Th	ursd	ay		Fr	ida	7	S	atur	da	y	S	und	ay		]
ID	(hr)	Man-hr	4	12	8	4	12	8	4	12	2	8	4	12	8		4	12	8	4	12	
1	6.98	0.5				0.	5h ₹	_	P	RF	er	forr	nano	ce T	ime			! !			!	
2	0.25	0.25				0.	25h	ı De	eter	mir	ne F	PR (	Cond	ditio	n			1			:	
3	0.25	0.25		!		0.	25h	ı In	iitiai	te F	PR	Pap	erw	ork				:			!	
4	0	0		į			į	4	▶ Ti	me,	/Re	SOL	rces	s fo	r Co	rr	ecti	ve A	ctio	n (V	aries	w/PR Classification)
5	2	2		i			2h	<b>→</b> F	PR (	Diag	gno	stic	s Ti	me				:			i	
6	1	1		:				hı Er										!			}	
7	1	1	l	!			1	hıE	ngr	/M(	gt C	Dete	rmi	ne (	orr	ec	tive	Act	ion		!	
8	6.5	4.5	l	į		4.	5h 🔻		₹ P	R A	۱dn	ninis	strat	ive	Tim	е		!			į	
9	0.5	0.5	l	;		C	).5h i	QE	Re	sea	rch	ı/Va	lidat	te P	R			:			;	
10	0	0	l					<b>♦</b> E	Engi	r Di	ispo	ositi	on l	PR (	(Var	ies	S W	ith F	epa	ir Cl	assit	ication)
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12	1.5	0		į			. (	Oh 🗖	P PI	ŖD	ela	y Ti	me									
13	0	0		i				0h 🛭	En	gr l	Dis	pos	itior	ı PF	R CI	os	ure				ì	
14	0.5	0					!	0h (	ı QE	Cl	ose	e PF	₹								!	

Figure 23. Base PR repair.

T.,	Duration			Wed	ne	sda	ay	Th	ı	rs	sda	y .	Ι	F	ric	iay		S	at	110	lay	L	ť	Su	nd	ay	ı		]
LID	(hr)	Man-hr	4	12	8		4	12	Ι	8	B	4	ľ	12	8	3	4	12	?	8	Ī	1	12	!	8		4	12	]
1	0.48	0.5					0.	5h •	•	٠١	Wa	ive	r I	Per	fo	rm	and	e T	im	е			! !						
2	0.25	0.25					0.2	25h	1	1	Det	teri	m	ine	PI	R C	on	diti	on										
3	0.25	0.25		!			0.2	25h	1		Init	tiat	te	PR	P	ape	erw	ork										ļ	1
4	0.5	0.5					0.	5h •	7	, 1	Wa	ive	ŗ	Ad	mi	inis	tra	tive	Ti	me	,		į					į	
5	0.5	0.5					0.	.5h	1	1	QΕ	Re	es	ear	ch	Νa	ild	ate	PF				:					ŀ	
6	11.98	12					1	2h	¥	_		▼	W	Vaiv	er	Di	agr	105	ics	T	im	е						!	
7	8	8						8h	6	_	_	Er	ŋg	jr/N	1g	t R	evi	ew/	As	se	SS	P	3					:	
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14	0.5	0					ļ						!	0	h	B (	)E	Clo	se	PF	1							!	

Figure 24. Base waiver/exception.

Table 18. SSME unscheduled processing summary.

ID	SSME PR Classification	Tech Base Peri MHrs	QC Base Perf MHrs	Engr Base Diag MHrs	Engr Base Admin MHrs	Total Base MHrs	Tech Pari MHrs	QC Perf MHrs	Engr Perf MHrs	Total Perf MHrs	Total MHrs	No. Techs	No. QCs	No. Engrs
1_	48hr Drying OMRSD Waiver	0	0.5	12	0.5	13	0	0	0	0	13	0	0	1
2	AFV Filter R&R	0	0.5	2	6.5	9	1	1	8.5	10.5	19.5	1	1	
3	Baggie Hose R&R	0	0.5	2	6.5	9	1.25	1.25	0	2.5	11.5	1	1	<del></del>
4	Baggie Hose Repair	0	0.5	2	4.5	7	1	1	0	2	9	1	1	+
5	Baggie R&R	0	0.5	2	6.5	9	1.5	1.5	0	3	12	1	1	+
6	Baggie Repair	0	0.5	2	4.5	7	0.75	0.75	0	1.5	8.5	1	1	+
7	Battery R&R	0	0.5	2	6.5	9	1.25	1.25	0	2.5	11.5	1	1	1
8	Burst Diaphragm R&R	0	0.5	2	6.5	9	0.5	0.5	0	1	10	1	1	<del> </del>
9	Contamination MR Repair	0.5	0.5	12	12.5	25.5	1.25	1.25	0	2.5	28	1	1	+
10	Contamination Repair	0	0.5	2	4.5	7	1.75	1.75	0	3.5	10.5	1	1	<del></del>
11	Contamination/Corrosion Accept	0	0.5	5	0.5	6	0	0	0	0	6	0	0	<del></del>
12	Contamination/Corrosion MR Accept	0.5	0.5	12	0.5	13.5	0	0	0	0	13.5	0	0	
13	Contamination/Corrosion Waiver	0	0.5	12	0.5	13	0	0	0	0	13	0	0	<del> </del>
14	Controller R&R: Post-FRT	0	0.5	2	6.5	9	154.5	74.25	93.25	322	331		па	na
15	Controller R&R: Pre-FRT	0	0.5	2	6.5	9	35.5	14.5	13	63	72		na	na
16	Coolant Diffuser R&R	0	0.5	2	6.5	9	2	2	0	4	13	1		
17	Coolant Duct R&R	0	0.5	2	6.5	9	2	2	0	4	13	1	<del></del>	<del>                                     </del>
18	EDNI Accept	0	0.5	5	0.5	6	0	0	0	0	6	0		<del></del>
19	EDNI MR Repair	0.5	0.5	12	12.5	25.5	5.5	5.5	0	11	36.5	1	1	<u> </u>
20	EDNI R&R	0	0.5	2	6.5	9	7	7	0	14	23	1	1	1
21	EDNI Repair	0	0.5	2	4.5	7	6	6	0	12	19	1	_ ;	· · · · · ·
22	Elliptical Plug R&R	0	0.5	2	6.5	9	1	1	0	2	11	1	1	
23	Engine Assembly R&R	0	0.5	2	6.5	9	8	8	8.5	24.5	33.5	1	1	+
24	Engineering Change	0	0.5	12	0.5	13	0	0	0.0	0	13	0	0	-
25	Flange Sealing Surface MR Repair	0.5	0.5	12	12.5	25.5	3.5	3.5	24.5	31.5	57	1	1	†
26	Flange Sealing Surface Repair	0	0.5	2	4.5	7	4	4	6.5	14.5	21.5	1	1	1
27	FPB Oxidizer Supply Duct R&R: Post-HPOTP	0	0.5	2	6.5	9	22.5	14.5	1	38		na	na	na
28	FPB Oxidizer Supply Duct R&R: Pre-HPOTP	0	0.5	2	6.5	9	13	9	0	22	31		па	па
29	Fuel Bleed Duct R&R	0	0.5	2	6.5	9	5	5	0	10	19	1	1	(
30	Functional Failure Accept	0	0.5	5	0.5	6	0	0	0	0	6	0	0	+
31	Functional Failure Clean/Adjust	0	0.5	2	4.5	7	4	4	0	8	15	1	1	
32	Functional Failure MR Accept	0.5	0.5	12	0.5	13.5	- 0	0	0	0	13.5	0	0	
33	Functional Failure Reperform/Retest	0	0.5	2	4.5	7	2.5	2.5	0	5	13.5	1	1	
34	Functional Failure Waiver	0	0.5	12	0.5	13	0	0	0	0	13	0	0	ļ
35	GCV Assembly R&R	0	0.5	2	6.5	- 13	3	3	0	6		na	na U	na

Table 18. SSME unscheduled processing summary (Continued).

ID	SSME PR Classification	Tech Base Perf MHrs	QC Base Perf MHrs	Engr Base Diag MHrs	Engr Base Admin MHrs	Total Base MHrs	Tech Perf MHrs	QC Perl MHrs	Engr Perf MHrs	Total Perf MHrs	Total MHrs	No. Techs	No. QCs	No. Engrs
36	Hardware Configuration Accept	0	0.5	5	0.5	6	0	0	0	0	6	0	0	0
37	Hardware Configuration MR Accept	0.5	0.5	12	0.5	13.5	0	0	0	0	13.5	0	0	
38	Hardware Configuration MR Repair	0.5	0.5	12	12.5	25.5	2.5	2.5	0	5	30.5	1	1	0
39	Hardware Configuration Reinstallation	0	0.5	2	4.5	7	3	3	0	6	13	1	1	0
40	Hardware Configuration Waiver	0	0.5	12	0.5	13	0	0	0	0	13	0	0	0
41	Hardware Crack/Weld Defect MR Repair	0.5	0.5	12	12.5	25.5	7.5	7.5	0	15	40.5	1	1	0
42	Hardware Crack/Weld Defect Repair	0	0.5	2	4.5	7	8	8	0	16	23	1	1	0
43	Hardware Damage Accept	0	0.5	5	0.5	6	0	0	0	0	6	0	0	0
44	Hardware Damage MR Accept	0.5	0.5	12	0.5	13.5	0	0	0	0	13.5	0	0	0
45	Hardware Damage MR Repair	0.5	0.5	12	12.5	25.5	3.5	3.5	0	7	32.5	1	1	0
46	Hardware Damage Repair	0	0.5	2	4.5	7	4	4	0	8	15	1	1	0
47	Hardware Damage Waiver	0	0.5	12	0.5	13	0	0	0	0	13	0	0	0
48	Harness Accept	0	0.5	5	0.5	6	0	0	0	0	6	0	0	0
49	Harness MR Accept	0.5	0.5	12	0.5	13.5	0	0	0	0	13.5	0	0	
50	Harness MR Repair	0.5	0.5	12	12.5	25.5	2	2	0	4	29.5	1	1	0
51	Harness R&R: Post-FRT	0	0.5	2	6.5	9	11	4	4	19	28	na	na	na
52	Harness R&R: Pre-FRT	0	0.5	2	6.5	9	3	3	0	6	15	1	1	0
53	Harness Repair	0	0.5	2	4.5	7	2.5	2.5	o İ	5	12	1	1	0
54	Heat Shield Clip/Bracket R&R	0	0.5	2	6.5	9	1	1	0	2	11	1	1	0
55	Hot Gas Manifold R&R	0	0.5	2	6.5	9	4	4	8.5	16.5	25.5	1	1	1
56	HPFD R&R: Pad	0	0.5	2	6.5	9	70.75	27.25	9	107	116	na	па	na
57	HPFD R&R: Shop Post-FRT	0	0.5	2	6.5	9	37.25	26.75	8	72	81		na	na
58	HPFD R&R: Shop Pre-HPFTP R&R	0	0.5	2	6.5	9	23.25	13	2.5	38.75	47.75		na	na
59	HPFTP Bellows Shield R&R	0	0.5	2	6.5	9	2	2	0	4	13	1	1	0
60	HPFTP R&R: Pre-R&R	0	0.5	2	6.5	9	0	0	0	0		na	na	na
61	HPFTP Thrust Bearing Housing R&R	0	0.5	2	6.5	9	8	8	0	16	25	1	1	0
62	HPOTP Preburner Volute R&R	0	0.5	2	6.5	9	16	16	0	32	41	1	1	0
63	HPOTP R&R: Pre-R&R	0	0.5	2	6.5	9	0	0	0	0		na	na	na
64	HPOTP Turbine Housing R&R	0	0.5	2	6.5	9	2	2	0	4	13	1	1	0
65	HPV Assembly R&R	0	0.5	2	6.5	9	8	8	0	16	25	1	1	0
66	Hydraulic QD R&R	0	0.5	2	6.5	9	6	6	0	12	21	1	1	0
67	Igniter R&R	0	0.5	2	6.5	9	2	2	0	4	13	1	1	0
68	Line Assembly R&R	0	0.5	2	6.5	9	5	5	0	10	19	<del>                                     </del>	1	0
69	LOX Post Support Pin R&R	0	0.5	2	6.5	9	0	10	8.5	18.5	27.5	0	1	1
70	LPFD R&R: OPF/Pad	0	0.5	2	6.5	9	64.75	24.75	5.5	95	104		па	na

Table 18. SSME unscheduled processing summary (Continued).

ID	SSME PR Classification	Tech Base Peri MHrs	QC Base Peri MHrs	Engr Base Diag MHrs	Engr Base Admin MHrs	Total Base MHrs	Tech Perf MHrs	QC Perf MHrs	Engr Porf MHrs	Total Perf MHrs	Total MHrs	No. Techs	No. QCs	No. Engrs
71	LPFD R&R: Shop Pre-HPFTP R&R	0	0.5	2	6.5	9	23.5	11.5	2.5	37.5	46.5	na	na	па
72	LPFT Discharge Duct R&R	0	0.5	2	6.5	9	26	10	0	36	45	na	na	па
73	LPFT Drive Duct R&R	0	0.5	2	6.5	9	25	10	0	35	44	na	па	na
74	LPFTP R&R	0	0.5	2	6.5	9	53.5	29	11.5	94	103	па	na	па
75	LPOD R&R	0	0.5	2	6.5	9	57.25	26.25	4	87.5	96.5	па	na	na
76	LPOTP R&R	0	0.5	2	6.5	9	52.5	28.5	13	94	103	na	na	na
77	Main Injector Assembly R&R	0	0.5	2	6.5	9	4	4	8.5	16.5	25.5	1	1	1
78	MCC Assembly R&R	0	0.5	2	6.5	9	4	4	8.5	16.5	25.5	1	1	
79	MCC Roughness Repair	0	0.5	2	4.5	7	4	4	6.5	14.5	21.5	1	1	1
80	Miscellaneous Hardware Config. MR Repair	0.5	0.5	12	12.5	25.5	2	2	0	4	29.5	1	1	
81	Miscellaneous Hardware Config. Repair	0	0.5	2	4.5	7	2.5	2.5	0	5	12	1	1	(
82	Miscellaneous Hardware Damage MR Repair	0.5	0.5	12	12.5	25.5	2	2	0	4	29.5	1	1	
83	Miscellaneous Hardware Damage Repair	0	0.5	2	4.5	7	2.5	2.5	0	5	12	1	1	(
84	Miscellaneous Hardware R&R	0	0.5	2	6.5	9	6	6	0	12	21	1	1	(
85	MOVA R&R: Pad	0	0.5	2	6.5	9	79.5	50.25	62.75	192.5	201.5	na	па	na
86	MOVA R&R: Shop	0	0.5	2	6.5	9	29.25	18.75	3.5	51.5	60.5	па	na	na
87	Nozzie FRI R&R	0	0.5	2	6.5	9	221.5	119.25	54	394.75	403.75	na	na	na
88	Nozzie R&R: Post-Testing	0	0.5	2	6.5	9	245	133.75	65	443.75	452.75	na	na	na
89	Nozzle R&R: Pre-Testing	0	0.5	2	6.5	9	213.5	111.25	54	378.75	387.75	na	па	па
90	Nozzie TPS MR Repair	0.5	0.5	12	12.5	25.5	5.5	5.5	0	11	36.5	1	1	
91	Nozzie TPS R&R	0	0.5	2	6.5	9	8	8	0	16	25	1	1	(
92	Nozzie TPS Repair	0	0.5	2	4.5	7	4	4	0	8	15	1	1	(
93	Nozzle Tube Leak MR Accept/Waiver	0	0.5	12	0.5	13	0	0	0	0	13	0	0	) (
94	Nozzle Tube Leak MR Repair	0.5	0.5	12	12.5	25.5	7.5	7.5	24.5	39.5	65	1	1	1
95	OPB Oxidizer Supply Duct R&R	0	0.5	2	6.5	9	6	4	0	10	19	na	na	па
96	Orifice R&R	0	0.5	2	6.5	9	2	2	0	4	13	1	1	(
97	PCA Assembly R&R	0	0.5	2	6.5	9	12	12	0	24	33	1	1	
98	Pogo Baffle R&R	0	0.5	2	6.5	9	51.25	24.25	4	79.5	88.5	na	na	na
99	Powerhead Assembly R&R	0	0.5	2	6.5	9	4	4	8.5	16.5	25.5	1	1	
180	Requirement/Documentation Change	0	0.5	12	0.5	13	0	0	0	0	13		0	
101	RIV Assembly R&R	0	0.5	2	6.5	9	6.75	6.75	0	13.5	22.5	па	na	na
102	Seal R&R	0	0.5	2	6.5	9	1	1	0	2	11	1	1	(
103	Sensor Accept	0	0.5	5	0.5	6	0	0	0	0	6	0	0	
104	Sensor Mount R&R	0	0.5	2	6.5	9	1	1	0	2	11	1	+	
105	Sensor MR Accept	0.5	0.5	12	0.5	13.5	0	0	0	0	13.5	0	+	
106	Sensor R&R: Post-Checkouts	0	0.5	2	6.5	9	19	8	8	35		na	na	na

Table 18. SSME unscheduled processing summary (Continued).

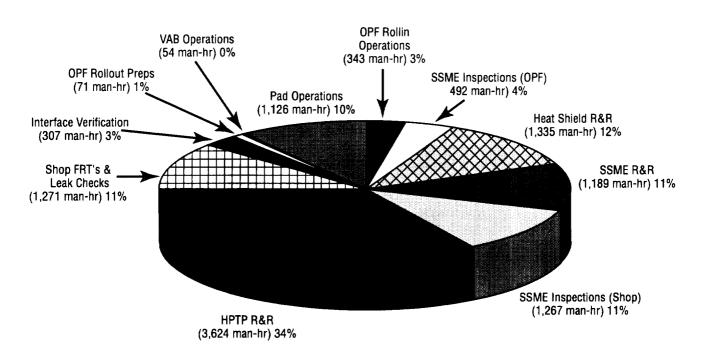
ID	SSME PR Classification	Tech Base Perf MHrs	QC Base Perf MHrs	Engr Base Diag MHrs	Engr Base Admin MHrs	Total Base MHrs	Tech Perf MHrs	QC Perf MHrs	Engr Perf MHrs	Total Perf MHrs	Total MHrs	No. Techs	No. QCs	No. Engrs
107	Sensor R&R: Pre-Checkouts	0	0.5	2	6.5	9	1	1	0	2	11	1	1	0
108	Sensor Repair	0	0.5	2	4.5	7	2.5	2.5	0	5	12	1	1	C
109	Stud/Bolt R&R	0	0.5	2	6.5	9	3	3	0	6	15	1	1	(
110	Surface Corrosion MR Repair	0.5	0.5	12	12.5	25.5	3.5	3.5	0	7	32.5	1	1	C
111	Surface Corrosion Repair	0	0.5	2	4.5	7	4	4	0	8	15	1	1	
112	Surface Discoloration MR Repair	0.5	0.5	12	12.5	25.5	3.5	3.5	0	7	32.5	1	1	0
113	Surface Discoloration Repair	0	0.5	2	4.5	7	4	4	0	8	15	1	1	
114	Threads Damage Repair	0	0.5	2	4.5	7	3	3	0	6	13	1	1	0
115	TVCA Pin R&R	0	0.5	2	6.5	9	5	5	0	10	19	1	1	C
116	Valve Actuator R&R: Pad Post-Testing	0	0.5	2	6.5	9	99.5	63	74	236.5	245.5	na	na	na
117	Valve Actuator R&R: Pad Pre-Testing	0	0.5	2	6.5	9	49.25	31.5	14.75	95.5	104.5	na	na	па
118	Valve Actuator R&R: Shop Pre-Testing	0	0.5	2	6.5	9	49.25	31.5	14.75	95.5	104.5	па	na	na
119	Valve R&R: Pad	0	0.5	2	6.5	9	127.75	80.25	93.5	301.5	310.5	na	na	na
120	Valve R&R: Shop Post-Testing	0	0.5	2	6.5	9	127.75	80.25	93.5	301.5	310.5	na	na	na
121	Valve R&R: Shop Pre-Testing	0	0.5	2	6.5	9	77.5	48.75	18.25	144.5	153.5	na	па	na
122	HPFTP R&R: Post-R&R	0	0.5	2	6.5	9	197	122.75	56	375.75	384.75	na	na	na
123	HPOTP R&R: Post-R&R	0	0.5	2	6.5	9	239.5	142.25	53.25	435		па	na	па

Table 19. Example of detailed data for unscheduled processing.

ID	Task Name	Duration	Work	Predecessors	Resource Names
1	LPFTP Removal and Replacement/V5E241	37.5h	94h		
2	LPFTP GSE Removal Prepsi	2h	6h		
3	Verify Proofload	2h	<b>4</b> h		Tech,QC
4	Perform LPFTP Receiving Inspection	1h	2h		Tech,QC
5	LPFTP Removal Prepsi	20.5h	25.5h		: : : : : : : : : : : : : : : : : : :
6	LAI Removal	2h	2h		Tech
7	Disconnect LPFTP Drain Line @ Joint D17	0.5h	0.5h	6	Tech
8	Disconnect LPFD @ Joint F2	3h	3h	7	Tech
9	Support LPFD	0.5h	0.5h	8	Tech
10	Disconnect LPFT Drive Duct @ Joint F8	3h	3h	9	Tech
11	Support LPFT Drive Duct	0.5h	0.5h	10	Tech
12	Disconnect LPFT Discharge Duct @ Joint F9	<b>3</b> h	3h	11	Tech
13	Support LPFT Discharge Duct	0.5h	0.5h	12	Tech
14	Demate Connectors @ LPFT Speed Transducer Joint F1.1	1h	1h	13	Tech
15	Install Handler Sling	1h	1h	14	Tech
16	Reference Check Joints F2, F8 and F9	5h	10h	15	Tech,QC
17	Horizontal Handler Removal Preps	0.5h	0.5h	16	Tech
18	LPFTP Removal from Engine!	7.25h	23.5h		· · · · · · · · · · · · · · · · · · ·
19	Establish Safety Clears for LPFTP Removal	0.25h	1.5h		Tech[3],QC,Safety,Engr
20	Connect J-Hook to Handler Sling	1h	6h	19	Tech[3],QC,Safety,Engr
21	Lower LPFTP to Floor	1h	6h	20	Tech[3],QC,Safety,Engr
22	Install LPFTP into Shipping Container	5h	10h	21	Tech,QC
23	LPFTP installationi	2.25h	13.5h	21	
24	Establish Safety Clears for LPFTP Installation	0.25h	1.5h		Tech[3],QC,Safety,Engr
25	Connect J-Hook to Handler Sling	1h	6h	24	Tech[3],QC,Safety,Engr
26	Install LPFTP onto Engine	1h	6h	25	Tech[3],QC,Safety,Engr
27	LPFTP Securingi	11.5h	24.5h	23	10011[0],40,041019,21191
28	Torque and Stretch Joint F9	2h	4h	<u> </u>	Tech,QC
29	Torque and Stretch Joint F8	2h	4h	28	Tech,QC
30	Torque and Stretch Joint F2	2h	4h	29	Tech,QC
31	Install LPFTP Speed Transducer @ Joint F1.1	1h	2h	30	Tech,QC
32	Perform Electrical Connector Mates	2h	4h	31	Tech,QC
33	Secure LPFTP Drain Line @ Joint D17	0.5h	1h	32	Tech.QC
34	Perform LPFTP Torque Check	1.5h	4.5h	33	Tech,QC,Engr
35	RTV Bolt Heads @ Joints F2, F8 and F9 and Reinstall LAI	0.5h	1h	34	Tech,QC
36	Retest Verification!	1h	1h	27	Engr

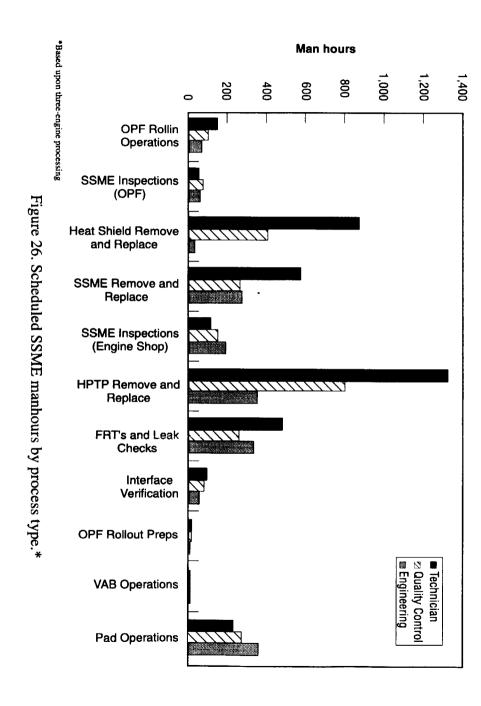
## APPENDIX D-Pertinent SSME Results From Analysis of Data Collected

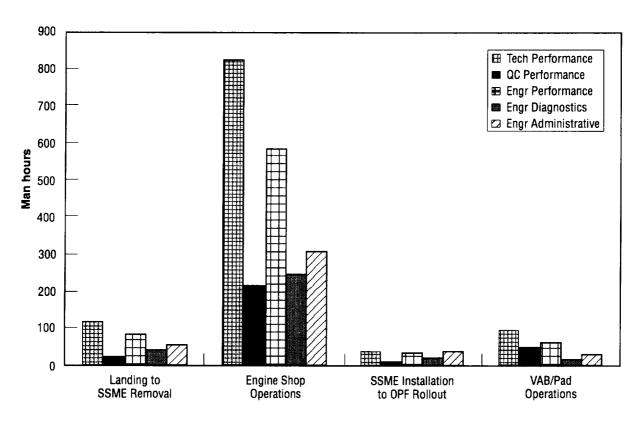
Figures 25–28 present examples of the fidelity of results supported by the data collected. These results, of course, apply to SSME processing and are subject to the assumptions, ground rules, and constraints described in section 5.



<sup>\*</sup>Based upon three-engine processing

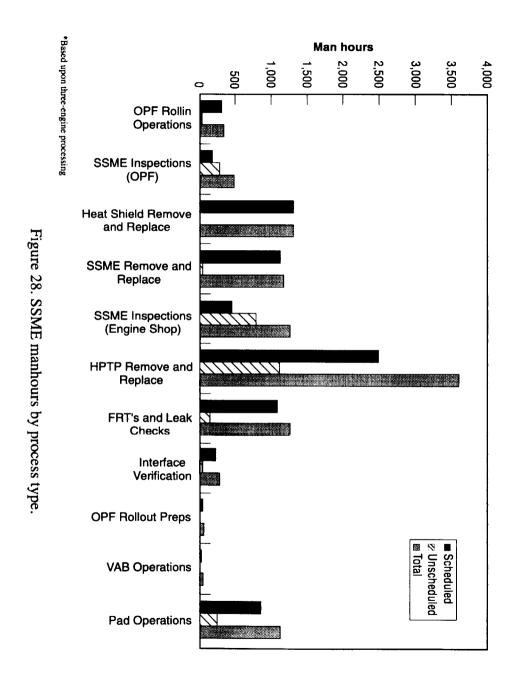
Figure 25. Total SSME manhours by process type.\*





<sup>\*</sup>Based upon three-engine processing

Figure 27. Unscheduled SSME manhours by process type.\*



### APPENDIX E—Reliability of Engine Sets With Engine Out Capability

The reliability estimates of future launch vehicles can be further refined upon receipt of more accurate estimates of engine reliability, catastrophic failure probabilities, coverage time, and trajectory requirements. This is a discussion of the effect of engine out capability and time of engine out on the reliability of aerospace vehicles. This study looks at sample data, sets out basic formulas, and presents results related to the issue of engine out. For the purpose of this study, only engine data will be considered. Upstream component reliabilities such as tanks, feed systems, power systems, etc. will be omitted.

Certain definitions are important to this discussion. Engine failure is failure to provide the level of thrust desired at the time desired. Catastrophic failure in an engine is a failure that results in a failure of a second engine in an engine set. Benign failure is the proportion of failures where failure does not result in catastrophic failure. Time of engine out refers to the time at which an engine can be shut down and the remaining engines will still provide the necessary thrust to achieve the desired orbit. Time of engine out refers to a known event.

Engine out capability is generally believed to provide increased overall engine set reliability. For example, using a binomial distribution<sup>27,28</sup> to analyze the example of three engines with one engine out at launch is as follows:

 $R = p^n + np^{n-1}(1-p)$ ; where R is the engine set reliability, p the engine reliability, and n the number of engines with one engine out capability.

A comparison between a two-engine set with no engine out capability and a three-engine set with one engine out capability is presented in table 20.

Engine Reliability ( <i>R</i> )	Two Engines/ No Out ( <i>R=p2</i> )	Three Engines/ One Out ( <i>R</i> )
0.95	0.903	0.993
0.97	0.941	0.997
0.99	0.98	0.9997
0.999	0.998	0.999997

Table 20. Engine out capability comparison.

With a baseline engine reliability at the above values, there is a significant gain displayed by a three-engine set with one engine out as opposed to the two-engine set with no engine out capability. The gain diminishes as the engine reliability improves.

This analysis is now expanded. The cases need to be examined where catastrophic failure fraction and coverage times are varied. The formula that incorporates time of engine out and benign failure fraction is:<sup>29</sup>

$$R_{EO} = S^n T_d^n R^n [1 + T_u^{n-1} bn(R^{-c} - 1)]$$
.

The parameters in the formula are:

R =Engine reliability

 $R_{EO}$  = Engine set reliability

S = Startup reliability

 $T_d$  = Throttle-down reliability

 $T_u$  = Throttle-up reliability

b = Benign failure fraction

c = Coverage

n = Number of engines.

For the following analysis, the formula will be simplified by setting both the throttle reliability and and startup reliability to 1. It is assumed, in this case, that throttling is accomplished within design margins and that startup reliability is ensured by some event such as holddown, both reasonable assumptions.

One study of the SSME<sup>30</sup> has suggested that such a catastrophic failure could occur in the main engines approximately 17 percent of the time (benign failure fraction of 83 percent). This is derived data based on a small amount of data—almost all main engine tests have occurred singly and the study concluded that only 3 of 17 failures could have resulted in a second engine failure. This conclusion was generated based on the incidence of explosions and test stand damage that occurred. The small amount of data, typical in the aerospace industry, makes it difficult to draw definitive conclusions or to use confidence intervals.

Another factor to be considered in overall engine set reliability is the time of engine out. If all three engines are needed for 100 sec of flight and then only two are necessary to obtain orbit, this time of engine out translates to an increased reliability for the engine system.

With example engine reliability, table 21 can be generated. Two conclusions can be drawn. First the probability of catastrophic failure rather quickly degrades the increase of reliability gained due to engine out capability. From table 21, at 0.97 reliability and engine out at time 0, a catastrophic failure probability increase from 0.1 to 0.25 results in a decline in reliability from 0.9889 to 0.9762 for the three-engine case. Still, this is considerably higher than the two-engine, no out case reliability of 0.941.

Second, it is evident that reliability can be gained if some engine out time is possible. For example, if engine out is possible for two-thirds of the flight (0.97 engine reliability and 0.2 catastrophic failure factor), then the reliability goes from 0.913 to 0.9578—a significant gain. Note that the engine reliability at t=1 for all catastrophic failure factor values is equal to the n engines/no out capability since this is equivalent to all engines being necessary for the full-duration flight.

Table 21. Engine out and time of engine out comparison.

Engine Reliability	Catastrophic Failure Probability	Engine Out Time	Three Engines/ One Out Reliability
0.95	0.1	0	0.9792
		0.33	0.9383
		0.67	0.8969
		1	0.8574
	0.2	0	0.9657
		0.33	0.9293
		0.67	0.8925
		1 1	0.8574
	0.25	Ö	0.9589
	5.25	0.33	0.9248
		0.67	0.8903
		1	0.8574
0.97	0.1	Ö	0.9889
0.37	0.1	0.33	0.9635
		0.67	0.9376
			0.9127
	0.0	1 0	
	0.2		0.9804
		0.33	0.9578
		0.67	0.9348
	0.05	1	0.9127
	0.25	0	0.9762
		0.33	0.9550
		0.67	0.9334
		1 1	0.9127
0.99	0.1	0	0.9968
		0.33	0.9880
		0.67	0.9790
		1	0.9703
	0.2	0	0.9938
		0.33	0.9860
		0.67	0.9780
		1 1	0.9703
	0.25	0	0.9924
		0.33	0.9850
		0.67	0.9776
		1 1	0.9703
0.999	0.1	0	0.9997
		0.33	0.9988
		0.67	0.9979
		1 1	0.9970
	0.2	o l	0.9994
	<del>-</del>	0.33	0.9986
		0.67	0.9978
		1 1	0.9970
	0.25	Ö	0.9992
	0.20	0.33	0.9985
		0.67	0.9977
		1 1	0.9970
			5.001

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This paper describes the methodology, model, input data, and analysis results of a reusable launch vehicle engine operability study conducted with the goal of supporting design from an operations perspective. Paralleling performance analyses in schedule and method, this requires the use of metrics in a validated operations model useful for design, sensitivity, and trade studies. Operations analysis in this view is one of several design functions.

An operations concept was developed given an engine concept and the predicted operations and maintenance processes incorporated into simulation models. Historical operations data at a level of detail suitable to model objectives were collected, analyzed, and formatted for use with the models, the simulations were run, and results collected and presented. The input data used included scheduled and unscheduled timeline and resource information collected into a Space Transportation System (STS) Space Shuttle Main Engine (SSME) historical launch operations database. Results reflect upon the importance not only of reliable hardware but upon operations and corrective maintenance process improvements.

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